(303) 333-1105

FAX (303) 333-1107
E-mail: Isc@Iscdenver.com

November 29, 2021
Mr. Richard Bratton
Gunnison Valley Properties, LLC
864 W. South Boulder Road, Suite 200
Louisville, CO 80027

Re: Gunnison Rising
Summary of Previous Studies
Gunnison, CO
LSC \#2 10040

Dear Mr. Bratton:
In response to the project team's request, LSC Transportation Consultants, Inc. has prepared this memorandum summarizing our work on previous traffic studies and CDOT access permits for the proposed Gunnison Rising development in Gunnison, Colorado.

## GUNNISON RISING MASTER TRAFFIC STUDY - BASIS OF ANNEXATION AND PUD APPROVAL

The Gunnison Rising - "Authentically Colorado" Master Plan Level Traffic Impact Analysis was completed by LSC on December 12, 2006. A Transportation Update Memo was completed on June 8, 2007 to address minor changes in the land use plan. These documents provide the transportation details that supported the annexation of the property into the City of Gunnison and the approved PUD.

## US HIGHWAY 50 ACCESS STUDY - CONCEPTUAL APPROVAL OF ACCESS A THROUGH ACCESS F

The City of Gunnison and CDOT completed the November, 2013 Access Study for US Highway 50 from Milepost 157.344 at SH 135 east to Milepost 161.250 which is further east than Ute Lane (East). The study was completed per the agreements reached with the annexation of the Gunnison Rising property noted above and included Access A through Access F. It also assumed local connectivity west to College Avenue, Georgia Avenue, and San Juan Avenue.

## GUNNISON RISING GOVERNMENT CAMPUS SUBDIVISION TRAFFIC IMPACT STUDY BASIS FOR ACCESS PERMITS FOR ACCESS E AND F

The first two access permits issued for Gunnison Rising are a public access aligning with Ute Lane (West) for public access and an emergency-only access aligning with Ute Lane (East).

These access permits will serve the planned Government Campus and RV Campground area of Gunnison Rising. Access Permit \#320085 was issued for Access E on September 24, 2020 and updated with Access Permit \#321037 on March 15, 2021. Access Permit \#320086 was issued for Access F on September 24, 2020. A one-year extension was granted for Access Permit \#320086 and a one-year extension will be needed for Access Permit \#321037 by March 15, 2022. Once this occurs, both active access permits will have one one-year extension available. These actions were supported by the August 28, 2020 and subsequent February 12, 2021 Gunnison Rising Government Campus Subdivision TIA by LSC. The applicant team is actively preparing construction plans for Access E and F to secure approval from CDOT (NTP) to construct the improvements in 2022.

## GUNNISON RISING ACCESS POINTS A AND B TRAFFIC IMPACT STUDY

An access permit from CDOT is currently being pursued for Access B. The February 25, 2021 Gunnison Rising Access Points A and B TIA by LSC was completed to support this effort. The TIA assumed US 50 access at Access A and Access B and local access west to College Avenue and Georgia Avenue. It was determined through coordination with CDOT that it would be best to submit the TIA for CDOT review and then submit access permit applications once CDOT's comments had been addressed.

CDOT's review of the TIA resulted in CDOT suggesting roundabout control for the Access B intersection on US 50 rather than traffic signal control as presented in the TIA and that the two access points would be consistent with, if not identical to, the US 50 Access Control Plan because the applicant is no longer interested in permitting Access C to the east of Access B. The applicant reserves the right to permit Access A and Access D in the future.

A virtual coordination meeting was held with CDOT at which the applicant expressed interest in the roundabout option so CDOT agreed to have their consultant, Kimley-Horn, prepare a conceptual roundabout layout for the applicant to consider. The conceptual layout was provided by CDOT in late August, 2021 and was reviewed positively by the applicant team because a roundabout would calm speeds and could be built with an initial phase and not need a warrant to be met prior to construction as the case would be with traffic signal control. The project team forwarded detailed Survey and CAD files in late September, 2021 to CDOT to further refine the roundabout design. This process is still ongoing. Once a design and cost estimate are available, a roundabout vs. traffic signal decision will be made and the traffic study updated if appropriate and submitted to CDOT with an "Access B" access permit application.

We trust our findings will assist you in your planning efforts for the proposed Gunnison Rising development. Please contact me if you have any questions or need further assistance.

Sincerely,
LSC TRANSPORTATION CONSULTANTS, INC.


Christopher S. McGranahan, PE, PTOE Principal

CSM/wc

$$
11-29-21
$$

Enclosures:

[^0]LSC TRANSPORTATION CONSULTANTS, INC.

1889 York Street
Denver, CO 80206
(303) 333-1105

FAX (303) 333-1107
E-mail: Isc@Iscdenver.com

February 25, 2021
Mr. Richard Bratton
Gunnison Valley Properties, LLC
864 W. South Boulder Road, Suite 200
Louisville, CO 80027

Re: Gunnison Rising<br>Access Points A and B<br>Gunnison, CO<br>LSC \#210040

Dear Mr. Bratton:
In response to your request, LSC Transportation Consultants, Inc. has prepared this traffic impact analysis (CDOT Level III traffic study) for the proposed Gunnison Rising Access Points A and B. As shown on Figure 1, the site is located north and south of US Highway (US) 50 on the far east end of Gunnison, Colorado.

## REPORT CONTENTS

The report contains the following: the existing roadway and traffic conditions in the vicinity of the site including the lane geometries, traffic controls, etc.; the existing weekday peak-hour traffic volumes; the existing daily traffic volumes in the area; an adjustment of the traffic volumes for the ongoing pandemic; the typical weekday site-generated traffic volume projections for the site; the short-term and long-term assignment of the projected traffic volumes to the area roadways; the projected short-term and long-term background and resulting total traffic volumes on the area roadways; the site's projected traffic impacts; and any recommended roadway improvements to mitigate the site's traffic impacts. The scope of work is consistent with the attached TIS Methodology Form.

## LAND USE AND ACCESS

The Access Points A and B site is proposed to include about 168 single-family dwelling units, about 72 townhome dwelling units, about 176 apartment dwelling units, about 9,500 square feet of retail space, about 4,000 square feet of restaurant space, about a 1,000 square-foot single-tenant office building, a 1,500 square-foot drinking place, a 200 square-foot coffee shop, and a 2,000 square-foot day care center.

Access is proposed to US 50 in two locations as shown in the site plan in Figure 2. The western access (Access A) will be three-quarter to the north by 2030 and right-in/right-out to the south
by 2041. The eastern access (Access B) will be full movement by 2030 and signalized once traffic signal warrants are met.

## ROADWAY AND TRAFFIC CONDITIONS

## Area Roadways

The major roadways in the site's vicinity are shown on Figure 1 and are described below.

- US Highway 50 (US 50) is an east-west, two-lane US highway adjacent to the site. It is designated R-A (Regional Highway) by CDOT per the attached CDOT Straight Line Diagram. The intersection with Adams Street is stop-sign controlled and shown as a full movement intersection in the US 50 Access Control Plan (ACP). An excerpt from the ACP is attached for reference. The posted speed limit in the vicinity of the site is 65 mph .
- Adams Street is a north-south, two-lane local roadway west of the site. The intersection with US 50 is stop-sign controlled. No speed limit is posted in the vicinity of the site.
- College Avenue is an east-west, two-lane local roadway west of the site. The intersection with Adams Street is stop-sign controlled. No speed limit is posted in the vicinity of the site.


## Existing Sight Distance

There is good sight distance in each direction of US 50 from the proposed access locations.

## Existing Traffic Conditions

Figure 3a shows the existing January 2021 weekday traffic volumes, existing lane geometry and the existing traffic controls in the vicinity of the site. The weekday peak-hour traffic volumes and average daily traffic volumes are from the attached traffic counts conducted by Counter Measures in January, 2021.

## Pandemic Adjustment

Figure 3 b shows the estimated July traffic volumes adjusted for the ongoing pandemic. These volumes are consistent with the existing July traffic volumes in the attached Figure 3b of the Gunnison Rising Government Campus Subdivision TIA by LSC.

## 2030 and 2041 Background Traffic

Figure 4 shows the estimated 2030 background traffic which assumes an annual growth rate of 0.2 percent based on the CDOT 20-year factor of 1.04 plus other areas of Gunnison Rising expected to be developed by 2030.

Figure 5 shows the estimated 2041 background traffic which assumes an annual growth rate of 0.2 percent based on the CDOT 20-year factor of 1.04 plus development of the balance of

Gunnison Rising planned through 2041. It also assumes half of the school trips are internal to the north side of US 50 .

## Existing, 2030, and 2041 Background Levels of Service

Level of service (LOS) is a quantitative measure of the level of congestion or delay at an intersection. Level of service is indicated on a scale from "A" to "F." LOS A is indicative of little congestion or delay and LOS F is indicative of a high level of congestion or delay. Attached are specific level of service definitions for signalized and unsignalized intersections.

The intersections in the study area were analyzed to determine the existing, 2030, and 2041 background levels of service using Synchro. Table 1 shows the level of service analysis results. The level of service reports are attached.

- Adams Street/College Avenue: All movements at this unsignalized intersection currently operate at LOS "A" during both morning and afternoon peak-hours and are expected to do so through 2041.
- US 50/Adams Street: All movements at this unsignalized intersection currently operate at LOS "C" or better during both morning and afternoon peak-hours and are expected to do so through 2030. By 2041, all movements are expected to operate at LOS "D" or better with the following exception: The northbound approach is expected to operate at LOS "E" in the afternoon peak-hour.
- US 50/West Site Access (Access A): All movements at this stop-sign controlled intersection are expected to operate at LOS "B" or better during both peak-hours through 2041.
- US 50/East Site Access (Access B): All movements at this stop-sign controlled intersection are expected to operate at LOS "C" or better during both peak-hours through 2030. By 2041 several movements are expected to operate at LOS "E" or "F" during both peakhours with stop-sign control.


## TRIP GENERATION

Tables 2 a and 2 b show the estimated average daily, weekday morning peak-hour, and weekday afternoon peak-hour trip generation potential for the proposed site through both 2030 and 2041 based on the rates from Trip Generation, $10^{\text {th }}$ Edition, 2017 by the Institute of Transportation Engineers (ITE).

At buildout the site is projected to generate about 4,389 external vehicle-trips on the average weekday, with about half entering and half exiting during a 24 -hour period. During the morning peak-hour, which generally occurs for one hour between 6:30 and 8:30 a.m., about 91 vehicles would enter and about 207 vehicles would exit the site. During the afternoon peakhour, which generally occurs for one hour between 4:00 and 6:00 p.m., about 256 vehicles would enter and about 164 vehicles would exit. These volumes will be reduced by internal trips. The Access Points A and B site land uses are shaded in Tables 2a and 2b. The balance of the land uses in Tables 2a and 2 b are the background traffic expected from the balance of Gunnison Rising through both 2030 (Table 2a) and 2041 (Table 2b).

These estimates include an internal trip rate of two percent for the AM peak-hour traffic, five percent for the daily traffic, and eight percent for the PM peak-hour traffic.

## TRIP DISTRIBUTION

Figure 6 shows the estimated directional distribution of the site-generated traffic volumes on the area roadways. The estimates were based on the location of the site with respect to the regional population, employment, and activity centers; the site's proposed land use; and on the attached TIS methodology form.

## TRIP ASSIGNMENT

Figure 7 shows the assignment of site-generated traffic volumes for the site based on the directional distribution percentages (from Figure 6) and the shaded line items in the trip generation estimate (from Tables 2a or 2 b ).

## 2030 AND 2041 TOTAL TRAFFIC

Figure 8 shows the 2030 total traffic which is the sum of the 2030 background traffic volumes (from Figure 4) and the site-generated traffic volumes (from Figure 7). Figure 8 also shows the recommended 2030 lane geometry and traffic control.

Figure 9 shows the 2041 total traffic which is the sum of the 2041 background traffic volumes (from Figure 5) and the site-generated traffic volumes (from Figure 7). Figure 9 also shows the recommended 2041 lane geometry and traffic control.

## PROJECTED LEVELS OF SERVICE

The intersections in the study area were analyzed as appropriate to determine the 2030 and 2041 total levels of service. Table 1 shows the level of service analysis results. The level of service reports are attached.

- Adams Street/College Avenue: All movements at this stop-sign controlled intersection are expected to operate at LOS "A" during both peak-hours through 2041.
- US 50/Adams Street: All movements at this stop-sign controlled intersection are expected to operate at LOS "D" or better during both peak-hours through 2030. By 2041, the northbound and southbound approaches are expected to operate at LOS "E" or "F" in both peak-hours. As a signalized intersection it is expected to operate at an overall LOS "A" during both peak-hours.
- US 50/West Site Access (Access A): All movements at this stop-sign controlled intersection are expected to operate at LOS "C" or better during both peak-hours through 2041.
- US 50/East Site Access (Access B): All movements at this stop-sign controlled intersection are expected to operate at LOS "D" or better during both peak-hours through 2030 with the following exception: The northbound left-turn movement is expected to operate at LOS "E" in the afternoon peak-hour with stop-sign control. By 2041, both the north-
bound left and southbound left-turn movements are expected to operate at LOS "E" or "F" during both peak-hours. As a signalized intersection it is expected to operate at LOS "A" during the morning peak-hour and LOS "B" during the afternoon peak-hour.


## CONCLUSIONS AND RECOMMENDATIONS

## Trip Generation

1. The site is projected to generate about 4,389 external vehicle-trips on the average weekday, with about half entering and half exiting during a 24 -hour period. During the morning peak-hour, about 91 vehicles would enter and about 207 vehicles would exit the site. During the afternoon peak-hour, about 256 vehicles would enter and about 164 vehicles would exit.
2. The trip generation estimates will be reduced by an internal trip rate of two percent for the AM peak-hour traffic, five percent for the daily traffic, and eight percent for the PM peakhour traffic.

## Projected Levels of Service

3. All movements at the unsignalized Adams Street/College Avenue and US 50/West Site Access (Access A) intersections are expected to operate at LOS "C" or better through 2041.
4. A few side road movements at the US 50/Adams Street and US 50/East Site Access (Access B) intersections are expected to operate at LOS "E" or "F" by 2041. If signalized these intersections are expected to operate at an overall LOS "B" or better.

## Conclusions

5. The impact of the Gunnison Rising Access Points A and B can be accommodated by the existing and proposed roadway network with the recommended improvements.

## Recommendations

6. The recommended improvements are shown in Figure 8.
7. The US 50/Eastern Site Access (Access B) intersection should be signalized once traffic signal warrants are met.

We trust our findings will assist you in gaining approval of the proposed Gunnison Rising Access Points A and B development. Please contact me if you have any questions or need further assistance.

## Sincerely,

LSC TRANSPORTATION CONSULTANTS, INC.


Christopher S. McGranahan, PE, PTOE Principal

CSM/wc

$$
2-25-21
$$

Enclosures: Tables 1 through 2b
Figures 1-9
TIS Methodology Form
CDOT Straight Line Diagram
CDOT US 50 Access Control Plan Excerpt
Traffic Count Reports
Level of Service Definitions
Level of Service Reports
W: \LSC $\backslash$ Projects $\backslash 2021 \backslash 210040$-GunnisonRisingPhase2 $\backslash$ Report \GunnisonRising-AccessPointsA\&B-022521.wpd

| Intersection Location | Traffic Control | Table 1 <br> Intersection Levels of Service Analysis Gunnison Rising Access A and B Gunnison, CO LSC \#210040; February, 2021 |  |  |  |  |  | $2041$ <br> Background Traffic |  | $\begin{gathered} 2041 \\ \text { Total Traffic } \\ \hline \end{gathered}$ |  | 2041 Total TrafficMitigated |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Existing Traffic |  | 2030Background Traffic |  | $\begin{gathered} 2030 \\ \text { Total Traffic } \\ \hline \end{gathered}$ |  |  |  |  |  |  |  |
|  |  | Level of Service AM | Level of <br> Service PM | Level of <br> Service AM | Level of Service PM | Level of <br> Service AM | Level of Service PM | Level of <br> Service AM | Level of Service PM | Level of Service AM | Level of Service PM | Level of Service AM | Level of Service PM |
| Adams Street/College Avenue | TWSC |  |  |  |  |  |  |  |  |  |  |  |  |
| WB Approach |  | A | A | A | A | A | A | A | A | A | A |  |  |
| SB Left/Through |  | A | A | A | A | A | A | A | A | A | A |  |  |
| Critical Movement Delay |  | 9.0 | 9.0 | 9.0 | 9.0 | 9.1 | 9.3 | 9.1 | 9.3 | 9.2 | 9.4 |  |  |
| E. Tomichi Avenue (US 50)/Adams Street | TWSC |  |  |  |  |  |  |  |  |  |  |  |  |
| NB Approach |  | B | c | C | c | c | D | D | E | E | F |  |  |
| EB Left |  | A | A | A | A | A | A | A | A | B | B |  |  |
| WB Left |  | A | A | A | A | A | A | A | A | A | B |  |  |
| SB Approach |  | B | B | B | c | c | C | D | D | E | F |  |  |
| Critical Movement Delay |  | 13.1 | 15.7 | 16.0 | 18.1 | 21.2 | 29.4 | 29.8 | 42.6 | 47.8 | 99.2 |  |  |
|  | Signalized |  |  |  |  |  |  |  |  |  |  |  |  |
| EB Left |  |  |  |  |  |  |  |  |  |  |  | A | A |
| EB Through/Right |  |  |  |  |  |  |  |  |  |  |  | A | A |
| WB Left |  |  |  |  |  |  |  |  |  |  |  | A | A |
| WB Through/Right |  |  |  |  |  |  |  |  |  |  |  | A | A |
| NB Approach |  |  |  |  |  |  |  |  |  |  |  | C | C |
| SB Approach |  |  |  |  |  |  |  |  |  |  |  | c | c |
| Entire Intersection Delay (sec./veh.) |  |  |  |  |  |  |  |  |  |  |  | 5.0 | 7.2 |
| Entire Intersection LOS |  |  |  |  |  |  |  |  |  |  |  | A | A |
| E. Tomichi Avenue (US 50)/West Site Access | TWSC |  |  |  |  |  |  |  |  |  |  |  |  |
| NB Right |  | -- | -- | -- | -- | -- | -- | A | B | A | c |  |  |
| EB Left |  | -- | -- | -- | -- | A | A | -- | -- | A | B |  |  |
| SB Right |  | -- | -- | -- | -- | A | A | -- | -- | A | A |  |  |
| Critical Movement Delay |  | -- | -- | -- | -- | 8.5 | 9.1 | 0.0 | 13.8 | 9.9 | 15.5 |  |  |
| E. Tomichi Avenue (US 50)/East Site Access | TWSC |  |  |  |  |  |  |  |  |  |  |  |  |
| NB Left |  | -- | -- | c | c | c | E | F | F | F | F |  |  |
| NB Through/Right or Right |  | -- | -- | B | B | B | c | C | c | C | E |  |  |
| EB Left |  | -- | -- | -- | -- | A | A | A | A | A | A |  |  |
| WB Left |  | -- | -- | A | A | A | A | A | A | A | A |  |  |
| SB Left |  | -- | -- | -- | -- | c | D | D | E | E | F |  |  |
| SB Through/Right |  | -- | -- | -- | $\stackrel{--}{-7}$ | B | B | B | B | C | C |  |  |
| Critical Movement Delay |  | -- | -- | 15.2 | 17.7 | 23.7 | 44.1 | 51.2 | >240 | 114.4 | >240 |  |  |
|  | Signalized |  |  |  |  |  |  |  |  |  |  |  |  |
| EB Left |  |  |  |  |  |  |  |  |  |  |  | A | A |
| EB Through |  |  |  |  |  |  |  |  |  |  |  | A | A |
| EB Right |  |  |  |  |  |  |  |  |  |  |  | A | A |
| WB Left |  |  |  |  |  |  |  |  |  |  |  | A | A |
| WB Through |  |  |  |  |  |  |  |  |  |  |  | A | B |
| WB Right |  |  |  |  |  |  |  |  |  |  |  | A | A |
| NB Left |  |  |  |  |  |  |  |  |  |  |  | D | D |
| NB Through/Right |  |  |  |  |  |  |  |  |  |  |  | C | c |
| SB Left |  |  |  |  |  |  |  |  |  |  |  | D | c |
| SB Through/Right |  |  |  |  |  |  |  |  |  |  |  | B | A |
| Entire Intersection Delay (sec./veh.) |  |  |  |  |  |  |  |  |  |  |  | 9.7 | 12.7 |
| Entire Intersection LOS |  |  |  |  |  |  |  |  |  |  |  | A | B |



TND NORTH OF US HIGHWAY 50 - The shaded areas are the "Site" and all others are background traffic.

| 2021-2025 ACCESS A, B, COLLEGE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 2 Single-Family Detached ${ }^{(2)}$ | $84 \mathrm{DU}^{(3)}$ | 9.44 | 0.185 | 0.555 | 0.624 | 0.366 | 793 | 16 | 47 | 52 | 31 |
| 2 Townhomes ${ }^{(4)}$ | 36 DU | 7.32 | 0.106 | 0.354 | 0.353 | 0.207 | 264 | 4 | 13 | 13 | 7 |
| 2 Apartments ${ }^{(4)}$ | 64 DU | 7.32 | 0.106 | 0.354 | 0.353 | 0.207 | 468 | 7 | 23 | 23 | 13 |
| 2 Drinking Place ${ }^{(5)}$ | $1.5 \mathrm{KSF}^{(6)}$ | 56.80 | 0.000 | 0.000 | 7.498 | 3.862 | 85 | 0 | 0 | 11 | 6 |
| 2 Coffee/Donut Shop ${ }^{(7)}$ | 0.2 KSF | 505.70 | 51.581 | 49.559 | 18.155 | 18.155 | 101 | 10 | 10 | 4 | 4 |
| 2 Retail ${ }^{(8)}$ | 3.5 KSF | 37.75 | 0.583 | 0.357 | 1.829 | 1.981 | 132 | 2 | 1 | 6 | 7 |
| 2 Restaurant ${ }^{(9)}$ | 2.5 KSF | 83.84 | 0.489 | 0.241 | 5.226 | 2.574 | 210 | 1 | 1 | 13 | 6 |
|  |  |  |  | Sub | Total Ph | hase 2 = | 2,053 | 40 | 95 | 122 | 74 |
| 2026-2030 ACCESS A, B, COLLEGE, GEORGIA |  |  |  |  |  |  |  |  |  |  |  |
| 3 Single-Family Detached | 84 DU | 9.44 | 0.185 | 0.555 | 0.624 | 0.366 | 793 | 16 | 47 | 52 | 31 |
| 3 Townhomes | 36 DU | 7.32 | 0.106 | 0.354 | 0.353 | 0.207 | 264 | 4 | 13 | 13 | 7 |
| 3 Apartments | 112 DU | 7.32 | 0.106 | 0.354 | 0.353 | 0.207 | 820 | 12 | 40 | 40 | 23 |
| 3 Day Care Center ${ }^{(10)}$ | 2 KSF | 47.62 | 5.830 | 5.170 | 5.226 | 5.894 | 95 | 12 | 10 | 10 | 12 |
| 3 Restaurant | 1.5 KSF | 83.84 | 0.489 | 0.241 | 5.226 | 2.574 | 126 | 1 | 0 | 8 | 4 |
| 3 Retail | 1 KSF | 37.75 | 0.583 | 0.357 | 1.829 | 1.981 | 38 | 1 | 0 | 2 | 2 |
|  |  |  |  | Sub | Total Ph | hase 3 = | 2,136 | 46 | 110 | 125 | 79 |
| PHASES 6-10 2041 AND BEYOND |  |  |  |  |  |  |  |  |  |  |  |
|  | Total Trips | North of | US High | way 50 | Through | $2030=$ | 4,189 | 86 | 205 | 247 | 153 |

MAKER DISTRICT SOUTH OF US HIGHWAY 50 - The shaded areas are the "Site" and all others are background traffic.

| 2021-2025 ACCESS E |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Government Office Building ${ }^{(13)}$ | 36 KSF | 22.59 | 2.505 | 0.835 | 0.428 | 1.283 | 813 | 90 | 30 | 15 | 46 |
| 1 | General Light Industrial ${ }^{(14)}$ | 16 KSF | 4.96 | 0.616 | 0.084 | 0.082 | 0.548 | 79 | 10 | 1 | 1 | 9 |
| 3 | RV Park ${ }^{(15)}$ | 150 Units | 1.35 | 0.076 | 0.134 | 0.176 | 0.095 | 203 | 11 | 20 | 26 | 14 |
| Sub-Total Phase 1 = |  |  |  |  |  |  |  | 1,095 | 111 | 51 | 42 | 69 |
| 2021-2025 B, CR 49 |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | Retail | 5 KSF | 37.75 | 0.583 | 0.357 | 1.829 | 1.981 | 189 | 3 | 2 | 9 | 10 |
| 2 | Single-Tenant Office ${ }^{(16)}$ | 1 KSF | 11.25 | 1.584 | 0.196 | 0.257 | 1.454 | 11 | 2 | 0 | 0 | 1 |
| Sub-Total Phase 2 = |  |  |  |  |  |  |  | 200 | 5 | 2 | 9 | 11 |
| 2026-2 | ACCESS E |  |  |  |  |  |  |  |  |  |  |  |
| 1 | Government Office Building | 8 KSF | 22.59 | 2.505 | 0.835 | 0.428 | 1.283 | 181 | 20 | 7 | 3 | 10 |
| 1 | General Light Industrial | 20 KSF | 4.96 | 0.616 | 0.084 | 0.082 | 0.548 | 99 | 12 | 2 | 2 | 11 |
| 3 | RV Park | 150 Units | 1.35 | 0.076 | 0.134 | 0.176 | 0.095 | 203 | 11 | 20 | 26 | 14 |
| Sub-Total Phase 3 = |  |  |  |  |  |  |  | 483 | 43 | 29 | 31 | 35 |
| 2026-2030 ACCESS A, B, CR 49 |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | Single-Tenant Office | 2 KSF | 11.25 | 1.584 | 0.196 | 0.257 | 1.454 | 23 | 3 | 0 | 1 | 3 |
| 4 | Research \& Development ${ }^{(17)}$ | 3 KSF | 11.26 | 0.315 | 0.105 | 0.074 | 0.417 | 34 | 1 | 0 | 0 | 1 |
| 4 | Building Materials ${ }^{(18)}$ | 20 KSF | 18.05 | 0.989 | 0.581 | 0.968 | 1.092 | 361 | 20 | 12 | 19 | 22 |
| 4 | Single-Tenant Office | 4 KSF | 11.25 | 1.584 | 0.196 | 0.257 | 1.454 | 45 | 6 | 1 | 1 | 6 |
| 4 | Nursery Garden Center ${ }^{(19)}$ | 1.5 KSF | 68.1 | 1.215 | 1.215 | 3.470 | 3.470 | 102 | 2 | 2 | 5 | 5 |
| 4 | Quick Lube Shop ${ }^{(20)}$ | 1.5 KSF | 69.57 | 4.350 | 1.450 | 3.654 | 5.046 | 104 | 7 | 2 | 5 | 8 |
| 4 | General Light Industrial | 3 KSF | 4.96 | 0.616 | 0.084 | 0.082 | 0.548 | 15 | 2 | 0 | 0 | 2 |
| 4 | Mini-Warehouse ${ }^{(21)}$ | 5 KSF | 1.51 | 0.060 | 0.040 | 0.080 | 0.090 | 8 | 0 | 0 | 0 | 0 |
|  |  |  |  |  | Sub | Total Ph | ase 4 = | 692 | 41 | 17 | 31 | 47 |
| Total Trips Maker District South of US Highway 50 Through $2030=$ |  |  |  |  |  |  |  | 2,470 | 200 | 99 | 113 | 162 |
| Total Trips Through $2041=$ |  |  |  |  |  |  |  | 6,659 | 286 | 304 | 360 | 315 |
| Internal Trips (25) = |  |  |  |  |  |  |  | 333 | 6 | 6 | 29 | 25 |
| Net External Trips = |  |  |  |  |  |  |  | 6,326 | 280 | 298 | 331 | 290 |
| Notes: |  |  |  |  |  |  |  |  |  |  |  |  |
| (1) Source: Trip Generation, Institute of Transportation Engineers, 10th Edition, 2017. |  |  |  |  |  |  |  |  |  |  |  |  |
| (2) ITE Land Use No. 210 - Single-Family Detached Housing |  |  |  |  |  |  |  |  |  |  |  |  |
| (3) DU = Dwelling Unit |  |  |  |  |  |  |  |  |  |  |  |  |
| (4) ITE Land Use No. 220 - Multifamily Housing (Low-Rise) |  |  |  |  |  |  |  |  |  |  |  |  |
| (5) ITE Land Use No. 925 - Drinking Place - daily rates assumed to be 5x PM peak hour rate - closed in the morning |  |  |  |  |  |  |  |  |  |  |  |  |
| (6) $\mathrm{KSF}=1,000$ square feet |  |  |  |  |  |  |  |  |  |  |  |  |
| (7) ITE Land Use No. 936 - Coffee/Donut Shop without drive-through - Daily rate assumed to be 5x AM peak hour rate |  |  |  |  |  |  |  |  |  |  |  |  |
| (8) ITE Land Use No. 820 - Shopping Center |  |  |  |  |  |  |  |  |  |  |  |  |
| (9) ITE Land Use No. 931 - Quality Restaurant - PM peak distribution used for AM peak as well |  |  |  |  |  |  |  |  |  |  |  |  |
| (10) ITE Land Use No. 565 - Day Care Center |  |  |  |  |  |  |  |  |  |  |  |  |
| (11) Intentionally left blank |  |  |  |  |  |  |  |  |  |  |  |  |
| (12) Intentionally left blank |  |  |  |  |  |  |  |  |  |  |  |  |
| (13) ITE Land Use No. 730 - Government Office Building |  |  |  |  |  |  |  |  |  |  |  |  |
| (14) ITE Land Use No. 110 - General Light Industrial |  |  |  |  |  |  |  |  |  |  |  |  |
| (15) ITE Land Use No. 416 - Campground/Recreational Vehicle Park: no weekday rate so 5x PM Peak Rate was used |  |  |  |  |  |  |  |  |  |  |  |  |
| (16) ITE Land Use No. 715 - Single Tenant Office Building |  |  |  |  |  |  |  |  |  |  |  |  |
| (17) ITE Land Use No. 760 - Research \& Development Center |  |  |  |  |  |  |  |  |  |  |  |  |
| (18) ITE Land Use No. 812 - Building Materials \& Lumber Store |  |  |  |  |  |  |  |  |  |  |  |  |
| (19) ITE Land Use No. 817 - Nursery (Garden Center) - no AM or PM peak-hour distribution available so 50\% in/out was used |  |  |  |  |  |  |  |  |  |  |  |  |
| (20) ITE Land Use No. 941 - Quick Lubrication Vehicle Shop |  |  |  |  |  |  |  |  |  |  |  |  |
| (21) ITE Land Use No. 151 - Mini-Warehouse |  |  |  |  |  |  |  |  |  |  |  |  |
| (22) Intentionally left blank |  |  |  |  |  |  |  |  |  |  |  |  |
| (23) Intentionally left blank |  |  |  |  |  |  |  |  |  |  |  |  |
| (24) Intentionally left blank |  |  |  |  |  |  |  |  |  |  |  |  |
| (25) Internal trips were assumed to be two percent in the AM peak-hour, five percent for daily, and eight percent in the PM peak-hour |  |  |  |  |  |  |  |  |  |  |  |  |













## COLORADO

## Department of Transportation

Region 3

## Transportation Impact Study <br> Methodology Form

Prior to starting a traffic impact study, a Methodology Form must be submitted for review and signed by the Region 3 Access Engineer. It shall be included as part of the study.

CONTACT INFORMATION

| Consultant: | Name: |
| ---: | :--- |
|  | LSC Transportation Consultants, Inc. (Chris McGranahan) |
|  | Telephone: |
| Email $:$ | chris@lsctrans.com and Isc@lscdenver.com |
| Developer/Owner Name: | Gunnison Valley Partners |

## PROJ ECT INFORMATION

| Project Name | Gunnison Rising |
| :--- | :--- |
| Project Location | East of Gunnison, CO on both sides of US 50 |
| Project Description <br> (Attached proposed site plan) | See attached site plan |
| State Highway | US 50 |
| County | Gunnison |
| Mile Post | Between 158 and 159 |
| Posted Speed Limit | 55 mph approaching from east and 65 mph approaching from west |

TIS ASSUMPTIONS

| Study Years | Current Year: 2020 | Buildout Year: 2025 |  | Long Term Year: 2040 |
| :---: | :---: | :---: | :---: | :---: |
| Traffic Assessment Level (Provide justification) | Level 3 Traffic Study |  |  |  |
| Study Intersections | 1. US 50/Adams Street |  | 6. |  |
|  | 2. Adams Street/College Avenue |  | 7. |  |
|  | 3. Proposed Access Point to US 50 |  | 8. |  |
|  | 4. |  | 9. |  |
|  | 5. |  | 10. |  |
| Future Growth Rate | $\square$ OTIS | $\square$ Regional TDM |  | $\square$ Other |
| Seasonal Adjustment Factor | Traffic counts will be modified using both a seasonal and pandemic adjustment. |  |  |  |

COLORADO
Department of Transportation
Region 3
ASSUMPTIONS CONTINUED

| Project Trip Distribution (State assumptions and attach sketch that shows individual movements.) | 95\% West and 5\% East |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| Trip Reduction Percentage | Internal Capture: | Up to that allowed per SHAC | Pass By: | Will be considered based on Trip Generation Handbook |
|  | Multi-Modal: | N/A | Other: |  |
| Study Time Periods <br> (Check all that apply) | $\square \mathrm{\square M}(7-9) \quad \square \mathrm{PM}$ |  | $\square \mathrm{PM}(4-6)$ | $\square$ Weekday |
|  | $\square$ SAT (Midday) | $\square$ Other |  |  |
| Existing and Proposed ITE Trip Generation Land Use | There will be a number of proposed land use types including Single-Family Detached Homes (210), Multi-Family (Low-Rise) (220), Free-Standing Discount Store (815), Retail Shopping (820), Drinking Place (925), Quality Restaurant (931), Coffee Shop (936), Super Convenience Market/Gas Station (960) |  |  |  |
| Analysis Methods (Check all that apply) | $\square$ Synchro or $\quad \square$ HCS(isolated intersections only) |  | SimTraffic or $\square$ Other (closely spaced intersections or when known/ expected queuing issue) |  |
|  | $\square$ Signal Warrants |  | $\square$ Pedestrian/Transit/Bicycle |  |
|  | $\square$ Safety/Sight Distance |  | $\square$ Queuing and Storage |  |
|  | $\square$ Other |  |  |  |
| Notes and Other Assumptions | We would prepare and submit an overall trip generation table for review by CDOT prior to preparing the full traffic study. |  |  |  |
| Crash Data | CDOT will perform a crash data analysis for the highway in the vicinity of the proposed access and provide to the consultant. As a part of the study consultant shall recommend mitigation measures for any identified safety issues. |  |  |  |
| Simulation Input Files | Consultant to provide computer files used for analysis with a signed and sealed copy of the study. |  |  |  |

## CDOT INTERNAL USE ONLY

Review Comments

Revise and Resubmit
Engineer Signature/Date $\square$ Approved

## GUNNISON RISING ANTICIPATED PHASING PLAN



## GUNNISON RISING ANTICIPATED PHASING PLAN



## Route 050A From 158 to 161




It may appear that information is missing from the straight line diagram. If so, reduce the number of miles/page and re-submit the request.




## COUNTER MEASURES INC.

## 1889 YORK STREET <br> DENVER.COLORADO 303-333-7409

N/S STREET: ADAMS STREET
E/W STREET: COLLEGE AVE CITY: GUNNISON
COUNTY: GUNNISON
File Name : ADAMSCOLL
Site Code : 00000017
Start Date : 1/12/2021
Page No : 1
Groups Printed- VEHICLES

|  | ADAMS STREET Southbound |  |  |  | COLLEGE AVENUE Westbound |  |  |  | ADAMS STREET Northbound |  |  |  | Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| 06:45 AM | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 4 |
| Total | 0 | 1 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |


| 07:00 AM | 1 | 1 | 0 | 1 | 1 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 7 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07:15 AM | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 8 |
| 07:30 AM | 1 | 4 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 11 |
| 07:45 AM | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 16 |
| Total | 3 | 8 | 0 | 1 | 1 | 0 | 3 | 0 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 42 |


| 08:00 AM | 1 | 7 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 18 |
| :--- | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $08: 15 \mathrm{AM}$ | 0 | 3 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 14 | 1 | 0 | 0 | 0 | 0 | 0 | 22 |

$\begin{array}{lllllllllllllllllllllllll}\text { Total } & 1 & 10 & 0 & 0 & 3 & 0 & 3 & 0 & 0 & 22 & 1 & 0 & 0 & 0 & 0 & 0 & 40\end{array}$

| 04:00 PM | 2 | 10 | 0 | 1 | 0 | 0 | 1 | 0 | 0 | 10 | 1 | 0 | 0 | 0 | 0 | 0 | 25 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 04:15 PM | 0 | 13 | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 24 |
| 04:30 PM | 1 | 14 | 0 | 2 | 0 | 0 | 1 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 30 |
| 04:45 PM | 1 | 15 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 17 | 1 | 0 | 0 | 0 | 0 | 0 | 36 |
| Total | 4 | 52 | 0 | 3 | 1 | 0 | 5 | 0 | 0 | 48 | 2 | 0 | 0 | 0 | 0 | 0 | 115 |


| 05:00 PM | 1 | 19 | 0 | 0 | 2 | 0 | 3 | 0 | 0 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 31 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 05:15 PM | 1 | 12 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 24 |
| 05:30 PM | 3 | 9 | 0 | 0 | 2 | 0 | 1 | 0 | 0 | 8 | 1 | 0 | 0 | 0 | 0 | 0 | 24 |
| 05:45 PM | 3 | 8 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 18 |
| Total | 8 | 48 | 0 | 0 | 5 | 0 | 5 | 0 | 0 | 28 | 3 | 0 | 0 | 0 | 0 | 0 | 97 |


| Grand Total | 16 | 119 | 0 | 4 | 10 | 0 | 18 | 0 | 0 | 132 | 6 | 0 | 0 | 0 | 0 | 0 | 305 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Apprch \% | 11.5 | 85.6 | 0.0 | 2.9 | 35.7 | 0.0 | 64.3 | 0.0 | 0.0 | 95.7 | 4.3 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total \% | 5.2 | 39.0 | 0.0 | 1.3 | 3.3 | 0.0 | 5.9 | 0.0 | 0.0 | 43.3 | 2.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |

## COUNTER MEASURES INC.

1889 YORK STREET
N/S STREET: ADAMS STREET
DENVER.COLORADO
File Name : ADAMSCOLL
E/W STREET: COLLEGE AVE 303-333-7409

Site Code : 00000017
Start Date: 1/12/2021 Page No : 2

|  | ADAMS STREET Southbound |  |  |  |  | COLLEGE AVENUE <br> Westbound |  |  |  |  | ADAMS STREET Northbound |  |  |  |  | Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | $\begin{array}{r} \hline \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | $\begin{array}{r\|} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{gathered} \text { Thr } \\ \mathrm{u} \end{gathered}$ | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | $\begin{array}{r\|} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |

Peak Hour From 07:30 AM to 08:15 AM - Peak 1 of 1



## COUNTER MEASURES INC.

1889 YORK STREET
N/S STREET: ADAMS STREET
DENVER.COLORADO
File Name : ADAMSCOLL 303-333-7409

Site Code : 00000017
Start Date: 1/12/2021
Page No : 2

|  | ADAMS STREET Southbound |  |  |  |  | COLLEGE AVENUE <br> Westbound |  |  |  |  | ADAMS STREET Northbound |  |  |  |  | Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \\ \hline \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \\ \hline \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | Thr $u$ | $\begin{gathered} \mathrm{Rig} \\ \mathrm{ht} \\ \hline \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \hline \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | Ped $s$ | App. Total | Int. Total |

Peak Hour From 04:30 PM to 05:15 PM - Peak 1 of 1



## COUNTER MEASURES INC.

```
1889 YORK STREET
DENVER.COLORADO
```

File Name: ADAMSUS50
Site Code : 00000015
Start Date : 1/11/2021 Page No : 1
Groups Printed- VEHICLES

|  | ADAMS STREET Southbound |  |  |  | EAST TOMICHI AVE (US <br> 50) <br> Westbound |  |  |  | ADAMS STREET Northbound |  |  |  | EAST TOMICHI AVE (US <br> 50) <br> Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 1 | 0 | 1 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 12 | 0 | 0 | 31 |
| 06:45 AM | 0 | 0 | 2 | 0 | 0 | 15 | 2 | 0 | 0 | 0 | 0 | 0 | 7 | 9 | 0 | 0 | 35 |
| Total | 1 | 0 | 3 | 0 | 0 | 28 | 2 | 0 | 0 | 0 | 0 | 0 | 11 | 21 | 0 | 0 | 66 |
| 07:00 AM | 2 | 0 | 3 | 0 | 0 | 19 | 7 | 0 | 0 | 0 | 0 | 0 | 3 | 11 | 0 | 0 | 45 |
| 07:15 AM | 0 | 1 | 7 | 0 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 16 | 0 | 0 | 59 |
| 07:30 AM | 0 | 0 | 6 | 0 | 0 | 22 | 3 | 0 | 0 | 0 | 0 | 0 | 9 | 19 | 0 | 0 | 59 |
| 07:45 AM | 0 | 0 | 9 | 0 | 0 | 42 | 3 | 0 | 0 | 0 | 0 | 0 | 14 | 17 | 3 | 0 | 88 |
| Total | 2 | 1 | 25 | 0 | 0 | 109 | 13 | 0 | 0 | 0 | 0 | 0 | 35 | 63 | 3 | 0 | 251 |
| 08:00 AM | 4 | 1 | 5 | 0 | 0 | 26 | 3 | 0 | 0 | 0 | 0 | 0 | 15 | 21 | 0 | 0 | 75 |
| 08:15 AM | 3 | 0 | 8 | 0 | 0 | 17 | 5 | 0 | 0 | 0 | 0 | 0 | 14 | 22 | 0 | 0 | 69 |
| Total | 7 | 1 | 13 | 0 | 0 | 43 | 8 | 0 | 0 | 0 | 0 | 0 | 29 | 43 | 0 | 0 | 144 |


| 04:00 PM | 4 | 1 | 20 | 0 | 0 | 29 | 2 | 0 | 0 | 2 | 0 | 0 | 12 | 31 | 1 | 0 | 102 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $04: 15 \mathrm{PM}$ | 3 | 0 | 16 | 0 | 0 | 20 | 0 | 0 | 1 | 0 | 0 | 2 | 8 | 27 | 1 | 0 | 78 |
| $04: 30 \mathrm{PM}$ | 4 | 0 | 17 | 0 | 0 | 38 | 1 | 0 | 4 | 1 | 0 | 0 | 10 | 36 | 1 | 0 | 112 |
| $04: 45 \mathrm{PM}$ | 4 | 0 | 17 | 0 | 0 | 27 | 2 | 0 | 0 | 0 | 0 | 0 | 8 | 32 | 4 | 0 | 94 |
| Total | 15 | 1 | 70 | 0 | 0 | 114 | 5 | 0 | 5 | 3 | 0 | 2 | 38 | 126 | 7 | 0 | 386 |


| 05:00 PM | 5 | 0 | 13 | 1 | 0 | 34 | 3 | 0 | 0 | 0 | 0 | 0 | 9 | 40 | 0 | 0 | 105 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $05: 15 ~ P M ~$ | 5 | 1 | 12 | 0 | 0 | 34 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 41 | 0 | 0 | 109 |
| $05: 30 ~ P M ~$ | 6 | 0 | 10 | 0 | 1 | 29 | 2 | 0 | 0 | 0 | 0 | 0 | 12 | 38 | 0 | 0 | 98 |
| 05:45 PM | 2 | 0 | 7 | 0 | 0 | 23 | 2 | 0 | 0 | 0 | 0 | 0 | 10 | 25 | 0 | 0 | 69 |
| Total | 18 | 1 | 42 | 1 | 1 | 120 | 7 | 0 | 0 | 0 | 0 | 0 | 47 | 144 | 0 | 0 | 381 |
| Grand Total | 43 | 4 | 153 | 1 | 1 | 414 | 35 | 0 | 5 | 3 | 0 | 2 | 160 | 397 | 10 | 0 | 1228 |
| Apprch \% | 21.4 | 2.0 | 76.1 | 0.5 | 0.2 | 92.0 | 7.8 | 0.0 | 50.0 | 30.0 | 0.0 | 20.0 | 28.2 | 70.0 | 1.8 | 0.0 |  |
| Total \% | 3.5 | 0.3 | 12.5 | 0.1 | 0.1 | 33.7 | 2.9 | 0.0 | 0.4 | 0.2 | 0.0 | 0.2 | 13.0 | 32.3 | 0.8 | 0.0 |  |

## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO
File Name : ADAMSUS50
303-333-7409
Site Code : 00000015
Start Date: 1/11/2021
Page No : 2

N/S STREET: ADAMS STREET
E/W STREET: EAST TOMICHI AVE (US 50)
CITY: GUNNISON
COUNTY: GUNNISON

|  | ADAMS STREET Southbound |  |  |  |  | EAST TOMICHI AVE (US 50) Westbound |  |  |  |  | ADAMS STREET <br> Northbound |  |  |  |  | EAST TOMICHI AVE (US 50) Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r\|} \hline \text { Ped } \\ \mathrm{s} \\ \hline \end{array}$ | App. <br> Total | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \text { ht } \end{array}$ | Ped s | App. <br> Total | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |

Peak Hour From 06:30 AM to 08:15 AM - Peak 1 of 1


## COUNTER MEASURES INC.

1889 YORK STREET
DENVER.COLORADO
File Name : ADAMSUS50
303-333-7409
Site Code : 00000015
Start Date: 1/11/2021
Page No : 2

N/S STREET: ADAMS STREET
E/W STREET: EAST TOMICHI AVE (US 50)
CITY: GUNNISON
COUNTY: GUNNISON

|  | ADAMS STREET Southbound |  |  |  |  | EAST TOMICHI AVE (US <br> 50) <br> Westbound |  |  |  |  | ADAMS STREET Northbound |  |  |  |  | EAST TOMICHI AVE (US 50) Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r\|} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \mathrm{ht} \end{gathered}$ | Ped | App. Total | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |

Peak Hour From 04:00 PM to 05:45 PM - Peak 1 of 1

| Intersecti on Volume | $04: 30$ 18 | PM | 59 | 1 | 79 | 0 | 133 | 6 | 0 | 139 | 4 | 1 | 0 | 0 | 5 | 43 | 149 | 5 | 0 | 197 | 420 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Percent | $\begin{array}{r} 22 . \\ 8 \end{array}$ | 1.3 | $74 .$ | 1.3 |  | 0.0 | 95 7 | 4.3 | 0.0 |  | 80. | 20. | 0.0 | 0.0 |  | 21. | 75. | 2.5 | 0.0 |  |  |
| 04:30 Volume Peak Factor | 4 | 0 | 17 | 0 | 21 | 0 | 38 | 1 | 0 | 39 | 4 | 1 | 0 | 0 | 5 | 10 | 36 | 1 | 0 | 47 | $\begin{aligned} & 112 \\ & 0.938 \end{aligned}$ |
| High Int. | 04:30 | PM |  |  |  | 04:30 | PM |  |  |  | 04:30 |  |  |  |  | 05:15 | PM |  |  |  |  |
| Volume | 4 | 0 | 17 | 0 | 21 | 0 | 38 | 1 | 0 | 39 | 4 | 1 | 0 | 0 | 5 | 16 | 41 | 0 | 0 | 57 |  |
| Peak Factor |  |  |  |  | 0.94 0 |  |  |  |  | 0.89 1 |  |  |  |  | 0.25 0 |  |  |  |  | 0.86 4 |  |



Location: ADAMS STREET N/O US 50 (TOMICHI AVE) City: GUNNISON County: GUNNISON
Direction: NORTH/SOUTH

COUNTER MEASURES INC.
1889 YORK STREET
DENVER,COLORADO 80206
Site Code: 211103
Station ID: 211103

| Start <br> Time | $\begin{gathered} \text { 12-Jan-21 } \\ \text { Tue } \end{gathered}$ | NORTHBOU | SOUTHBOU |  |  |  |  |  |  | Total |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 12:00 AM |  | 0 | 0 |  |  |  |  |  |  | 0 |
| 01:00 |  | 1 | 0 |  |  |  |  |  |  | 1 |
| 02:00 |  | 1 | 0 |  |  |  |  |  |  | 1 |
| 03:00 |  | 1 | 0 |  |  |  |  |  |  | 1 |
| 04:00 |  | 0 | 0 |  |  |  |  |  |  | 0 |
| 05:00 |  | 1 | 0 |  |  |  |  |  |  | 1 |
| 06:00 |  | 4 | 1 |  |  |  |  |  |  | 5 |
| 07:00 |  | 24 | 1 |  |  |  |  |  |  | 25 |
| 08:00 |  | 37 | 5 |  |  |  |  |  |  | 42 |
| 09:00 |  | 56 | 19 |  |  |  |  |  |  | 75 |
| 10:00 |  | 52 | 34 |  |  |  |  |  |  | 86 |
| 11:00 |  | 39 | 44 |  |  |  |  |  |  | 83 |
| 12:00 PM |  | 60 | 71 |  |  |  |  |  |  | 131 |
| 01:00 |  | 75 | 32 |  |  |  |  |  |  | 107 |
| 02:00 |  | 42 | 37 |  |  |  |  |  |  | 79 |
| 03:00 |  | 40 | 67 |  |  |  |  |  |  | 107 |
| 04:00 |  | 60 | 50 |  |  |  |  |  |  | 110 |
| 05:00 |  | 38 | 49 |  |  |  |  |  |  | 87 |
| 06:00 |  | 27 | 17 |  |  |  |  |  |  | 44 |
| 07:00 |  | 23 | 10 |  |  |  |  |  |  | 33 |
| 08:00 |  | 29 | 7 |  |  |  |  |  |  | 36 |
| 09:00 |  | 10 | 4 |  |  |  |  |  |  | 14 |
| 10:00 |  | 5 | 4 |  |  |  |  |  |  | 9 |
| 11:00 |  | 3 | 0 |  |  |  |  |  |  | 3 |
| Total |  | 628 | 452 |  |  |  |  |  |  | 1080 |
| Percent |  | 58.1\% | 41.9\% |  |  |  |  |  |  |  |
| AM Peak | - | 09:00 | 11:00 | - | - | - | - | - | - | 10:00 |
| Vol. | - | 56 | 44 | - | - | - | - | - | - | 86 |
| PM Peak | - | 13:00 | 12:00 | - | - | - | - | - | - | 12:00 |
| Vol. | - | 75 | 71 | - | - | - | - | - | - | 131 |
| Grand Total |  | 628 | 452 |  |  |  |  |  |  | 1080 |
| Percent |  | 58.1\% | 41.9\% |  |  |  |  |  |  |  |
| ADT |  | ADT 1,080 |  | AADT 1,080 |  |  |  |  |  |  |

## LEVEL OF SERVICE DEFINITIONS

From Highway Capacity Manual, Transportation Research Board, 2016, 6th Edition
SIGNALIZED INTERSECTION LEVEL OF SERVICE (LOS)

| LOS | Average Vehicle Delay sec/vehicle | Operational Characteristics |
| :---: | :---: | :---: |
| A | <10 seconds | Describes operations with low control delay, up to $10 \mathrm{sec} / \mathrm{veh}$. This LOS occurs when progression is extremely favorable and most vehicles arrive during the green phase. Many vehicles do not stop at all. Short cycle lengths may tend to contribute to low delay values. |
| B | 10 to 20 seconds | Describes operations with control delay greater than 10 seconds and up to $20 \mathrm{sec} / \mathrm{veh}$. This level generally occurs with good progression, short cycle lengths, or both. More vehicles stop than with LOS A, causing higher levels of delay. |
| c | 20 to 35 seconds | Describes operations with control delay greater than 20 and up to $35 \mathrm{sec} / \mathrm{veh}$. These higher delays may result from only fair progression, longer cycle length, or both. Individual cycle failures may begin to appear at this level. Cycle failure occurs when a given green phase does not serve queued vehicles, and overflows occur. The number of vehicles stopping is significant at this level, though many still pass through the intersection without stopping. |
| D | 35 to 55 seconds | Describes operations with control delay greater than 35 and up to $55 \mathrm{sec} / \mathrm{veh}$. At LOS D, the influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, and high v/c ratios. Many vehicles stop, and the proportion of vehicles not stopping declines. Individual cycle failures are noticeable. |
| E | 55 to 80 seconds | Describes operations with control delay greater than 55 and up to 80 sec/veh. These high delay values generally indicate poor progression, long cycle lengths, and high v/c ratios. Individual cycle failures are frequent. |
| F | $\begin{gathered} >80 \\ \text { seconds } \end{gathered}$ | Describes operations with control delay in excess of 80 sec/veh. This level, considered unacceptable to most drivers, often occurs with over-saturation, that is, when arrival flow rates exceed the capacity of lane groups. It may also occur at high $\mathrm{v} / \mathrm{c}$ ratios with many individual cycle failures. Poor progression and long cycle lengths may also contribute significantly to high delay levels. |

## LEVEL OF SERVICE DEFINITIONS

From Highway Capacity Manual, Transportation Research Board, 2016, 6th Edition
UNSIGNALIZED INTERSECTION LEVEL OF SERVICE (LOS)
Applicable to Two-Way Stop Control, All-Way Stop Control, and Roundabouts

| LOS | Average Vehicle Control Delay | Operational Characteristics |
| :---: | :---: | :---: |
| A | <10 seconds | Normally, vehicles on the stop-controlled approach only have to wait up to 10 seconds before being able to clear the intersection. Left-turning vehicles on the uncontrolled street do not have to wait to make their turn. |
| B | 10 to 15 seconds | Vehicles on the stop-controlled approach will experience delays before being able to clear the intersection. The delay could be up to 15 seconds. Left-turning vehicles on the uncontrolled street may have to wait to make their turn. |
| C | 15 to 25 seconds | Vehicles on the stop-controlled approach can expect delays in the range of 15 to 25 seconds before clearing the intersection. Motorists may begin to take chances due to the long delays, thereby posing a safety risk to through traffic. Left-turning vehicles on the uncontrolled street will now be required to wait to make their turn causing a queue to be created in the turn lane. |
| D | 25 to 35 seconds | This is the point at which a traffic signal may be warranted for this intersection. The delays for the stop-controlled intersection are not considered to be excessive. The length of the queue may begin to block other public and private access points. |
| E | 35 to 50 seconds | The delays for all critical traffic movements are considered to be unacceptable. The length of the queues for the stop-controlled approaches as well as the left-turn movements are extremely long. There is a high probability that this intersection will meet traffic signal warrants. The ability to install a traffic signal is affected by the location of other existing traffic signals. Consideration may be given to restricting the accesses by eliminating the left-turn movements from and to the stop-controlled approach. |
| F | >50 seconds | The delay for the critical traffic movements are probably in excess of 100 seconds. The length of the queues are extremely long. Motorists are selecting alternative routes due to the long delays. The only remedy for these long delays is installing a traffic signal or restricting the accesses. The potential for accidents at this intersection are extremely high due to motorist taking more risky chances. If the median permits, motorists begin making two-stage left-turns. |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | 1 |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 5 | 5 | 65 | 5 | 5 | 35 |
| Future Vol, veh/h | 5 | 5 | 65 | 5 | 5 | 35 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, $\#$ | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 6 | 6 | 72 | 6 | 6 | 39 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.2 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{*}$ | 㻢 |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 75 | 200 | 4 | 1 | 260 | 30 | 1 | 1 | 1 | 20 | 1 | 40 |
| Future Vol, veh/h | 75 | 200 | 4 | 1 | 260 | 30 | 1 | 1 | 1 | 20 | 1 | 40 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 83 | 222 | 4 | 1 | 289 | 33 | 1 | 1 | 1 | 22 | 1 | 44 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | MF |  | $\mathbf{F}$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 5 | 10 | 65 | 5 | 10 | 90 |
| Future Vol, veh/h | 5 | 10 | 65 | 5 | 10 | 90 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 6 | 11 | 72 | 6 | 11 | 100 |


| Major/Minor | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 197 | 75 | 0 | 0 | 78 | 0 |
| Stage 1 | 75 | - | - | - | - | - |
| Stage 2 | 122 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 792 | 986 | - | - | 1520 | - |
| Stage 1 | 948 | - | - | - | - | - |
| Stage 2 | 903 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 786 | 986 | - | - | 1520 | - |
| Mov Cap-2 Maneuver | 786 | - | - | - | - | - |
| Stage 1 | 948 | - | - | - | - | - |
| Stage 2 | 896 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 9 |  | 0 |  | 0.7 |  |
| HCM LOS | A |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - | - | 909 | 1520 | - |
| HCM Lane V/C Ratio |  | - | - | 0.018 | 0.007 | - |
| HCM Control Delay (s) |  | - | - | 9 | 7.4 | 0 |
| HCM Lane LOS |  | - | - | A | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.1 | 0 | - |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.8 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  |  | \$ |  |  | \$ |  |
| Traffic Vol, veh/h | 60 | 270 | 6 | 1 | 315 | 15 | 5 | 1 | 1 | 35 | 1 | 85 |
| Future Vol, veh/h | 60 | 270 | 6 | 1 | 315 | 15 | 5 | 1 | 1 | 35 | 1 | 85 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control F | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 67 | 300 | 7 | 1 | 350 | 17 | 6 | 1 | 1 | 39 | 1 | 94 |





| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh 1.8 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{*}$ | 中 ${ }^{\text {a }}$ |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 76 | 350 | 4 | 1 | 315 | 31 | 1 | 1 | 1 | 21 | 1 | 41 |
| Future Vol, veh/h | 76 | 350 | 4 | 1 | 315 | 31 | 1 | 1 | 1 | 21 | 1 | 41 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 84 | 389 | 4 | 1 | 350 | 34 | 1 | 1 | 1 | 23 | 1 | 46 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.1 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | MF |  | $\mathbf{F}$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 5 | 10 | 66 | 5 | 10 | 93 |
| Future Vol, veh/h | 5 | 10 | 66 | 5 | 10 | 93 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 6 | 11 | 73 | 6 | 11 | 103 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.7 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 虫 |  | ${ }^{*}$ | 㻢 |  |  | \& |  |  | \& |  |
| Traffic Vol, veh/h | 61 | 315 | 6 | 1 | 420 | 15 | 5 | 1 | 1 | 36 | 1 | 87 |
| Future Vol, veh/h | 61 | 315 | 6 | 1 | 420 | 15 | 5 | 1 | 1 | 36 | 1 | 87 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 68 | 350 | 7 | 1 | 467 | 17 | 6 | 1 | 1 | 40 | 1 | 97 |




| Major/Minor | Major1 | Major2 |  |  |  |  |  | Minor1 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 0 | 0 | 417 | 0 | 854 | 386 |  |  |  |  |
| Stage 1 | - | - | - | - | 386 | - |  |  |  |  |
| Stage 2 | - | - | - | - | 468 | - |  |  |  |  |
| Critical Hdwy | - | - | 4.12 | - | 6.42 | 6.22 |  |  |  |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |  |  |  |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |  |  |  |  |
| Follow-up Hdwy | - | - | 2.218 | - | 3.518 | 3.318 |  |  |  |  |
| Pot Cap-1 Maneuver | - | - | 1142 | - | 329 | 662 |  |  |  |  |
| Stage 1 | - | - | - | - | 687 | - |  |  |  |  |
| Stage 2 | - | - | - | - | 630 | - |  |  |  |  |
| Platoon blocked, \% | - | - |  | - |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | - | - | 1142 | - | 329 | 662 |  |  |  |  |
| Mov Cap-2 Maneuver | - | - | - | - | 329 | - |  |  |  |  |
| Stage 1 | - | - | - | - | 687 | - |  |  |  |  |
| Stage 2 | - | - | - | - | 629 | - |  |  |  |  |


| Approach | EB | WB | NB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0 | 0 | 17.4 |
| HCM LOS |  | $C$ |  |


| Minor Lane/Major Mvmt | NBLn1 NBLn2 |  | EBT | EBR | WBL | WBT |
| :--- | ---: | ---: | ---: | ---: | ---: | :--- |
| Capacity (veh/h) | 329 | 662 | - | -1142 | - |  |
| HCM Lane V/C Ratio | 0.142 | 0.003 | - | -0.001 | - |  |
| HCM Control Delay (s) | 17.7 | 10.5 | - | - | 8.2 | - |
| HCM Lane LOS | C | B | - | - | A | - |
| HCM 95th \%tile Q(veh) | 0.5 | 0 | - | - | 0 | - |


| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.3 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 10 | 5 | 69 | 7 | 5 | 42 |
| Future Vol, veh/h | 10 | 5 | 69 | 7 | 5 | 42 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 6 | 77 | 8 | 6 | 47 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.4 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | i | 4 | $\mathbf{4}$ | $\mathbf{7}$ |  | $\mathbf{7}$ |
| Traffic Vol, veh/h | 40 | 423 | 448 | 2 | 0 | 95 |
| Future Vol, veh/h | 40 | 423 | 448 | 2 | 0 | 95 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | Free |
| Storage Length | 300 | - | - | 300 | - | 0 |
| Veh in Median Storage, $\#$ | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, $\%$ | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 44 | 470 | 498 | 2 | 0 | 106 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.2 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\mathbf{F}$ |  |  | $\mathbf{\uparrow}$ |
| Traffic Vol, veh/h | 9 | 10 | 72 | 11 | 10 | 97 |
| Future Vol, veh/h | 9 | 10 | 72 | 11 | 10 | 97 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 10 | 11 | 80 | 12 | 11 | 108 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.9 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{*}$ | 中 ${ }^{\text {a }}$ |  |  | $\uparrow$ |  |  | \& |  |
| Traffic Vol, veh/h | 73 | 527 | 6 | 1 | 560 | 15 | 5 | 1 | 1 | 36 | 1 | 95 |
| Future Vol, veh/h | 73 | 527 | 6 | 1 | 560 | 15 | 5 | 1 | 1 | 36 | 1 | 95 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 81 | 586 | 7 | 1 | 622 | 17 | 6 | 1 | 1 | 40 | 1 | 106 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0.8 |  |  |  |  |  |
| Movement | EBL | EBT | WBT | WBR | SBL | SBR |
| Lane Configurations | $\mathbf{a}$ | $\mathbf{4}$ | 个 | $\mathbf{F}$ |  | $\mathbf{7}$ |
| Traffic Vol, veh/h | 97 | 480 | 525 | 6 | 0 | 65 |
| Future Vol, veh/h | 97 | 480 | 525 | 6 | 0 | 65 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | Free |
| Storage Length | 300 | - | - | 300 | - | 0 |
| Veh in Median Storage, \# | - | 0 | 0 | - | 0 | - |
| Grade, \% | - | 0 | 0 | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 108 | 533 | 583 | 7 | 0 | 72 |





| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.7 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | 10 |  | $\mathbf{T}$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 10 | 10 | 70 | 10 | 10 | 40 |
| Future Vol, veh/h | 10 | 10 | 70 | 10 | 10 | 40 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 11 | 78 | 11 | 11 | 44 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.1 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 虫 |  | ${ }^{7}$ | 中 ${ }^{\text {c }}$ |  |  | $\uparrow$ |  |  | \& |  |
| Traffic Vol, veh/h | 80 | 555 | 5 | 2 | 655 | 35 | 2 | 2 | 2 | 25 | 2 | 45 |
| Future Vol, veh/h | 80 | 555 | 5 | 2 | 655 | 35 | 2 | 2 | 2 | 25 | 2 | 45 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 89 | 617 | 6 | 2 | 728 | 39 | 2 | 2 | 2 | 28 | 2 | 50 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 个 | $\mathbf{7}$ |  | 个 |  | $\mathbf{7}$ |
| Traffic Vol, veh/h | 562 | 24 | 0 | 689 | 0 | 0 |
| Future Vol, veh/h | 562 | 24 | 0 | 689 | 0 | 0 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 300 | - | - | - | 0 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 624 | 27 | 0 | 766 | 0 | 0 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 2.5 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | 「 | ${ }^{1}$ | 4 | 「 | ${ }^{*}$ | $\uparrow$ |  | ${ }^{1 /}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 30 | 485 | 47 | 4 | 575 | 2 | 24 | 1 | 1 | 5 | 1 | 90 |
| Future Vol, veh/h | 30 | 485 | 47 | 4 | 575 | 2 | 24 | 1 | 1 | 5 | 1 | 90 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 300 | - | 300 | 300 | - | 300 | 100 | - | - | 100 | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 33 | 539 | 52 | 4 | 639 | 2 | 27 | 1 | 1 | 6 | 1 | 100 |



| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 1.6 |  |  |  |  |  |
| Movement | WBL | WBR | NBT | NBR | SBL | SBT |
| Lane Configurations | Mr |  | $\uparrow$ |  |  | $\uparrow$ |
| Traffic Vol, veh/h | 10 | 15 | 70 | 10 | 15 | 95 |
| Future Vol, veh/h | 10 | 15 | 70 | 10 | 15 | 95 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Stop | Stop | Free | Free | Free | Free |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | 0 | - | - | - | - | - |
| Veh in Median Storage, \# | 0 | - | 0 | - | - | 0 |
| Grade, \% | 0 | - | 0 | - | - | 0 |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 11 | 17 | 78 | 11 | 17 | 106 |


| Major/Minor M | Minor1 |  | Major1 |  | Major2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 224 | 84 | 0 | 0 | 89 | 0 |
| Stage 1 | 84 | - | - | - | - | - |
| Stage 2 | 140 | - | - | - | - | - |
| Critical Hdwy | 6.42 | 6.22 | - | - | 4.12 | - |
| Critical Hdwy Stg 1 | 5.42 | - | - | - | - | - |
| Critical Hdwy Stg 2 | 5.42 | - | - | - | - | - |
| Follow-up Hdwy | 3.518 | 3.318 | - | - | 2.218 | - |
| Pot Cap-1 Maneuver | 764 | 975 | - | - | 1506 | - |
| Stage 1 | 939 | - | - | - | - | - |
| Stage 2 | 887 | - | - | - | - | - |
| Platoon blocked, \% |  |  | - | - |  | - |
| Mov Cap-1 Maneuver | 755 | 975 | - | - | 1506 | - |
| Mov Cap-2 Maneuver | 755 | - | - | - | - | - |
| Stage 1 | 939 | - | - | - | - | - |
| Stage 2 | 876 | - | - | - | - | - |
|  |  |  |  |  |  |  |
| Approach | WB |  | NB |  | SB |  |
| HCM Control Delay, s | 9.3 |  | 0 |  | 1 |  |
| HCM LOS | A |  |  |  |  |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | NBT | NBRWBLn1 |  | SBL | SBT |
| Capacity (veh/h) |  | - |  | 873 | 1506 | - |
| HCM Lane V/C Ratio |  | - | - | 0.032 | 0.011 | - |
| HCM Control Delay (s) |  | - | - | 9.3 | 7.4 | 0 |
| HCM Lane LOS |  | - | - | A | A | A |
| HCM 95th \%tile Q(veh) |  | - | - | 0.1 | 0 | - |




| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Int Delay, s/veh | 0 |  |  |  |  |  |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |
| Lane Configurations | 个 | $\mathbf{r}$ |  | 个 |  | $\mathbf{7}$ |
| Traffic Vol, veh/h | 675 | 39 | 0 | 684 | 0 | 3 |
| Future Vol, veh/h | 675 | 39 | 0 | 684 | 0 | 3 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Stop | Stop |
| RT Channelized | - | None | - | None | - | None |
| Storage Length | - | 300 | - | - | - | 0 |
| Veh in Median Storage, \# | 0 | - | - | 0 | 0 | - |
| Grade, \% | 0 | - | - | 0 | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 750 | 43 | 0 | 760 | 0 | 3 |





| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 1.3 | 0 | 254.5 | 15.7 |
| HCM LOS |  |  | F | C |


| Minor Lane/Major Mvmt | NBLn1 NBLn2 | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 SBLn2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 84 | 218 | 977 | - | - | 938 | - | - | 98 |
| 451 |  |  |  |  |  |  |  |  |  |
| HCM Lane V/C Ratio | 1.243 | 0.025 | 0.108 | - | -0.004 | - | - | 0.034 | 0.14 |
| HCM Control Delay (s) | 266.9 | 21.9 | 9.1 | - | - | 8.9 | - | - | 43 |
| HCM Lane LOS | F | C | A | - | - | A | - | - | E |
| HCM 95th \%tile Q(veh) | 7.7 | 0.1 | 0.4 | - | - | 0 | - | - | 0.1 |
| H |  |  | 0.5 |  |  |  |  |  |  |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

| Intersection |  |  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 3 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 中 ${ }^{\text {a }}$ |  | ${ }^{1}$ | 的 |  |  | $\uparrow$ |  |  | \& |  |
| Traffic Vol, veh/h | 84 | 638 | 5 | 2 | 843 | 35 | 2 | 2 | 2 | 25 | 2 | 55 |
| Future Vol, veh/h | 84 | 638 | 5 | 2 | 843 | 35 | 2 | 2 | 2 | 25 | 2 | 55 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Frest | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 93 | 709 | 6 | 2 | 937 | 39 | 2 | 2 | 2 | 28 | 2 | 61 |





| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 5.5 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | 「 | ${ }^{1}$ | 4 | 「 | ${ }^{7}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 68 | 485 | 52 | 4 | 578 | 4 | 26 | 2 | 1 | 15 | 2 | 180 |
| Future Vol, veh/h | 68 | 485 | 52 | 4 | 578 | 4 | 26 | 2 | 1 | 15 | 2 | 180 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 300 | - | 300 | 300 | - | 300 | 100 | - | - | 100 | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 76 | 539 | 58 | 4 | 642 | 4 | 29 | 2 | 1 | 17 | 2 | 200 |





| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 8.3 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | 虫 |  | ${ }^{1}$ | 中 ${ }^{\text {a }}$ |  |  | \$ |  |  | \$ |  |
| Traffic Vol, veh/h | 77 | 877 | 10 | 2 | 790 | 20 | 10 | 2 | 2 | 40 | 2 | 98 |
| Future Vol, veh/h | 77 | 877 | 10 | 2 | 790 | 20 | 10 | 2 | 2 | 40 | 2 | 98 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 90 | - | - | 100 | - | - | - | - | - | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 86 | 974 | 11 | 2 | 878 | 22 | 11 | 2 | 2 | 44 | 2 | 109 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh | 0.6 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | 「゙ |  | 个 | 「 |  |  | 「＇ |  |  | 「＇ |
| Traffic Vol，veh／h | 97 | 790 | 39 | 0 | 759 | 6 | 0 | 0 | 3 | 0 | 0 | 65 |
| Future Vol，veh／h | 97 | 790 | 39 | 0 | 759 | 6 | 0 | 0 | 3 | 0 | 0 | 65 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | Free |
| Storage Length | 300 | － | 300 | － | － | 300 | － | － | 0 | － | － | 0 |
| Veh in Median Storage，\＃ | \＃ | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles，\％ | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 108 | 878 | 43 | 0 | 843 | 7 | 0 | 0 | 3 | 0 | 0 | 72 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 75.4 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 4 | 「 | ${ }^{1}$ | 4 | 「 | ${ }^{1}$ | $\uparrow$ |  | ${ }^{7}$ | $\uparrow$ |  |
| Traffic Vol, veh/h | 201 | 555 | 37 | 3 | 539 | 11 | 104 | 4 | 4 | 10 | 4 | 120 |
| Future Vol, veh/h | 201 | 555 | 37 | 3 | 539 | 11 | 104 | 4 | 4 | 10 | 4 | 120 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 300 | - | 300 | 300 | - | 300 | 100 | - | - | 100 | - | - |
| Veh in Median Storage, | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 | 90 |
| Heavy Vehicles, \% | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 | 2 |
| Mvmt Flow | 223 | 617 | 41 | 3 | 599 | 12 | 116 | 4 | 4 | 11 | 4 | 133 |


| Major/Minor | Major1 |  |  | Major2 |  |  | Minor1 |  |  | Minor2 |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 611 | 0 | 0 | 658 | 0 | 0 | 1743 | 1680 | 617 | 1693 | 1709 | 599 |  |
| Stage 1 | - | - | - | - | - | - | 1063 | 1063 | - | 605 | 605 | - |  |
| Stage 2 | - | - | - | - | - | - | 680 | 617 | - | 1088 | 1104 | - |  |
| Critical Hdwy | 4.12 | - | - | 4.12 | - | - | 7.12 | 6.52 | 6.22 | 7.12 | 6.52 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | - | - | 6.12 | 5.52 | - | 6.12 | 5.52 | - |  |
| Follow-up Hdwy | 2.218 | - | - | 2.218 | - | - | 3.518 | 4.018 | 3.318 | 3.518 | 4.018 | 3.318 |  |
| Pot Cap-1 Maneuver | 968 | - | - | 930 | - | - | ~ 68 | 95 | 490 | 74 | 91 | 502 |  |
| Stage 1 | - | - | - | - | - | - | 270 | 300 | - | 485 | 487 | - |  |
| Stage 2 | - | - | - | - | - | - | 441 | 481 | - | 261 | 287 | - |  |
| Platoon blocked, \% |  | - | - |  | - | - |  |  |  |  |  |  |  |
| Mov Cap-1 Maneuver | 968 | - | - | 930 | - | - | ~ 39 | 73 | 490 | 57 | 70 | 502 |  |
| Mov Cap-2 Maneuver | - | - | - | - | - | - | ~ 39 | 73 | - | 57 | 70 | - |  |
| Stage 1 | - | - | - | - | - | - | 208 | 231 | - | 373 | 486 | - |  |
| Stage 2 | - | - | - | - | - | - | 320 | 480 | - | 195 | 221 | - |  |


| Approach | EB | WB | NB | SB |
| :--- | ---: | ---: | ---: | ---: |
| HCM Control Delay, s | 2.5 | 0 | $\$ 1026.8$ | 22.6 |
| HCM LOS |  |  | F | C |


| Minor Lane/Major Mvmt | NBLn1 NBLn2 |  | EBL | EBT | EBR | WBL | WBT | WBR SBLn1 SBLn2 |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 39 | 127 | 968 | - | - | 930 | - | - | 57 |
| HCM Lane V/C Ratio | 2.963 | 0.07 | 0.231 | - | - | 419 |  |  |  |
| HCM Control Delay (s) | $\$ 1103$ | 35.5 | 9.8 | - | - | 8.9 | - | -0.195 | 0.329 |
| HCM Lane LOS | F | E | A | - | - | A | - | - | F |
| HCM 95th \%tile Q(veh) | 12.9 | 0.2 | 0.9 | - | - | 0 | - | - | 0.7 |

## Notes

$\sim$ : Volume exceeds capacity $\$$ : Delay exceeds 300s $\quad+$ : Computation Not Defined $\quad$ : All major volume in platoon

|  | 4 |  | 6 | $\leftarrow$ | 4 |  | - | $\dagger$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
| Lane Configurations | ${ }^{7}$ | 中 ${ }^{\text {P }}$ | ${ }^{7}$ | 中 ${ }^{\text {P }}$ |  | \& |  |  |
| Traffic Volume (vph) | 84 | 638 | 2 | 843 | 2 | 2 | 25 | 2 |
| Future Volume (vph) | 84 | 638 | 2 | 843 | 2 | 2 | 25 | 2 |
| Turn Type | pm+pt | NA | pm+pt | NA | Perm | NA | Perm | NA |
| Protected Phases | 7 | 4 | 3 | 8 |  | 2 |  | 6 |
| Permitted Phases | 4 |  | 8 |  | 2 |  | 6 |  |
| Detector Phase | 7 | 4 | 3 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 23.0 | 9.5 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |
| Total Split (s) | 12.0 | 53.0 | 12.0 | 53.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Total Split (\%) | 13.3\% | 58.9\% | 13.3\% | 58.9\% | 27.8\% | 27.8\% | 27.8\% | 27.8\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.5 | 1.0 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |  | 0.0 |
| Total Lost Time (s) | 4.5 | 5.0 | 4.5 | 5.0 |  | 5.0 |  | 5.0 |
| Lead/Lag | Lead | Lag | Lead | Lag |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes |  |  |  |  |
| Recall Mode | None | C-Max | None | C-Max | None | None | None | None |
| Act Effct Green (s) | 74.3 | 73.3 | 70.2 | 66.3 |  | 7.8 |  | 7.8 |
| Actuated g/C Ratio | 0.83 | 0.81 | 0.78 | 0.74 |  | 0.09 |  | 0.09 |
| v/c Ratio | 0.19 | 0.25 | 0.00 | 0.38 |  | 0.04 |  | 0.49 |
| Control Delay | 3.0 | 3.5 | 2.0 | 4.3 |  | 31.4 |  | 25.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |  | 0.0 |
| Total Delay | 3.0 | 3.5 | 2.0 | 4.3 |  | 31.4 |  | 25.2 |
| LOS | A | A | A | A |  | C |  | C |
| Approach Delay |  | 3.4 |  | 4.3 |  | 31.4 |  | 25.2 |
| Approach LOS |  | A |  | A |  | C |  | C |
| Intersection Summary |  |  |  |  |  |  |  |  |

## Cycle Length: 90

Actuated Cycle Length: 90
Offset: 42 (47\%), Referenced to phase 4:EBTL and 8:WBTL, Start of Green
Natural Cycle: 60
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.49
Intersection Signal Delay: $5.0 \quad$ Intersection LOS: A
Intersection Capacity Utilization 47.4\% ICU Level of Service A
Analysis Period (min) 15

Splits and Phases: 2: Adams Street \& E. Tomichi Avenue


|  | 4 |  |  |  |  |  | 4 | $\dagger$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Configurations | 7 | $\uparrow$ | 「 | \% | $\uparrow$ | 「 | \% | $\uparrow$ | \% | $\uparrow$ |
| Traffic Volume (vph) | 68 | 485 | 52 | , | 578 | 4 | 26 | 2 | 15 | 2 |
| Future Volume (vph) | 68 | 485 | 52 | 4 | 578 | 4 | 26 | 2 | 15 | 2 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm | NA |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 2 |  | 6 |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 6 |  |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 10.0 | 23.0 | 23.0 | 10.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |
| Total Split (s) | 12.0 | 53.0 | 53.0 | 12.0 | 53.0 | 53.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Total Split (\%) | 13.3\% | 58.9\% | 58.9\% | 13.3\% | 58.9\% | 58.9\% | 27.8\% | 27.8\% | 27.8\% | 27.8\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes |  |  |  |  |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None |
| Act Effct Green (s) | 70.8 | 69.3 | 69.3 | 66.6 | 62.2 | 62.2 | 8.6 | 8.6 | 8.6 | 8.6 |
| Actuated g/C Ratio | 0.79 | 0.77 | 0.77 | 0.74 | 0.69 | 0.69 | 0.10 | 0.10 | 0.10 | 0.10 |
| v/c Ratio | 0.14 | 0.38 | 0.05 | 0.01 | 0.50 | 0.00 | 0.35 | 0.02 | 0.13 | 0.61 |
| Control Delay | 2.7 | 7.0 | 2.6 | 2.8 | 9.5 | 0.0 | 48.8 | 31.0 | 37.6 | 14.2 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 2.7 | 7.0 | 2.6 | 2.8 | 9.5 | 0.0 | 48.8 | 31.0 | 37.6 | 14.2 |
| LOS | A | A | A | A | A | A | D | C | D | B |
| Approach Delay |  | 6.1 |  |  | 9.4 |  |  | 47.2 |  | 16.0 |
| Approach LOS |  | A |  |  | A |  |  | D |  | B |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |

## Cycle Length: 90

Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 4:EBTL and 8:WBTL, Start of Green
Natural Cycle: 60
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.61
Intersection Signal Delay: 9.7 Intersection LOS: A
Intersection Capacity Utilization 66.7\%
ICU Level of Service C
Analysis Period (min) 15
Splits and Phases: 4: Site Access \& E. Tomichi Avenue


|  | 4 | $\rightarrow$ | $\%$ |  | 4 |  | $\pm$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | WBL | WBT | NBL | NBT | SBL | SBT |
| Lane Configurations | ${ }^{7}$ | 㻢 | ${ }^{1}$ | 中 ${ }^{\text {P }}$ |  | 4 |  |  |
| Traffic Volume (vph) | 77 | 877 | 2 | 790 | 10 | 2 | 40 | 2 |
| Future Volume (vph) | 77 | 877 | 2 | 790 | 10 | 2 | 40 | 2 |
| Turn Type | pm+pt | NA | pm+pt | NA | Perm | NA | Perm | NA |
| Protected Phases | 7 | 4 | 3 | 8 |  | 2 |  | 6 |
| Permitted Phases | 4 |  | 8 |  | 2 |  | 6 |  |
| Detector Phase | 7 | 4 | 3 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 9.5 | 23.0 | 9.5 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |
| Total Split (s) | 12.0 | 53.0 | 12.0 | 53.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Total Split (\%) | 13.3\% | 58.9\% | 13.3\% | 58.9\% | 27.8\% | 27.8\% | 27.8\% | 27.8\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.0 | 1.5 | 1.0 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |  | 0.0 |
| Total Lost Time (s) | 4.5 | 5.0 | 4.5 | 5.0 |  | 5.0 |  | 5.0 |
| Lead/Lag | Lead | Lag | Lead | Lag |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes |  |  |  |  |
| Recall Mode | None | C-Max | None | C-Max | None | None | None | None |
| Act Effct Green (s) | 71.1 | 69.0 | 66.9 | 62.0 |  | 9.0 |  | 9.0 |
| Actuated g/C Ratio | 0.79 | 0.77 | 0.74 | 0.69 |  | 0.10 |  | 0.10 |
| v/c Ratio | 0.18 | 0.36 | 0.00 | 0.37 |  | 0.13 |  | 0.62 |
| Control Delay | 3.4 | 4.8 | 4.0 | 6.7 |  | 33.9 |  | 24.6 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 |  | 0.0 |
| Total Delay | 3.4 | 4.8 | 4.0 | 6.7 |  | 33.9 |  | 24.6 |
| LOS | A | A | A | A |  | C |  | C |
| Approach Delay |  | 4.7 |  | 6.7 |  | 33.9 |  | 24.6 |
| Approach LOS |  | A |  | A |  | C |  | C |
| Intersection Summary |  |  |  |  |  |  |  |  |

## Cycle Length: 90

Actuated Cycle Length: 90
Offset: 42 (47\%), Referenced to phase 4:EBTL and 8:WBTL, Start of Green
Natural Cycle: 60
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.62
Intersection Signal Delay: $7.2 \quad$ Intersection LOS: A
Intersection Capacity Utilization 49.0\% ICU Level of Service A
Analysis Period (min) 15
Splits and Phases: 2: Adams Street \& E. Tomichi Avenue


|  | 4 |  |  |  |  |  | 4 | $\dagger$ |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | SBL | SBT |
| Lane Configurations | \% | $\uparrow$ | 「 | ${ }_{7}$ | $\uparrow$ | 「 | \% | $\hat{F}$ | \% | $\hat{1}$ |
| Traffic Volume (vph) | 201 | 555 | 37 | , | 539 | 11 | 104 | 4 | 10 | 4 |
| Future Volume (vph) | 201 | 555 | 37 | 3 | 539 | 11 | 104 | 4 | 10 | 4 |
| Turn Type | pm+pt | NA | Perm | pm+pt | NA | Perm | Perm | NA | Perm | NA |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 2 |  | 6 |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 6 |  |
| Detector Phase | 7 | 4 | 4 | 3 | 8 | 8 | 2 | 2 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Minimum Split (s) | 10.0 | 23.0 | 23.0 | 10.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 | 23.0 |
| Total Split (s) | 12.0 | 53.0 | 53.0 | 12.0 | 53.0 | 53.0 | 25.0 | 25.0 | 25.0 | 25.0 |
| Total Split (\%) | 13.3\% | 58.9\% | 58.9\% | 13.3\% | 58.9\% | 58.9\% | 27.8\% | 27.8\% | 27.8\% | 27.8\% |
| Yellow Time (s) | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 | 3.5 |
| All-Red Time (s) | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 | 1.5 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Lead/Lag | Lead | Lag | Lag | Lead | Lag | Lag |  |  |  |  |
| Lead-Lag Optimize? | Yes | Yes | Yes | Yes | Yes | Yes |  |  |  |  |
| Recall Mode | None | C-Max | C-Max | None | C-Max | C-Max | None | None | None | None |
| Act Effct Green (s) | 65.4 | 64.0 | 64.0 | 58.6 | 53.0 | 53.0 | 13.9 | 13.9 | 13.9 | 13.9 |
| Actuated g/C Ratio | 0.73 | 0.71 | 0.71 | 0.65 | 0.59 | 0.59 | 0.15 | 0.15 | 0.15 | 0.15 |
| v/c Ratio | 0.43 | 0.47 | 0.04 | 0.01 | 0.55 | 0.01 | 0.67 | 0.03 | 0.05 | 0.38 |
| Control Delay | 9.0 | 5.9 | 0.1 | 5.0 | 14.7 | 0.0 | 53.4 | 22.9 | 29.9 | 9.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 9.0 | 5.9 | 0.1 | 5.0 | 14.7 | 0.0 | 53.4 | 22.9 | 29.9 | 9.4 |
| LOS | A | A | A | A | B | A | D | C | C | A |
| Approach Delay |  | 6.4 |  |  | 14.3 |  |  | 51.4 |  | 11.0 |
| Approach LOS |  | A |  |  | B |  |  | D |  | B |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |

## Cycle Length: 90

Actuated Cycle Length: 90
Offset: $0(0 \%)$, Referenced to phase 4:EBTL and 8:WBTL, Start of Green
Natural Cycle: 60
Control Type: Actuated-Coordinated
Maximum v/c Ratio: 0.67
Intersection Signal Delay: $12.7 \quad$ Intersection LOS: B
Intersection Capacity Utilization 69.6\% ICU Level of Service C
Analysis Period (min) 15
Splits and Phases: 4: Site Access \& E. Tomichi Avenue

(303) 333-1105

FAX (303) 333-1107
E-mail: Isc@Iscdenver.com

August 28, 2020
Mr. Byron Chrisman
Gunnison Valley Properties, LLC
864 W. South Boulder Road
Louisville, CO 80027

Re: Gunnison Rising Government<br>Campus Subdivision<br>Gunnison, CO<br>LSC \#191121

Dear Mr. Chrisman:
In response to your request, LSC Transportation Consultants, Inc. has prepared this traffic impact analysis (CDOT Level III traffic study) for the proposed Gunnison Rising Government Campus Subdivision. As shown on Figure 1, the site is located south of US Highway (US) 50 near the intersection with Ute Lane West (CR 72) in Gunnison, Colorado.

## REPORT CONTENTS

The report contains the following: the existing roadway and traffic conditions in the vicinity of the site including the lane geometries, traffic controls, etc.; the existing weekday peak-hour traffic volumes; the existing daily traffic volumes in the area; the typical weekday site-generated traffic volume projections for the site; the short-term and long-term assignment of the projected traffic volumes to the area roadways; the projected short-term and long-term background and resulting total traffic volumes on the area roadways; the site's projected traffic impacts; and any recommended roadway improvements to mitigate the site's traffic impacts. The scope of work is consistent with the attached TIS Methodology Form approved by CDOT with the exception of a few proposed land use details that were modified throughout the process.

## LAND USE AND ACCESS

The site is proposed to include a government office campus with about 68,000 square feet of office/light industrial space, a 5,000 square-foot convenience/gas store, and an RV Campground with about 300 sites. Access is proposed to US 50 aligning with Ute Lane West (CR 72) as shown in the site plan in Figure 2. Emergency only access is proposed to US 50 aligning with Ute Lane East (CR 72). A preliminary plat for the government campus portion of the site is attached for reference.

## ROADWAY AND TRAFFIC CONDITIONS

## Area Roadways

The major roadways in the site's vicinity are shown on Figure 1 and are described below.

- US Highway $\mathbf{5 0}$ (US 50) is an east-west, two-lane US highway north of the site. It is designated R-A (Regional Highway) by CDOT per the attached CDOT Straight Line Diagram. The intersection with Ute Lane West (CR 72) is stop-sign controlled and shown as a full movement intersection in the US 50 Access Control Plan (ACP). An excerpt from the ACP is attached for reference. The posted speed limit in the vicinity of the site is 65 mph .
- Ute Lane West (CR 72) is a two-lane county roadway north of the site. The intersection with US 50 is stop-sign controlled. The posted speed limit in the vicinity of the site is 25 mph .


## Existing Sight Distance

There is very good sight distance in each direction of US 50 from the proposed access location aligning with Ute Lane West (CR 72).

## Existing Traffic Conditions

Figure 3a shows the existing weekday traffic volumes, existing lane geometry and the existing traffic controls in the vicinity of the site. The weekday peak-hour traffic volumes and average daily traffic volumes are from the attached traffic counts conducted by Counter Measures in February, 2020.

Figure 3b shows the estimated July traffic volumes based on a seasonal adjustment factor of 2.27 for US 50 traffic and a conservative 1.50 factor for Ute Lane West (CR 72).

## 2024 and 2040 Background Traffic

Figure 4 shows the estimated 2024 background traffic and Figure 5 shows the estimated 2040 background traffic. The background traffic volumes on SH 50 assume an annual growth rate of about 0.2 percent based on CDOT's 20-year factor of 1.04 per the approved TIS methodology. Little or no growth was assumed for side street traffic as any future development will be required to prepare its own traffic impact analysis.

## Existing, 2024, and 2040 Background Levels of Service

Level of service (LOS) is a quantitative measure of the level of congestion or delay at an intersection. Level of service is indicated on a scale from "A" to "F." LOS A is indicative of little congestion or delay and LOS F is indicative of a high level of congestion or delay. Attached are specific level of service definitions for signalized and unsignalized intersections.

The intersections in the study area were analyzed to determine the existing, 2024, and 2040 background levels of service using Synchro. Table 1 shows the level of service analysis results. The level of service reports are attached.

- US 50/Ute Lane West (CR 72): All movements at this unsignalized intersection currently operate at LOS "B" or better during both morning and afternoon peak-hours and are expected to do so through 2040.


## TRIP GENERATION

Table 2 shows the estimated average daily, weekday morning peak-hour, and weekday afternoon peak-hour trip generation potential for the proposed site based on the rates from Trip Generation, $10^{\text {th }}$ Edition, 2017 by the Institute of Transportation Engineers (ITE).

By 2024, the site is projected to generate about 2,365 external vehicle-trips on the average weekday, with about half entering and half exiting during a 24 -hour period. During the morning peak-hour, which generally occurs for one hour between 6:30 and 8:30 a.m., about 155 vehicles would enter and about 118 vehicles would exit the site. During the afternoon peakhour, which generally occurs for one hour between 4:00 and 6:00 p.m., about 131 vehicles would enter and about 152 vehicles would exit.

At buildout, the site is projected to generate about 3,252 external vehicle-trips on the average weekday, with about half entering and half exiting during a 24 -hour period. During the morning peak-hour, which generally occurs for one hour between 6:30 and 8:30 a.m., about 231 vehicles would enter and about 173 vehicles would exit the site. During the afternoon peakhour, which generally occurs for one hour between 4:00 and 6:00 p.m., about 192 vehicles would enter and about 212 vehicles would exit.

## TRIP DISTRIBUTION

Figure 6 shows the estimated directional distribution of the site-generated traffic volumes on the area roadways. The estimates were based on the location of the site with respect to the regional population, employment, and activity centers; the site's proposed land use; and on the approved TIS methodology form. The RV Campground was added after the form was approved the assumed directional distribution for the campground is half to the west and half to the east.

## TRIP ASSIGNMENT

Figure 7 shows the assignment of 2024 site-generated traffic volumes for the site based on the directional distribution percentages (from Figure 6) and the 2024 trip generation estimate (from Table 2).

Figure 8a shows the assignment of 2040 government-campus site-generated traffic volumes for the site based on the directional distribution percentages (from Figure 6) and the 2040 government campus trip generation estimate (from Table 2).

Figure 8 b shows the assignment of 2040 RV Campground site-generated traffic volumes for the site based on the directional distribution percentages (from Figure 6) and the 2040 RV Campground trip generation estimate (from Table 2).

## 2024 AND 2040 TOTAL TRAFFIC

Figure 9 shows the 2024 total traffic which is the sum of the 2024 background traffic volumes (from Figure 4) and the 2024 site-generated traffic volumes (from Figure 7). Figure 9 also shows the recommended 2024 lane geometry and traffic control.

Figure 10 shows the 2040 total traffic which is the sum of the 2040 background traffic volumes (from Figure 5) and the 2040 site-generated traffic volumes (from Figures 8a and 8b). Figure 10 also shows the recommended 2040 lane geometry and traffic control.

## PROJECTED LEVELS OF SERVICE

The intersections in the study area were analyzed as appropriate to determine the 2024 and 2040 total levels of service. Table 1 shows the level of service analysis results. The level of service reports are attached.

- US 50/Ute Lane West (SH 72): All movements at this stop-sign controlled intersection are expected to operate at LOS "D" or better in both peak-hours through 2024. The northbound left/through movement is expected to operate at LOS " F " in the 2040 afternoon peak-hour at site buildout with the recommended improvements. The intersection would operate at an overall LOS "B" or better through 2040 with traffic signal control.


## TRAFFIC SIGNAL WARRANT ANALYSIS

Figures 11a and 11b show the traffic volumes for 2024 and 2040 total traffic plotted on a fourhour and peak-hour traffic signal warrant chart. Neither warrant is expected to be met with the land uses proposed through 2024 but both will likely be met by 2040 with full site buildout. Per the State Highway Access Code, a traffic signal warrant would need to be met to allow traffic signal installation in the future.

## $95^{\mathrm{TH}}$ PERCENTILE QUEUE LENGTHS

Table 3 shows the estimated $95^{\text {th }}$ percentile queue lengths for the signalized scenarios. The recommended northbound right-turn lane should be about 200 feet to avoid being blocked by queued vehicles waiting to turn left or proceed straight across US 50.

## ACCESS PERMIT APPLICATION

An access permit application should be made to CDOT for the proposed uses through 2024 to avoid needing to permit a traffic signal - the traffic volumes for this scenario are shown in Figures 7 and 9 .

## CONCLUSIONS AND RECOMMENDATIONS

## Trip Generation

1. By 2024, the site is projected to generate about 2,365 external vehicle-trips on the average weekday, with about half entering and half exiting during a 24 -hour period. During the morning peak-hour, about 155 vehicles would enter and about 118 vehicles would exit the
site. During the afternoon peak-hour, about 131 vehicles would enter and about 152 vehicles would exit.
2. At buildout, the site is projected to generate about 3,252 external vehicle-trips on the average weekday, with about half entering and half exiting during a 24 -hour period. During the morning peak-hour, about 231 vehicles would enter and about 173 vehicles would exit the site. During the afternoon peak-hour, about 192 vehicles would enter and about 212 vehicles would exit.

## Projected Levels of Service

3. All movements at the unsignalized US 50/Ute Lane West (CR 72) intersection are expected to operate at LOS "D" or better through 2024. The northbound left/through movement is expected to operate at LOS "F" in the 2040 afternoon peak-hour at site buildout with the recommended improvements. The intersection will operate at an overall LOS "B" or better through 2040 with traffic signal control.

## Conclusions

4. The impact of the Gunnison Rising Government Campus Subdivision can be accommodated by the existing and proposed roadway network with the following recommendations.

## Recommendations

5. The applicant should construct an eastbound right-turn deceleration lane on US 50 approaching the site access intersection. An appropriate length for the 65 mph posted speed limit would be a 500 -foot lane plus a 300 -foot transition taper. This lane will be needed by 2024.
6. The applicant should stripe a westbound left-turn deceleration lane on US 50 approaching the site access intersection. An appropriate length for the 65 mph posted speed limit would be 575 feet ( 500 feet for deceleration plus 75 feet for vehicle storage) and a 300-foot transition taper. This lane will be needed by 2024.
7. The applicant should construct a northbound to eastbound acceleration lane on US 50 heading east from the site access intersection. An appropriate length for the 65 mph posted speed limit would be 1,080 feet plus a 300 -foot transition taper. This lane is recommended by 2024.
8. The applicant should construct a dedicated northbound right-turn lane along with a shared through/left lane. The length of the right-turn lane should be about 200 feet to avoid being blocked by queued vehicles waiting to turn left or proceed straight across US 50.
9. Traffic signal control will not be warranted by the land uses through 2024 but will likely be by 2040 if the site reaches buildout.
10. The applicant should submit an access permit application for the land uses proposed through 2024 to avoid needing to permit a future traffic signal. The impacts through 2024 are shown in Figures 7 and 9.

We trust our findings will assist you in gaining approval of the proposed Gunnison Rising Government Campus Subdivision. Please contact me if you have any questions or need further assistance.

Sincerely,


Enclosures: Tables 1-3
Figures 1-11b
Approved TIS Methodology Form
Preliminary Plat for Government Campus Portion of the site
CDOT Straight Line Diagram
CDOT US 50 Access Control Plan Excerpt
Traffic Count Reports
Level of Service Definitions
Level of Service Reports
Queuing Reports
W: \LSC $\backslash$ Projects $\backslash 2019 \backslash 191121$-GunnisonRisingGovernmentCampusSubdivision $\backslash$ Aug-2020 $\backslash$ GunnisonRising-082820.wpd







Figure 2
Site Plan













## COLORADO

Department of Transportation
Region 3

## Transportation Impact Study <br> Methodology Form

Prior to starting a traffic impact study, a Methodology Form must be submitted for review and signed by the Region 3 Access Engineer. It shall be included as part of the study. Form submitted to CDOT 02/05/2020.

## CONTACT INFORMATION

| Consultant: | Name: |
| ---: | :---: |
| LSC TransDortation Consultants. Inc. (Chris McGranahan) |  |
|  | Telephone: |
| Email $:$ | chris@lsctrans.com and Isc@lscdenver.com |
| Developer/Owner Name: | Gunnison Valley Partners |

## PROJ ECT INFORMATION

| Project Name | Gunnison Rising |
| :--- | :--- |
| Project Location | East of Gunnison, CO on both sides of US 50 |
| Project Description <br> (Attached proposed site plan) | See attached site plan |
| State Highway | US 50 |
| County | Gunnison |
| Mile Post | Between 158 and 159 |
| Posted Speed Limit | 55 mph approaching from east and 65 mph approaching from west |

TIS ASSUMPTIONS

| Study Years | Current Year: 2020 | Buildout Year: 2025 |  | Long Term Year: 2040 |
| :---: | :---: | :---: | :---: | :---: |
| Traffic Assessment Level (Provide justification) | Level 3 Traffic Study |  |  |  |
| Study Intersections | 1. US 50/Adams Street |  | 6. |  |
|  | 2. Adams Street/College Avenue |  | 7. |  |
|  | 3. Proposed Access Point to US 50 |  | 8. |  |
|  | 4. |  | 9. |  |
|  | 5. |  | 10. |  |
| Future Growth Rate | $\square$ OTIS | $\square$ Regional TDM |  | $\square$ Other |
| Seasonal Adjustment Factor | Traffic counts will be modified using both a seasonal and pandemic adjustment. |  |  |  |

COLORADO
Department of Transportation
Region 3
ASSUMPTIONS CONTINUED


## CDOT INTERNAL USE ONLY

Review Comments

Revise and Resubmit



| 1 | $93,225 / 2.14 \mathrm{ac}$ | $14,500-29,000$ |
| :---: | ---: | :---: |
| 2 | $95,400 / 2.19 \mathrm{ac}$ | $15,500-31,000$ |
| 3 | $190,800 / 4.38 \mathrm{ac}$ | $32,000-64,000$ |
| 4 | $125,900 / 2.89 \mathrm{ac}$ | $21,000-42,000$ |
| 5 | $119,800 / 2.75 \mathrm{ac}$ | $22,000-44,000$ |
| Total | $\mathbf{6 2 5 , 1 2 5} / \mathbf{1 4 . 3 5} \mathbf{~ a c}$ | $\mathbf{1 0 5 , 0 0 0}-\mathbf{2 1 0 , 0 0 0}$ |




## Route 050A From 158 to 161




It may appear that information is missing from the straight line diagram. If so, reduce the number of miles/page and re-submit the request.


COUNTER MEASURES INC.
1889 YORK STREET
N/S STREET: UTE LANE
DENVER.COLORADO 303-333-7409
E/W STREET: HWY-50 CITY: GUNNISON

File Name : UTEHWY50
Site Code : 00000015
Start Date: 2/18/2020 Page No : 1
Groups Printed- VEHICLES

|  | UTE LANE Southbound |  |  |  | HWY-50 Westbound |  |  |  | Northbound |  |  |  | HWY-50 Eastbound |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | Left | Thru | Right | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 0 | 0 | 4 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 0 | 0 | 30 |
| 06:45 AM | 0 | 0 | 5 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 16 | 0 | 0 | 41 |
| Total | 0 | 0 | 9 | 0 | 0 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 32 | 0 | 0 | 71 |


| $07: 00$ AM | 0 | 0 | 2 | 0 | 0 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 32 |
| ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $07: 15$ AM | 0 | 0 | 5 | 0 | 0 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 38 |
| $07: 30$ AM | 0 | 0 | 6 | 0 | 0 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 0 | 0 | 50 |
| $07: 45$ AM | 1 | 0 | 10 | 0 | 0 | 34 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 24 | 0 | 0 | 73 |
| Total | 1 | 0 | 23 | 0 | 0 | 98 | 3 | 0 | 0 | 0 | 0 | 0 | 1 | 67 | 0 | 0 | 193 |


| 08:00 AM | 0 | 0 | 1 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 0 | 0 | 51 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08:15 AM | 0 | 0 | 3 | 0 | 0 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 26 | 0 | 0 | 60 |
| Total | 0 | 0 | 4 | 0 | 0 | 57 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 48 | 0 | 0 | 111 |


| 04:00 PM | 1 | 0 | 4 | 0 | 0 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 34 | 0 | 0 | 70 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 04:15 PM | 0 | 0 | 2 | 0 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 21 | 0 | 0 | 61 |
| 04:30 PM | 0 | 0 | 2 | 0 | 0 | 28 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 39 | 0 | 0 | 70 |
| 04:45 PM | 1 | 0 | 1 | 0 | 0 | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 33 | 0 | 0 | 87 |
| Total | 2 | 0 | 9 | 0 | 0 | 139 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 127 | 0 | 0 | 288 |


| $05: 00 ~ P M ~$ | 0 | 0 | 3 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 34 | 0 | 0 | 69 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $05: 15 ~ P M ~$ | 1 | 0 | 4 | 0 | 0 | 19 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 29 | 0 | 0 | 57 |
| $05: 30 ~ P M ~$ | 0 | 0 | 3 | 0 | 0 | 25 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 29 | 0 | 0 | 59 |
| $05: 45$ PM | 0 | 0 | 5 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 33 | 0 | 0 | 69 |
| Total | 1 | 0 | 15 | 0 | 0 | 94 | 1 | 0 | 0 | 0 | 0 | 0 | 18 | 125 | 0 | 0 | 254 |


| Grand Total | 4 | 0 | 60 | 0 | 0 | 417 | 4 | 0 | 0 | 0 | 0 | 0 | 33 | 399 | 0 | 0 | 917 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Apprch \% | 6.3 | 0.0 | 93.8 | 0.0 | 0.0 | 99.0 | 1.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 7.6 | 92.4 | 0.0 | 0.0 |  |
| Total \% | 0.4 | 0.0 | 6.5 | 0.0 | 0.0 | 45.5 | 0.4 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 3.6 | 43.5 | 0.0 | 0.0 |  |

## COUNTER MEASURES INC.

1889 YORK STREET
N/S STREET: UTE LANE
DENVER.COLORADO
File Name : UTEHWY50
E/W STREET: HWY-50
CITY: GUNNISON 303-333-7409

Site Code : 00000015
Start Date: 2/18/2020
Page No : 2

|  | UTE LANE Southbound |  |  |  |  | HWY-50 Westbound |  |  |  |  | Northbound |  |  |  |  | HWY-50 <br> Eastbound |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | $\begin{gathered} \text { Rig } \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Left | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Int. Total |

Peak Hour From 06:30 AM to 08:30 AM - Peak 1 of 1


## COUNTER MEASURES INC.

1889 YORK STREET
N/S STREET: UTE LANE
DENVER.COLORADO
File Name : UTEHWY50
E/W STREET: HWY-50
CITY: GUNNISON
303-333-7409
Site Code : 00000015
Start Date: 2/18/2020
Page No : 2


|  |  |  |
| :---: | :---: | :---: |
|  |  |  |
|  |  |  |

## LEVEL OF SERVICE DEFINITIONS

From Highway Capacity Manual, Transportation Research Board, 2016, 6th Edition
SIGNALIZED INTERSECTION LEVEL OF SERVICE (LOS)

| LOS | Average Vehicle Delay sec/vehicle | Operational Characteristics |
| :---: | :---: | :---: |
| A | <10 seconds | Describes operations with low control delay, up to $10 \mathrm{sec} / \mathrm{veh}$. This LOS occurs when progression is extremely favorable and most vehicles arrive during the green phase. Many vehicles do not stop at all. Short cycle lengths may tend to contribute to low delay values. |
| B | 10 to 20 seconds | Describes operations with control delay greater than 10 seconds and up to $20 \mathrm{sec} / \mathrm{veh}$. This level generally occurs with good progression, short cycle lengths, or both. More vehicles stop than with LOS A, causing higher levels of delay. |
| c | 20 to 35 seconds | Describes operations with control delay greater than 20 and up to $35 \mathrm{sec} / \mathrm{veh}$. These higher delays may result from only fair progression, longer cycle length, or both. Individual cycle failures may begin to appear at this level. Cycle failure occurs when a given green phase does not serve queued vehicles, and overflows occur. The number of vehicles stopping is significant at this level, though many still pass through the intersection without stopping. |
| D | 35 to 55 seconds | Describes operations with control delay greater than 35 and up to $55 \mathrm{sec} / \mathrm{veh}$. At LOS D, the influence of congestion becomes more noticeable. Longer delays may result from some combination of unfavorable progression, long cycle lengths, and high v/c ratios. Many vehicles stop, and the proportion of vehicles not stopping declines. Individual cycle failures are noticeable. |
| E | 55 to 80 seconds | Describes operations with control delay greater than 55 and up to 80 sec/veh. These high delay values generally indicate poor progression, long cycle lengths, and high v/c ratios. Individual cycle failures are frequent. |
| F | $\begin{gathered} >80 \\ \text { seconds } \end{gathered}$ | Describes operations with control delay in excess of 80 sec/veh. This level, considered unacceptable to most drivers, often occurs with over-saturation, that is, when arrival flow rates exceed the capacity of lane groups. It may also occur at high $\mathrm{v} / \mathrm{c}$ ratios with many individual cycle failures. Poor progression and long cycle lengths may also contribute significantly to high delay levels. |

## LEVEL OF SERVICE DEFINITIONS

From Highway Capacity Manual, Transportation Research Board, 2016, 6th Edition
UNSIGNALIZED INTERSECTION LEVEL OF SERVICE (LOS)
Applicable to Two-Way Stop Control, All-Way Stop Control, and Roundabouts

| LOS | Average Vehicle Control Delay | Operational Characteristics |
| :---: | :---: | :---: |
| A | <10 seconds | Normally, vehicles on the stop-controlled approach only have to wait up to 10 seconds before being able to clear the intersection. Left-turning vehicles on the uncontrolled street do not have to wait to make their turn. |
| B | 10 to 15 seconds | Vehicles on the stop-controlled approach will experience delays before being able to clear the intersection. The delay could be up to 15 seconds. Left-turning vehicles on the uncontrolled street may have to wait to make their turn. |
| C | 15 to 25 seconds | Vehicles on the stop-controlled approach can expect delays in the range of 15 to 25 seconds before clearing the intersection. Motorists may begin to take chances due to the long delays, thereby posing a safety risk to through traffic. Left-turning vehicles on the uncontrolled street will now be required to wait to make their turn causing a queue to be created in the turn lane. |
| D | 25 to 35 seconds | This is the point at which a traffic signal may be warranted for this intersection. The delays for the stop-controlled intersection are not considered to be excessive. The length of the queue may begin to block other public and private access points. |
| E | 35 to 50 seconds | The delays for all critical traffic movements are considered to be unacceptable. The length of the queues for the stop-controlled approaches as well as the left-turn movements are extremely long. There is a high probability that this intersection will meet traffic signal warrants. The ability to install a traffic signal is affected by the location of other existing traffic signals. Consideration may be given to restricting the accesses by eliminating the left-turn movements from and to the stop-controlled approach. |
| F | >50 seconds | The delay for the critical traffic movements are probably in excess of 100 seconds. The length of the queues are extremely long. Motorists are selecting alternative routes due to the long delays. The only remedy for these long delays is installing a traffic signal or restricting the accesses. The potential for accidents at this intersection are extremely high due to motorist taking more risky chances. If the median permits, motorists begin making two-stage left-turns. |



| Major/Minor | Major1 | Major2 |  |  | Minor2 |  |  |
| :--- | ---: | :--- | :--- | :--- | ---: | ---: | :---: |
| Conflicting Flow All | 312 | 0 | - | 0 | 575 | 309 |  |
| Stage 1 | - | - | - | - | 309 | - |  |
| Stage 2 | - | - | - | - | 266 | - |  |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |  |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |  |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |  |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |  |
| Pot Cap-1 Maneuver | 1248 | - | - | - | 480 | 731 |  |
| $\quad$ Stage 1 | - | - | - | - | 745 | - |  |
| Stage 2 | - | - | - | - | 779 | - |  |
| Platoon blocked, \% |  | - | - | - |  |  |  |
| Mov Cap-1 Maneuver | 1248 | - | - | - | 478 | 731 |  |
| Mov Cap-2 Maneuver | - | - | - | - | 564 | - |  |
| Stage 1 | - | - | - | - | 741 | - |  |
| Stage 2 | - | - | - | - | 779 | - |  |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.2 | 0 | 10.3 |
| HCM LOS |  | $B$ |  |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1248 | - | - | -718 |
| HCM Lane V/C Ratio | 0.005 | - | - | -0.053 |
| HCM Control Delay (s) | 7.9 | - | - | -10.3 |
| HCM Lane LOS | A | - | - | - |
| HCM 95th \%tile Q(veh) | 0 | - | - | - |



| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 368 | 0 | - | 0 | 743 | 368 |
| Stage 1 | - | - | - | - | 368 | - |
| Stage 2 | - | - | - | - | 375 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1191 | - | - | - | 383 | 677 |
| $\quad$ Stage 1 | - | - | - | - | 700 | - |
| Stage 2 | - | - | - | - | 695 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1191 | - | - | - | 376 | 677 |
| Mov Cap-2 Maneuver | - | - | - | - | 487 | - |
| Stage 1 | - | - | - | - | 688 | - |
| Stage 2 | - | - | - | - | 695 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.5 | 0 | 10.9 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1191 | - | - | - | 633 |
| HCM Lane V/C Ratio | 0.017 | - | - | -0.031 |  |
| HCM Control Delay (s) | 8.1 | - | - | -10.9 |  |
| HCM Lane LOS | A | - | - | - | B |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | - | 0.1 |



| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | :--- | :--- | :--- | ---: | ---: |
| Conflicting Flow All | 314 | 0 | - | 0 | 579 | 311 |
| Stage 1 | - | - | - | - | 311 | - |
| Stage 2 | - | - | - | - | 268 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1246 | - | - | - | 477 | 729 |
| $\quad$ Stage 1 | - | - | - | - | 743 | - |
| Stage 2 | - | - | - | - | 777 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1246 | - | - | - | 475 | 729 |
| Mov Cap-2 Maneuver | - | - | - | - | 562 | - |
| Stage 1 | - | - | - | - | 739 | - |
| Stage 2 | - | - | - | - | 777 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.2 | 0 | 10.3 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |
| :--- | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1246 | - | - | -716 |
| HCM Lane V/C Ratio | 0.005 | - | - | -0.053 |
| HCM Control Delay (s) | 7.9 | - | - | -10.3 |
| HCM Lane LOS | A | - | - | - |
| HCM 95th \%ttile Q(veh) | 0 | - | - | - |



| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 372 | 0 | - | 0 | 749 | 372 |
| Stage 1 | - | - | - | - | 372 | - |
| Stage 2 | - | - | - | - | 377 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1186 | - | - | - | 379 | 674 |
| $\quad$ Stage 1 | - | - | - | - | 697 | - |
| Stage 2 | - | - | - | - | 694 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1186 | - | - | - | 373 | 674 |
| Mov Cap-2 Maneuver | - | - | - | - | 485 | - |
| Stage 1 | - | - | - | - | 685 | - |
| Stage 2 | - | - | - | - | 694 | - |


| Approach | EB | WB | SB |
| :--- | ---: | ---: | ---: |
| HCM Control Delay, s | 0.4 | 0 | 10.9 |
| HCM LOS |  |  | B |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1186 | - | - | - | 631 |
| HCM Lane V/C Ratio | 0.017 | - | - | -0.031 |  |
| HCM Control Delay (s) | 8.1 | - | - | -10.9 |  |
| HCM Lane LOS | A | - | - | - | B |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | - | 0.1 |




| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay，s／veh 4.6 |  |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 4 | 「 | ${ }^{*}$ | $\uparrow$ |  |  | ${ }_{4}$ | 「゙ |  | ＊ |  |
| Traffic Vol，veh／h | 17 | 266 | 90 | 41 | 294 | 1 | 107 | 2 | 45 | 3 | 2 | 14 |
| Future Vol，veh／h | 17 | 266 | 90 | 41 | 294 | 1 | 107 | 2 | 45 | 3 | 2 | 14 |
| Conflicting Peds，\＃／hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | － | － | None | － | － | None | － | － | None | － | － | None |
| Storage Length | 140 | － | 100 | 100 | － | － | － | － | 0 | － | － | － |
| Veh in Median Storage，\＃ |  | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Grade，\％ | － | 0 | － | － | 0 | － | － | 0 | － | － | 0 | － |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles，\％ | 2 | 2 | 4 | 4 | 2 | 2 | 4 | 4 | 4 | 2 | 4 | 2 |
| Mvmt Flow | 19 | 302 | 102 | 47 | 334 | 1 | 122 | 2 | 51 | 3 | 2 | 16 |




| Major/Minor | Major1 |  | Major2 |  | Minor2 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Conflicting Flow All | 324 | 0 | 0 | 0 | 597 | 321 |
| Stage 1 | - |  | - - | - | 321 | - |
| Stage 2 | - |  | - - | - | 276 | - |
| Critical Hdwy | 4.12 |  | - - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - |  | - - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - - | - | 3.518 | 3.318 |
| Pot Cap-1 Maneuver | 1236 | - | - - | - | 466 | 720 |
| Stage 1 | - | - | - - | - | 735 | - |
| Stage 2 | - | - | - - | - | 771 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1236 | - | - | - | 464 | 720 |
| Mov Cap-2 Maneuver | - | - | - - | - | 554 | - |
| Stage 1 | - | - | - - | - | 731 | - |
| Stage 2 | - | - | - - | - | 771 | - |
|  |  |  |  |  |  |  |
| Approach | EB |  | WB |  | SB |  |
| HCM Control Delay, s | 0.2 |  | 0 |  | 10.4 |  |
| HCM LOS |  |  |  |  | B |  |
|  |  |  |  |  |  |  |
| Minor Lane/Major Mvmt |  | EBL | EBT | WBT WBR SBLn1 |  |  |
| Capacity (veh/h) |  | 1236 | - | - | - | 707 |
| HCM Lane V/C Ratio |  | 0.005 | 5 | - | - | 0.054 |
| HCM Control Delay (s) |  | 7.9 | 9 | - | - | 10.4 |
| HCM Lane LOS |  | A | A | - | - | B |
| HCM 95th \%tile Q(veh) |  | 0 | 0 | - | - | 0.2 |



| Major/Minor | Major1 | Major2 |  | Minor2 |  |  |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Conflicting Flow All | 384 | 0 | - | 0 | 773 | 384 |
| Stage 1 | - | - | - | - | 384 | - |
| Stage 2 | - | - | - | - | 389 | - |
| Critical Hdwy | 4.12 | - | - | - | 6.42 | 6.22 |
| Critical Hdwy Stg 1 | - | - | - | - | 5.42 | - |
| Critical Hdwy Stg 2 | - | - | - | - | 5.42 | - |
| Follow-up Hdwy | 2.218 | - | - | -3.518 | 3.318 |  |
| Pot Cap-1 Maneuver | 1174 | - | - | - | 367 | 664 |
| $\quad$ Stage 1 | - | - | - | - | 688 | - |
| Stage 2 | - | - | - | - | 685 | - |
| Platoon blocked, \% |  | - | - | - |  |  |
| Mov Cap-1 Maneuver | 1174 | - | - | - | 361 | 664 |
| Mov Cap-2 Maneuver | - | - | - | - | 475 | - |
| Stage 1 | - | - | - | - | 676 | - |
| Stage 2 | - | - | - | - | 685 | - |


| Approach | EB | WB | SB |
| :--- | :---: | :---: | :---: |
| HCM Control Delay, s | 0.4 | 0 | 11 |
| HCM LOS |  | $B$ |  |


| Minor Lane/Major Mvmt | EBL | EBT | WBT | WBR SBLn1 |  |
| :--- | ---: | ---: | ---: | ---: | ---: |
| Capacity (veh/h) | 1174 | - | - | -620 |  |
| HCM Lane V/C Ratio | 0.017 | - | - | -0.032 |  |
| HCM Control Delay (s) | 8.1 | - | - | - | 11 |
| HCM Lane LOS | A | - | - | - | B |
| HCM 95th \%tile Q(veh) | 0.1 | - | - | - | 0.1 |


| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 5.2 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{1}$ | 4 | 「 | ${ }^{7}$ | $\uparrow$ |  |  | $\uparrow$ | 「 |  | \& |  |
| Traffic Vol, veh/h | 5 | 204 | 164 | 67 | 245 | 5 | 116 | 2 | 57 | 2 | 2 | 30 |
| Future Vol, veh/h | 5 | 204 | 164 | 67 | 245 | 5 | 116 | 2 | 57 | 2 | 2 | 30 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control Frest | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 140 | - | 100 | 100 | - | - | - | - | 0 | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 2 | 2 | 20 | 20 | 2 | 2 | 20 | 20 | 20 | 2 | 20 | 2 |
| Mvmt Flow | 6 | 232 | 186 | 76 | 278 | 6 | 132 | 2 | 65 | 2 | 2 | 34 |



| Intersection |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Int Delay, s/veh | 9.5 |  |  |  |  |  |  |  |  |  |  |  |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | 「 | ${ }^{7}$ | $\uparrow$ |  |  | $\uparrow$ | 「 |  | \& |  |
| Traffic Vol, veh/h | 17 | 276 | 123 | 69 | 304 | 1 | 147 | 2 | 65 | 3 | 2 | 14 |
| Future Vol, veh/h | 17 | 276 | 123 | 69 | 304 | 1 | 147 | 2 | 65 | 3 | 2 | 14 |
| Conflicting Peds, \#/hr | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Sign Control | Free | Free | Free | Free | Free | Free | Stop | Stop | Stop | Stop | Stop | Stop |
| RT Channelized | - | - | None | - | - | None | - | - | None | - | - | None |
| Storage Length | 140 | - | 100 | 100 | - | - | - | - | 0 | - | - | - |
| Veh in Median Storage, \# | \# | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Grade, \% | - | 0 | - | - | 0 | - | - | 0 | - | - | 0 | - |
| Peak Hour Factor | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 | 88 |
| Heavy Vehicles, \% | 2 | 2 | 20 | 20 | 2 | 2 | 20 | 20 | 20 | 2 | 20 | 2 |
| Mvmt Flow | 19 | 314 | 140 | 78 | 345 | 1 | 167 | 2 | 74 | 3 | 2 | 16 |



|  | 4 | $\rightarrow$ | $\cdots$ |  |  | 4 | 4 | $\dagger$ | $p$ | ( |  | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{7}$ | 4 | F | ${ }^{7}$ | $\uparrow$ |  |  | * | 「 |  | \$ |  |
| Traffic Volume (vph) | 17 | 276 | 123 | 69 | 304 | 1 | 147 | 2 | 65 | 3 | 2 | 14 |
| Future Volume (vph) | 17 | 276 | 123 | 69 | 304 | 1 | 147 | 2 | 65 | 3 | 2 | 14 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 140 |  | 100 | 100 |  | 0 | 0 |  | 0 | 0 |  | 0 |
| Storage Lanes | 1 |  | 1 | 1 |  | 0 | 0 |  | 1 | 0 |  | 0 |
| Taper Length (ft) | 25 |  |  | 25 |  |  | 25 |  |  | 25 |  |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  |  | 0.850 |  |  |  |  |  | 0.850 |  | 0.899 |  |
| Flt Protected | 0.950 |  |  | 0.950 |  |  |  | 0.953 |  |  | 0.993 |  |
| Satd. Flow (prot) | 1770 | 1863 | 1346 | 1504 | 1863 | 0 | 0 | 1509 | 1346 | 0 | 1634 | 0 |
| Flt Permitted | 0.554 |  |  | 0.577 |  |  |  | 0.714 |  |  | 0.962 |  |
| Satd. Flow (perm) | 1032 | 1863 | 1346 | 914 | 1863 | 0 | 0 | 1131 | 1346 | 0 | 1583 | 0 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  |  | 134 |  |  |  |  |  | 71 |  | 15 |  |
| Link Speed (mph) |  | 65 |  |  | 65 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 1490 |  |  | 1465 |  |  | 936 |  |  | 1270 |  |
| Travel Time (s) |  | 15.6 |  |  | 15.4 |  |  | 21.3 |  |  | 28.9 |  |
| Peak Hour Factor | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 | 0.92 |
| Heavy Vehicles (\%) | 2\% | 2\% | 20\% | 20\% | 2\% | 2\% | 20\% | 20\% | 20\% | 2\% | 20\% | 2\% |
| Adj. Flow (vph) | 18 | 300 | 134 | 75 | 330 | 1 | 160 | 2 | 71 | 3 | 2 | 15 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 18 | 300 | 134 | 75 | 331 | 0 | 0 | 162 | 71 | 0 | 20 | 0 |
| Enter Blocked Intersection | No | No | No | No | No | No | No | No | No | No | No | No |
| Lane Alignment | Left | Left | Right | Left | Left | Right | Left | Left | Right | Left | Left | Right |
| Median Width(ft) |  | 12 |  |  | 12 |  |  | 0 |  |  | 0 |  |
| Link Offset(ft) |  | 0 |  |  | 0 |  |  | 0 |  |  | 0 |  |
| Crosswalk Width(ft) |  | 16 |  |  | 16 |  |  | 16 |  |  | 16 |  |
| Two way Left Turn Lane |  |  |  |  | Yes |  |  |  |  |  |  |  |
| Headway Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Turning Speed (mph) | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 | 15 |  | 9 |
| Number of Detectors | 1 | 2 | 1 | 1 | 2 |  | 1 | 2 | 1 | 1 | 2 |  |
| Detector Template | Left | Thru | Right | Left | Thru |  | Left | Thru | Right | Left | Thru |  |
| Leading Detector (ft) | 20 | 100 | 20 | 20 | 100 |  | 20 | 100 | 20 | 20 | 100 |  |
| Trailing Detector (ft) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Detector 1 Position(ft) | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 |  |
| Detector 1 Size(ft) | 20 | 6 | 20 | 20 | 6 |  | 20 | 6 | 20 | 20 | 6 |  |
| Detector 1 Type | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex |  | $\mathrm{Cl}+\mathrm{Ex}$ | Cl+Ex | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ | $\mathrm{Cl}+\mathrm{Ex}$ |  |
| Detector 1 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 1 Extend (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Detector 1 Queue (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Detector 1 Delay (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Detector 2 Position(ft) |  | 94 |  |  | 94 |  |  | 94 |  |  | 94 |  |
| Detector 2 Size(ft) |  | 6 |  |  | 6 |  |  | 6 |  |  | 6 |  |
| Detector 2 Type |  | $\mathrm{Cl}+\mathrm{Ex}$ |  |  | Cl+Ex |  |  | Cl+Ex |  |  | Cl+Ex |  |
| Detector 2 Channel |  |  |  |  |  |  |  |  |  |  |  |  |
| Detector 2 Extend (s) |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 |  |
| Turn Type | Perm | NA | Perm | Perm | NA |  | Perm | NA | Perm | Perm | NA |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |



3: Site Access/Ute Lane \& Highway 50

|  | * | $\rightarrow$ | 7 | $\checkmark$ | $\downarrow$ | $\dagger$ | 1 | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | NBT | NBR | SBT |
| Lane Group Flow (vph) | 18 | 300 | 134 | 75 | 331 | 162 | 71 | 20 |
| v/c Ratio | 0.03 | 0.24 | 0.14 | 0.12 | 0.26 | 0.72 | 0.22 | 0.06 |
| Control Delay | 6.4 | 6.8 | 1.7 | 6.9 | 7.0 | 48.5 | 8.4 | 14.4 |
| Queue Delay | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Delay | 6.4 | 6.8 | 1.7 | 6.9 | 7.0 | 48.5 | 8.4 | 14.4 |
| Queue Length 50th (ft) | 3 | 53 | 0 | 12 | 59 | 77 | 0 | 2 |
| Queue Length 95th (ft) | 12 | 115 | 21 | 37 | 128 | 142 | 31 | 19 |
| Internal Link Dist (ft) |  | 1410 |  |  | 1385 | 856 |  | 1190 |
| Turn Bay Length (ft) | 140 |  | 100 | 100 |  |  |  |  |
| Base Capacity (vph) | 697 | 1259 | 953 | 617 | 1259 | 332 | 445 | 475 |
| Starvation Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Spillback Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Storage Cap Reductn | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Reduced v/c Ratio | 0.03 | 0.24 | 0.14 | 0.12 | 0.26 | 0.49 | 0.16 | 0.04 |
| Intersection Summary |  |  |  |  |  |  |  |  |

## ROUNDABOUT OPERATIONAL ANALYSIS MEMO

050A \& Access B Gunnison, CO

## CDOT REGION 3

## September 2021



Prepared by:
Mark Lenters, P.E., and Jay VonAhsen
Kimley-Horn and Associates, Inc.
4582 South Ulster Street, Suite 1500
Denver, CO 80237

Prepared for: CDOT Region 3 Traffic and Safety Unit
September 03, 2021

## Kimley»)Horn

## PROPOSED ROUNDABOUT

Location: 050A \& Access B, Gunnison, CO, MP 158.50
Traffic Volume Source: Gunnison Rising Access Points A and B Traffic Impact Analysis (TIA) prepared by LSC Transportation Consultants, Inc. dated February 25, 2021
Analysis Parameters: $\quad$ Truck Percentages $=2 \%$ (all movements)
Peak Hour Factor (PHF) $=0.90$

## Design Parameters:

Table 1

| PARAMETER | Single-lane Roundabout |
| :--- | :---: |
| Approach road half-width, ft | 12.0 |
| Entry width, ft (effective width, not physical width) | 13.0 |
| Effective flare length, ft | 65.0 |
| Entry radius, ft | Varies, $65-85$ |
| Inscribed circle diameter, ft | 130 |
| PHI - Conflict (entry) angle, deg | 25.0 |
| Splitter Island Length from ICD, ft (along Hwy 50) | 350 |
| Nominal widths on approaches (FOC to FOC), ft | 18.0 |
| Circulating Width, ft | 20.0 |
| Design Vehicle | WB-67 |

## Notes:

1. The splitter island length along Hwy 50 has been increased from a typical high-speed approach value of 200 ft to 350 ft to account for the 65 mph posted speed limit. This additional splitter island length assists with the transitional zone where approaching motorist speed is being slowed down via the use of horizontal curvature and the introduction of a physical raised divider (the splitter island). Superelevation within 500 ft of the ICD of the roundabout should be prohibited to ensure driver eye height maintains a constant visual of roadway surface along the approach to the roundabout.
2. The intersection's average daily volume is well below the typical threshold of a single-lane roundabout daily capacity of 20,000 to $25,000 \mathrm{vpd}$. This level of daily traffic converted to peak hour traffic would not be foreseen to create any type of capacity constraint for the proposed single-lane roundabout scenario.

## Kimley»)Horn

## Results:

Table 2 - Year 2041 Roundabout Capacity Analysis

| MODEL |  | EAST LEG <br> - WB <br> Approach | NORTH <br> LEG - SB <br> Approach | WEST <br> LEG - EB <br> Approach | SOUTH LEG - <br> Northbound <br> Approach | OVERALL <br> INTERSECTION |
| :--- | :--- | :---: | :---: | :---: | :---: | :---: |
| Arcady | AM Peak | $5.8(\mathrm{~A})$ | $4.8(\mathrm{~A})$ | $6.0(\mathrm{~A})$ | $5.0(\mathrm{~A})$ | $5.7(\mathrm{~A})$ |
|  | PM Peak | $6.4(\mathrm{~A})$ | $4.9(\mathrm{~A})$ | $6.2(\mathrm{~A})$ | $5.5(\mathrm{~A})$ | $6.1(\mathrm{~A})$ |
| HCM 6 | AM Peak | $9.1(\mathrm{~A})$ | $9.6(\mathrm{~A})$ | $8.1(\mathrm{~A})$ | $5.6(\mathrm{~A})$ | $8.6(\mathrm{~A})$ |
|  | PM Peak | $13.8(\mathrm{~B})$ | $8.5(\mathrm{~A})$ | $11.2(\mathrm{~B})$ | $9.4(\mathrm{~A})$ | $11.8(\mathrm{~B})$ |

## Right-of-Way:

Approximate right-of-way boundaries have been sketched on Exhibit 1.0 based on the Gunnison County Map Viewer tool sourced from https://gis.gunnisoncounty.org/default map.aspx. The southern leg of the proposed roundabout would assume to be provided with sufficient ROW width at the time the adjacent development files its plat documents.


Above: 130 ft ICD roundabout southern leg. Red line represents ROW boundary traced from the Gunnison County Map Viewer database.

# Kimley»)Horn 

## Sight Distance:



Above: Eastbound view near the proposed roundabout intersection (Source: Google Earth)
The longitudinal grade of Hwy 50 is relatively flat adjacent to the proposed intersection location. The topography to the north is steeply upward and to the south is steeply downward. Associated vertical sight distance checks will be important during the engineering phase to maintain reciprocal sight distance for motorists and stopping sight distance for approaching, circulating, and exiting vehicles.

## Conclusion:

it is recommended a single-lane roundabout be further considered at the subject intersection by performing right-of-way boundary survey and preliminary engineering design to determine if other limiting factors may be present at this location.

## Kimley»)Horn

## Methodology:

The anticipated capacity of the proposed roundabout intersection was analyzed using Junctions 10 roundabout design and capacity analysis software. Two models were created and analyzed to compare a range of predicted capacity based on an empirical model (Arcady) and the current U.S. roundabout capacity model (HCM $6^{\text {th }}$ Edition).

Arcady (Assessment of Roundabout Capacity and Delay) is a roundabout capacity model based on U.K. empirical research into geometry-capacity relationships. The findings on capacity performance for U.S. roundabouts to-date and our experience suggests a reduction in the Arcady capacity assumed for modeling this type of intersection as a roundabout is appropriate. The Arcady analysis includes a capacity equation reduction of $10 \%$ for the design year (2041) analysis. Since Arcady is an empirical data-based model, design parameters have been assigned to analyze the roundabout concept design. The parameters in Table 1 were assigned to the Concept Design (Exhibit 1.0 Appendix A) as well as the Arcady roundabout capacity model.

## APPENDIX A:

## Exhibit 1.0 - Roundabout Concept Design <br> Exhibit 1.1 - Fastest Path Speed Performance Checks Exhibit 1.2 - AutoTURN® Truck Turning Paths





# Kimley»Horn 

## APPENDIX B:

## Design Year Traffic Volumes (Year 2041)

# Kimley»Horn 

## APPENDIX C:

Roundabout Capacity Analysis Report (Arcady model)


Filename: Location \#2 Gunnison Arcady Model Year 2041 Traffic.j10
Path: \KKimley-Horn.comISE_ATLIATL_Roadway\000 ROUNDABOUTSI2021ICDOTICDOT Feasibility Studies 102 50A New Int Gunnisonl01_C̄ALCS
Report generation date: 9/3/2021 10:15:44 AM

```
"2041, AM
"2041, PM
```


## Summary of intersection performance

|  | AM |  |  |  |  |  |  |  |  | PM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Set <br> ID | $\begin{gathered} \text { Q } \\ (\text { Veh }) \end{gathered}$ | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay <br> (s) | V/C | LOS | Int Del <br> (s) | Int LOS | Res Cap | Set ID | $\underset{\text { (Veh) }}{\text { Q }}$ | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | V/C | LOS | Int Del (s) | Int LOS | Res Cap |
|  | 2041 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Leg 1 | D1 | 0.6 | 2.1 | 5.77 | 0.38 | A | 5.68 | A | $\begin{gathered} 112 \\ \% \\ {[\mathrm{Leg}} \\ 3] \end{gathered}$ | D2 | 0.7 | 2.7 | 6.35 | 0.42 | A | 6.07 | A | $\begin{gathered} 92 \\ \% \\ {\left[\begin{array}{c} \text { [eg } \\ 1] \end{array}\right.} \end{gathered}$ |
| Leg 2 |  | 0.1 | 0.5 | 4.79 | 0.05 | A |  |  |  |  | 0.0 | 0.5 | 4.89 | 0.03 | A |  |  |  |
| Leg 3 |  | 0.7 | 1.9 | 6.03 | 0.43 | A |  |  |  |  | 0.8 | 2.4 | 6.19 | 0.44 | A |  |  |  |
| Leg 4 |  | 0.3 | 1.2 | 4.95 | 0.22 | A |  |  |  |  | 0.4 | 1.1 | 5.47 | 0.26 | A |  |  |  |

There are warnings associated with one or more model runs - see the 'Data Errors and Warnings' tables for each Analysis or Demand Set.
$V$ Values shown are the highest values encountered over all time segments. Delay is the maximum value of $A v$. delay per arriving vehicle. Int $L O S$ and Int Del are demand-weighted Av.s. Res Cap indicates the amount by which network flow could be increased before a user-definable threshold (see Analysis Options) is met.

## File summary

File Description

| Title |  |
| :--- | :--- |
| Location |  |
| Site number |  |
| Date | $8 / 12 / 2021$ |
| Version |  |
| Status | (new file) |
| Identifier |  |
| Client |  |
| Jobnumber |  |
| Analyst | KIMLEY-HORN\Jay.VonAhsen |
| Description |  |

## Units

| Distance units | Speed units | Traffic units input | Traffic units results | Flow units | Av. delay units | Total delay units | Rate of delay units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ft | mph | Veh | Veh | perHour | s | -Min | perMin |

## Analysis Options

| Vehicle length (ft) | $\begin{gathered} \text { Calculate } \\ Q \\ \text { Percentiles } \end{gathered}$ | Calculate detailed queueing delay | Show lane queues in feet / metres | Show all PICADY stream intercepts | Calculate residual capacity | Residual capacity criteria type | V/C <br> Threshold | Av. Delay threshold (s) | Q threshold (PCE) | Use iterations with HCM roundabouts | Max number of iterations for roundabouts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 18.86 | $\checkmark$ |  |  |  | $\checkmark$ | Delay | 0.85 | 36.00 | 20.00 |  | 500 |

## Demand Set Summary

| ID | Scenario <br> name | Time Period <br> name | Traffic profile <br> type | Start time <br> (HH:mm) | Finish time <br> (HH:mm) | Time segment length <br> (min) | Run <br> automatically |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 2041 | AM | PHF | $08: 00$ | $09: 00$ | 15 | $\checkmark$ |
| D2 | 2041 | PM | ONE HOUR | $17: 00$ | $18: 30$ | 15 | $\checkmark$ |

## Analysis Set Details

| ID | Include in report | Network flow scaling factor (\%) | Network capacity scaling factor (\%) |
| :---: | :---: | :---: | :---: |
| A1 | $\checkmark$ | 100.000 | 100.000 |

## 2041, AM

Data Errors and Warnings

| Severity | Area | Item | Description |
| :---: | :---: | :---: | :---: |
| Warning | Queue variations | Analysis Options | Q percentiles may be unreliable if the mean queue in any time segment is very low or very high. |

## Intersection Network

## Intersections

| Intersection | Name | Intersection type | Use circulating lanes | Leg order | Int Del (s) | Int LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | untitled | Standard Roundabout |  | $1,2,3,4$ | 5.68 | A |

## Intersection Network

| Driving side | Lighting | Res Cap (\%) | First leg reaching threshold | Network delay (s) | Network LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Right | Normal/unknown | 112 | Leg 3 | 5.68 | A |

## Legs

## Legs

| Leg | Name | Description | No yield line |
| :---: | :---: | :--- | :--- |
| $\mathbf{1}$ | untitled |  |  |
| 2 | untitled |  |  |
| 3 | untitled |  |  |
| 4 | untitled |  |  |

Roundabout Geometry

| Leg | V (ft) | E (ft) | I' (ft) | R (ft) | D (ft) | PHI (deg) | Entry only | Exit only |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 12.00 | 13.00 | 65.0 | 75.0 | 130.0 | 25.0 |  |  |
| $\mathbf{2}$ | 12.00 | 13.00 | 65.0 | 64.0 | 130.0 | 25.0 |  |  |
| $\mathbf{3}$ | 12.00 | 13.00 | 65.0 | 84.0 | 130.0 | 25.0 |  |  |
| $\mathbf{4}$ | 12.00 | 13.00 | 65.0 | 65.0 | 130.0 | 25.0 |  |  |

## Slope / Intercept / Capacity

Leg Intercept Adjustments

| Leg | Type | Reason | Intercept Adj (\%) |
| :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | Percentage |  | 90.00 |
| $\mathbf{2}$ | Percentage |  | 90.00 |
| $\mathbf{3}$ | Percentage |  | 90.00 |
| $\mathbf{4}$ | Percentage |  | 90.00 |

Roundabout Slope and Intercept used in model

| Leg | Final slope | Final intercept (PCE/hr) |
| :---: | :---: | :---: |
| $\mathbf{1}$ | 0.555 | 1102 |
| $\mathbf{2}$ | 0.551 | 1094 |
| $\mathbf{3}$ | 0.557 | 1107 |
| $\mathbf{4}$ | 0.551 | 1095 |

The slope and intercept shown above include any corrections and adjustments.

## Traffic Demand

Demand Set Details

| ID | Scenario <br> name | Time Period <br> name | Traffic profile <br> type | Start time <br> (HH:mm) | Finish time <br> (HH:mm) | Time segment length <br> (min) | Run <br> automatically |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 2041 | AM | PHF | $08: 00$ | $09: 00$ | 15 | $\checkmark$ |


| Vehicle mix varies over turn | Vehicle mix varies over entry | Vehicle mix source | PCE Factor for a Truck (PCE) |
| :---: | :---: | :---: | :---: |
| $\checkmark$ | $\checkmark$ | Truck \%s | 2.00 |

Demand overview (Traffic)

| Leg | Linked leg | Profile type | Use O-D data | Av. Demand (Veh/hr) | Scaling Factor (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ |  | PHF | $\checkmark$ | 317 | 100.000 |
| $\mathbf{2}$ |  | PHF | $\checkmark$ | 34 | 100.000 |
| $\mathbf{3}$ |  | PHF | $\checkmark$ | 373 | 100.000 |
| $\mathbf{4}$ |  | PHF | $\checkmark$ | 175 | 100.000 |

## Peak Hour Factor Data (Traffic)

| Leg | Hourly volume (Veh/hr) | Peak hour factor | Peak time segment |
| :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 317 | 0.84 | SecondQuarter |
| $\mathbf{2}$ | 34 | 0.84 | SecondQuarter |
| $\mathbf{3}$ | 373 | 0.84 | SecondQuarter |
| $\mathbf{4}$ | 175 | 0.84 | SecondQuarter |

## Origin-Destination Data

Demand (Veh/hr)

|  | To |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ |
|  | $\mathbf{1}$ | 0 | 5 | 245 | 67 |
|  | $\mathbf{2}$ | 2 | 0 | 30 | 2 |
|  | $\mathbf{3}$ | 204 | 5 | 0 | 164 |
|  | $\mathbf{4}$ | 57 | $\mathbf{2}$ | 116 | 0 |

## Vehicle Mix

Truck \%s

|  | To |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ |
|  | $\mathbf{1}$ | 2 | 2 | 2 | 2 |
|  | $\mathbf{2}$ | 2 | 2 | 2 | 2 |
|  | $\mathbf{3}$ | 2 | 2 | 2 | 2 |
|  | $\mathbf{4}$ | 2 | 2 | 2 | 2 |

## Results

Results Summary for whole modelled period

| Leg | Max V/C | Max Delay (s) | Max Q (Veh) | Max Q95 (Veh) | Max LOS | Av. Demand <br> (Veh/hr) | Total Intersection <br> Arrivals (Veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.38 | 5.77 | 0.6 | 2.1 | A | 317 | 317 |
|  |  |  |  |  |  |  |  |


| $\mathbf{2}$ | 0.05 | 4.79 | 0.1 | 0.5 | A | 34 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{3}$ | 0.43 | 6.03 | 0.7 | 1.9 | A | 373 |
| $\mathbf{4}$ | 0.22 | 4.95 | 0.3 | 1.2 | A | 373 |

## Main Results for each time segment

08:00-08:15

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) | Capacity (Veh/hr) | V/C | Throughput (Veh/hr) | Throughput (exit) (Veh/hr) | Start queue (Veh) | End queue (Veh) | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 277 | 69 | 107 | 1021 | 0.271 | 275 | 228 | 0.0 | 0.4 | 4.817 | A |
| 2 | 30 | 7 | 372 | 868 | 0.034 | 30 | 10 | 0.0 | 0.0 | 4.294 | A |
| 3 | 326 | 81 | 62 | 1051 | 0.310 | 324 | 340 | 0.0 | 0.4 | 4.940 | A |
| 4 | 153 | 38 | 183 | 972 | 0.157 | 152 | 202 | 0.0 | 0.2 | 4.385 | A |

08:15-08:30

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) | Capacity (Veh/hr) | V/C | Throughput (Veh/hr) | $\begin{aligned} & \text { Throughput } \\ & \text { (exit) } \\ & \text { (Veh/hr) } \end{aligned}$ | Start queue (Veh) | End queue (Veh) | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 377 | 94 | 146 | 999 | 0.378 | 376 | 312 | 0.4 | 0.6 | 5.772 | A |
| 2 | 40 | 10 | 508 | 793 | 0.051 | 40 | 14 | 0.0 | 0.1 | 4.786 | A |
| 3 | 444 | 111 | 84 | 1038 | 0.428 | 443 | 464 | 0.4 | 0.7 | 6.035 | A |
| 4 | 208 | 52 | 251 | 935 | 0.223 | 208 | 277 | 0.2 | 0.3 | 4.948 | A |

08:30-08:45

| Leg | Total <br> Demand <br> (Veh/hr) | Intersection <br> Arrivals <br> (Veh) | Circulating <br> flow <br> $(V e h / h r)$ | Capacity <br> (Veh/hr) | V/C | Throughput <br> (Veh/hr) | Throughput <br> (exit) <br> (Veh/hr) | Start <br> queue <br> (Veh) | End <br> queue <br> (Veh) | Delay <br> (s) | Unsignalised <br> level of <br> service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 337 | 84 | 131 | 1008 | 0.335 | 338 | 280 | 0.6 | 0.5 | 5.374 | A |
| $\mathbf{2}$ | 36 | 9 | 456 | 822 | 0.044 | 36 | 13 | 0.1 | 0.0 | 4.585 | A |
| $\mathbf{3}$ | 397 | 99 | 76 | 1043 | 0.380 | 397 | 416 | 0.7 | 0.6 | 5.579 | A |
| $\mathbf{4}$ | 186 | 47 | 225 | 950 | 0.196 | 186 | 248 | 0.3 | 0.2 | 4.717 | A |

08:45-09:00

| Leg | Total <br> Demand <br> (Veh/hr) | Intersection <br> Arrivals <br> (Veh) | Circulating <br> flow <br> (Veh/hr) | Capacity <br> (Veh/hr) | V/C | Throughput <br> (Veh/hr) | Throughput <br> $(\mathbf{e x i t})$ <br> $(\mathbf{V e h} / \mathbf{h r})$ | Start <br> queue <br> (Veh) | End <br> queue <br> (Veh) | Delay <br> (s) | Unsignalised <br> level of <br> service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 277 | 69 | 108 | 1021 | 0.271 | 277 | 230 | 0.5 | 0.4 | 4.845 | A |
| $\mathbf{2}$ | 30 | 7 | 374 | 866 | 0.034 | 30 | 10 | 0.0 | 0.0 | 4.302 | A |
| $\mathbf{3}$ | 326 | 81 | 62 | 1051 | 0.310 | 326 | 342 | 0.6 | 0.5 | 4.974 | A |
| $\mathbf{4}$ | 153 | 38 | 185 | 972 | 0.157 | 153 | 204 | 0.2 | 0.2 | 4.398 | A |

## Q Variation Results for each time segment

08:00-08:15

| Leg | Mean <br> (Veh) | Q05 <br> (Veh) | Q50 <br> (Veh) | Q90 <br> (Veh) | Q95 <br> (Veh) | Percentile <br> message | Marker <br> message | Probability of reaching or <br> exceeding marker | Probability of exactly <br> reaching marker |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.37 | 0.00 | 0.00 | 0.37 | 0.37 |  |  | N/A |  |
| $\mathbf{2}$ | 0.04 | 0.03 | 0.25 | 0.45 | 0.48 |  |  | N/A |  |
| $\mathbf{3}$ | 0.45 | 0.00 | 0.00 | 0.45 | 0.45 |  |  | N/A | N/A |
| $\mathbf{4}$ | 0.19 | 0.00 | 0.00 | 0.19 | 0.19 |  |  | N/A | N/A |

08:15-08:30

| Leg | Mean <br> (Veh) | Q05 <br> (Veh) | Q50 <br> (Veh) | Q90 <br> (Veh) | Q95 <br> (Veh) | Percentile <br> message | Marker <br> message | Probability of reaching or <br> exceeding marker | Probability of exactly <br> reaching marker |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |


| $\mathbf{1}$ | 0.60 | 0.03 | 0.25 | 0.60 | 0.60 |  |  | N/A | N/A |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $\mathbf{2}$ | 0.05 | 0.03 | 0.26 | 0.46 | 0.49 |  |  | N/A | N/A |
| $\mathbf{3}$ | 0.74 | 0.03 | 0.26 | 0.74 | 0.74 |  |  | N/A | N/A |
| $\mathbf{4}$ | 0.28 | 0.03 | 0.25 | 0.46 | 0.48 |  |  | N/A | N/A |

08:30-08:45

| Leg | Mean <br> (Veh) | Q05 <br> (Veh) | Q50 <br> (Veh) | Q90 <br> (Veh) | Q95 <br> (Veh) | Percentile <br> message | Marker <br> message | Probability of reaching or <br> exceeding marker | Probability of exactly <br> reaching marker |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.51 | 0.03 | 0.29 | 0.98 | 2.15 |  |  | N/A |  |
| $\mathbf{2}$ | 0.05 | 0.00 | 0.00 | 0.05 | 0.05 |  |  | N/A |  |
| $\mathbf{3}$ | 0.62 | 0.03 | 0.28 | 0.62 | 1.95 |  |  | N/A | N/A |
| $\mathbf{4}$ | 0.25 | 0.03 | 0.29 | 0.78 | 1.15 |  |  | N/A |  |

08:45-09:00

| Leg | Mean <br> (Veh) | Q05 <br> (Veh) | Q50 <br> (Veh) | Q90 <br> (Veh) | Q95 <br> (Veh) | Percentile <br> message | Marker <br> message | Probability of reaching or <br> exceeding marker | Probability of exactly <br> reaching marker |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.37 | 0.00 | 0.00 | 0.37 | 0.37 |  |  | N/A | N/A |
| $\mathbf{2}$ | 0.04 | 0.00 | 0.00 | 0.04 | 0.04 |  |  | N/A | N/A |
| $\mathbf{3}$ | 0.45 | 0.00 | 0.00 | 0.45 | 0.45 |  |  | N/A | N/A |
| $\mathbf{4}$ | 0.19 | 0.00 | 0.00 | 0.19 | 0.19 |  |  | N/A | N/A |

## 2041, PM

Data Errors and Warnings

| Severity | Area | Item |  |
| :---: | :---: | :---: | :---: |
| Warning | Queue variations | Analysis Options | Q percentiles may be unreliable if the mean queue in any time segment is very low or very high. |

## Intersection Network

## Intersections

| Intersection | Name | Intersection type | Use circulating lanes | Leg order | Int Del (s) | Int LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | untitled | Standard Roundabout |  | $1,2,3,4$ | 6.07 | A |

## Intersection Network

| Driving side | Lighting | Res Cap (\%) | First leg reaching threshold | Network delay (s) | Network LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Right | Normal/unknown | 92 | Leg 1 | 6.07 | A |

## Traffic Demand

Demand Set Details

| ID | Scenario <br> name | Time Period <br> name | Traffic profile <br> type | Start time <br> (HH:mm) | Finish time <br> (HH:mm) | Time segment length <br> (min) | Run <br> automatically |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D2 | 2041 | PM | ONE HOUR | $17: 00$ | $18: 30$ | 15 | $\checkmark$ |


| Vehicle mix varies over turn | Vehicle mix varies over entry | Vehicle mix source | PCE Factor for a Truck (PCE) |
| :---: | :---: | :---: | :---: |
| $\checkmark$ | $\checkmark$ | Truck \%s | 2.00 |

Demand overview (Traffic)

| Leg | Linked leg | Profile type | Use O-D data | Av. Demand (Veh/hr) | Scaling Factor (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ |  | ONE HOUR | $\checkmark$ | 374 | 100.000 |
| $\mathbf{2}$ |  | ONE HOUR | $\checkmark$ | 19 | 100.000 |
| $\mathbf{3}$ |  | ONE HOUR | $\checkmark$ | 416 | 100.000 |
| $\mathbf{4}$ |  | ONE HOUR | $\checkmark$ | 214 | 100.000 |

## Origin-Destination Data

Demand (Veh/hr)

|  | To |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ |
|  | $\mathbf{1}$ | 0 | 1 | 304 | 69 |
|  | $\mathbf{2}$ | 3 | 0 | 14 | 2 |
|  | $\mathbf{3}$ | 276 | 17 | 0 | 123 |
|  | $\mathbf{4}$ | 65 | 2 | 147 | 0 |

## Vehicle Mix

Truck \%s
$\square$

|  | To |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| From |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ |  |
|  | $\mathbf{1}$ | 2 | 2 | 2 | 2 |  |
|  | $\mathbf{2}$ | 2 | 2 | 2 | 2 |  |
|  | $\mathbf{3}$ | 2 | 2 | 2 | 2 |  |
|  | $\mathbf{4}$ | 2 | 2 | 2 | 2 |  |

## Results

Results Summary for whole modelled period

| Leg | Max V/C | Max Delay (s) | Max Q (Veh) | Max Q95 (Veh) | Max LOS | Av. Demand <br> (Veh/hr) | Total Intersection <br> Arrivals (Veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.42 | 6.35 | 0.7 | 2.7 | A | 343 |  |
| $\mathbf{2}$ | 0.03 | 4.89 | 0.0 | 0.5 | A | 17 |  |
| $\mathbf{3}$ | 0.44 | 6.19 | 0.8 | 2.4 | $A$ | 26 |  |
| $\mathbf{4}$ | 0.26 | 5.47 | 0.4 | 1.1 | $A$ | 382 |  |

## Main Results for each time segment

17:00-17:15

| Leg | Total <br> Demand <br> $($ Veh/hr) | Intersection <br> Arrivals <br> (Veh) | Circulating <br> flow <br> $($ Veh/hr) | Capacity <br> $($ Veh/hr) | V/C | Throughput <br> $($ (Veh/hr) | Throughput <br> $(\mathbf{e x i t})$ <br> $($ Veh/hr) | Start <br> queue <br> $($ Veh $)$ | End <br> queue <br> (Veh) | Delay <br> $(\mathbf{s})$ | Unsignalised <br> level of <br> service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 282 | 70 | 124 | 1011 | 0.278 | 280 | 258 | 0.0 | 0.4 | 4.913 | A |
| $\mathbf{2}$ | 14 | 4 | 389 | 858 | 0.017 | 14 | 15 | 0.0 | 0.0 | 4.266 | A |
| $\mathbf{3}$ | 313 | 78 | 55 | 1054 | 0.297 | 312 | 348 | 0.0 | 0.4 | 4.836 | A |
| $\mathbf{4}$ | 161 | 40 | 222 | 951 | 0.169 | 160 | 145 | 0.0 | 0.2 | 4.547 | A |

17:15-17:30

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) | Capacity (Veh/hr) | V/C | Throughput (Veh/hr) | Throughput (exit) (Veh/hr) | Start queue (Veh) | End queue <br> (Veh) | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 336 | 84 | 149 | 998 | 0.337 | 336 | 309 | 0.4 | 0.5 | 5.436 | A |
| 2 | 17 | 4 | 467 | 815 | 0.021 | 17 | 18 | 0.0 | 0.0 | 4.509 | A |
| 3 | 374 | 93 | 66 | 1048 | 0.357 | 373 | 417 | 0.4 | 0.5 | 5.328 | A |
| 4 | 192 | 48 | 266 | 927 | 0.208 | 192 | 174 | 0.2 | 0.3 | 4.898 | A |

17:30-17:45

| Leg | Total <br> Demand <br> (Veh/hr) | Intersection <br> Arrivals <br> (Veh) | Circulating <br> flow <br> (Veh/hr) | Capacity <br> (Veh/hr) | V/C | Throughput <br> (Veh/hr) | Throughput <br> $(\mathbf{e x i t )}$ <br> $(\mathbf{V e h} / \mathbf{h r})$ | Start <br> queue <br> (Veh) | End <br> queue <br> (Veh) | Delay <br> (s) | Unsignalised <br> level of <br> service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 412 | 103 | 182 | 979 | 0.421 | 411 | 378 | 0.5 | 0.7 | 6.327 | A |
| $\mathbf{2}$ | 21 | 5 | 571 | 758 | 0.028 | 21 | 22 | 0.0 | 0.0 | 4.884 | A |
| $\mathbf{3}$ | 458 | 115 | 81 | 1040 | 0.440 | 457 | 511 | 0.5 | 0.8 | 6.167 | A |
| $\mathbf{4}$ | 236 | 59 | 325 | 894 | 0.264 | 235 | 213 | 0.3 | 0.4 | 5.462 | A |

17:45-18:00

| Leg | Total <br> Demand <br> (Veh/hr) | Intersection <br> Arrivals <br> (Veh) | Circulating <br> flow <br> (Veh/hr) | Capacity <br> (Veh/hr) | V/C | Throughput <br> (Veh/hr) | Throughput <br> (exit) <br> (Veh/hr) | Start <br> queue <br> (Veh) | End <br> queue <br> (Veh) | Delay <br> (s) | Unsignalised <br> level of <br> service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 412 | 103 | 183 | 979 | 0.421 | 412 | 379 | 0.7 | 0.7 | 6.347 | A |
| $\mathbf{2}$ | 21 | 5 | 573 | 757 | 0.028 | 21 | 22 | 0.0 | 0.0 | 4.888 | A |
| $\mathbf{3}$ | 458 | 115 | 81 | 1040 | 0.441 | 458 | 512 | 0.8 | 0.8 | 6.187 | A |
| $\mathbf{4}$ | 236 | 59 | 326 | 894 | 0.264 | 236 | 214 | 0.4 | 0.4 | 5.469 | A |

18:00-18:15

| Leg | Total <br> Demand <br> (Veh/hr) | Intersection <br> Arrivals <br> (Veh) | Circulating <br> flow <br> (Veh/hr) | Capacity <br> (Veh/hr) | V/C | Throughput <br> (Veh/hr) | Throughput <br> (exit) <br> (Veh/hr) | Start <br> queue <br> (Veh) | End <br> queue <br> (Veh) | Delay <br> (s) | Unsignalised <br> level of <br> service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 336 | 84 | 150 | 997 | 0.337 | 337 | 310 | 0.7 | 0.5 | 5.458 | A |
| $\mathbf{2}$ | 17 | 4 | 469 | 814 | 0.021 | 17 | 18 | 0.0 | 0.0 | 4.514 | A |
| $\mathbf{3}$ | 374 | 93 | 67 | 1048 | 0.357 | 375 | 419 | 0.8 | 0.6 | 5.356 | A |
| $\mathbf{4}$ | 192 | 48 | 267 | 926 | 0.208 | 193 | 175 | 0.4 | 0.3 | 4.911 | A |

18:15-18:30

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) | Capacity <br> (Veh/hr) | V/C | Throughput (Veh/hr) | Throughput (exit) (Veh/hr) | Start queue (Veh) | End queue (Veh) | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 282 | 70 | 125 | 1011 | 0.279 | 282 | 259 | 0.5 | 0.4 | 4.944 | A |
| 2 | 14 | 4 | 392 | 857 | 0.017 | 14 | 15 | 0.0 | 0.0 | 4.274 | A |
| 3 | 313 | 78 | 56 | 1054 | 0.297 | 314 | 351 | 0.6 | 0.4 | 4.867 | A |
| 4 | 161 | 40 | 223 | 950 | 0.170 | 161 | 146 | 0.3 | 0.2 | 4.563 | A |

Q Variation Results for each time segment

17:00-17:15

| Leg | Mean <br> (Veh) | Q05 <br> (Veh) | Q50 <br> (Veh) | Q90 <br> (Veh) | Q95 <br> (Veh) | Percentile <br> message | Marker <br> message | Probability of reaching or <br> exceeding marker | Probability of exactly <br> reaching marker |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.38 | 0.00 | 0.00 | 0.38 | 0.38 |  |  | N/A |  |
| $\mathbf{2}$ | 0.02 | 0.00 | 0.00 | 0.02 | 0.02 |  |  | N/A |  |
| $\mathbf{3}$ | 0.42 | 0.00 | 0.00 | 0.42 | 0.42 |  |  | N/A | N/A |
| $\mathbf{4}$ | 0.20 | 0.00 | 0.00 | 0.20 | 0.20 |  |  | N/A | N/A |

17:15-17:30

| Leg | Mean <br> (Veh) | Q05 <br> (Veh) | Q50 <br> (Veh) | Q90 <br> (Veh) | Q95 <br> (Veh) | Percentile <br> message | Marker <br> message | Probability of reaching or <br> exceeding marker | Probability of exactly <br> reaching marker |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.50 | 0.50 | 1.00 | 1.40 | 1.45 |  |  | N/A |  |
| $\mathbf{2}$ | 0.02 | 0.02 | 0.25 | 0.45 | 0.48 |  |  | N/A |  |
| $\mathbf{3}$ | 0.55 | 0.55 | 1.00 | 1.40 | 1.45 |  |  | N/A | N/A |
| $\mathbf{4}$ | 0.26 | 0.00 | 0.00 | 0.26 | 0.26 |  |  | N/A | N/A |

17:30-17:45

| Leg | Mean <br> (Veh) | Q05 <br> (Veh) | Q50 <br> (Veh) | Q90 <br> (Veh) | Q95 <br> (Veh) | Percentile <br> message | Marker <br> message | Probability of reaching or <br> exceeding marker | Probability of exactly <br> reaching marker |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.72 | 0.03 | 0.26 | 0.72 | 0.72 |  |  | N/A | N/A |
| $\mathbf{2}$ | 0.03 | 0.00 | 0.00 | 0.03 | 0.03 |  |  | N/A | N/A |
| $\mathbf{3}$ | 0.78 | 0.03 | 0.26 | 0.78 | 0.78 |  |  | N/A | N/A |
| $\mathbf{4}$ | 0.35 | 0.03 | 0.25 | 0.46 | 0.48 |  |  | N/A | N/A |

17:45-18:00

| Leg | Mean <br> (Veh) | Q05 <br> (Veh) | Q50 <br> (Veh) | Q90 <br> (Veh) | Q95 <br> (Veh) | Percentile <br> message | Marker <br> message | Probability of reaching or <br> exceeding marker | Probability of exactly <br> reaching marker |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.72 | 0.03 | 0.28 | 0.74 | 2.67 |  |  | N/A |  |
| $\mathbf{2}$ | 0.03 | 0.00 | 0.00 | 0.03 | 0.03 |  |  | N/A |  |
| $\mathbf{3}$ | 0.78 | 0.03 | 0.28 | 0.78 | 2.43 |  |  | N/A | N/A |
| $\mathbf{4}$ | 0.36 | 0.03 | 0.32 | 1.08 | 1.08 |  |  | N/A | N/A |

18:00-18:15

| Leg | Mean <br> (Veh) | Q05 <br> (Veh) | Q50 <br> (Veh) | Q90 <br> (Veh) | Q95 <br> (Veh) | Percentile <br> message | Marker <br> message | Probability of reaching or <br> exceeding marker | Probability of exactly <br> reaching marker |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.51 | 0.51 | 1.00 | 1.40 | 1.45 |  |  | N/A |  |
| $\mathbf{2}$ | 0.02 | 0.00 | 0.00 | 0.02 | 0.02 |  |  | N/A |  |
| $\mathbf{3}$ | 0.56 | 0.55 | 1.00 | 1.40 | 1.45 |  |  | N/A |  |
| $\mathbf{4}$ | 0.26 | 0.00 | 0.00 | 0.26 | 0.26 |  |  | N/A | N/A |

Page 10 of 10
18:15-18:30

| Leg | Mean <br> (Veh) | Q05 <br> (Veh) | Q50 <br> (Veh) | Q90 <br> (Veh) | Q95 <br> (Veh) | Percentile <br> message | Marker <br> message | Probability of reaching or <br> exceeding marker | Probability of exactly <br> reaching marker |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.39 | 0.00 | 0.00 | 0.39 | 0.39 |  |  | N/A | N/A |
| $\mathbf{2}$ | 0.02 | 0.00 | 0.00 | 0.02 | 0.02 |  |  | N/A | N/A |
| $\mathbf{3}$ | 0.43 | 0.00 | 0.00 | 0.43 | 0.43 |  |  | N/A | N/A |
| $\mathbf{4}$ | 0.21 | 0.00 | 0.00 | 0.21 | 0.21 |  |  | N/A | N/A |

# Kimley»Horn 

## APPENDIX D:

Roundabout Capacity Analysis Report (HCM 6 model)


Filename: Location \#2 Gunnison HCM Model Year 2041 Traffic.j10
Path: \KKimley-Horn.comISE_ATLIATL_Roadway1000 ROUNDABOUTSI2021ICDOTICDOT Feasibility Studies 102 50A New Int Gunnisonl01_C̄ALCS
Report generation date: 9/3/2021 10:16:56 AM

```
"2041, AM
"2041, PM
```


## Summary of intersection performance

|  | AM |  |  |  |  |  |  |  |  | PM |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Set <br> ID | $\begin{gathered} Q \\ \text { (Veh) } \end{gathered}$ | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | V/C | LOS | Int Del (s) | Int LOS | Res Cap | Set <br> ID | $\begin{gathered} \mathbf{Q} \\ \text { (Veh) } \end{gathered}$ | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | V/C | LOS | Int Del (s) | Int LOS | Res Cap |
|  | 2021 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Leg 1 | D1 |  | 3.3 | 9.06 | 0.54 | A | 8.64 | A | $\begin{gathered} 58 \\ \% \\ {\left[\begin{array}{c} \text { Leg } \\ 2] \end{array}\right.} \end{gathered}$ | D2 |  | 5.0 | 13.80 | 0.65 | B | 11.76 | B | $\begin{gathered} 28 \\ \% \\ {[\mathrm{Leg}} \\ \text { 1] } \end{gathered}$ |
| Leg 2 |  |  | 1.4 | 9.59 | 0.33 | A |  |  |  |  |  | 0.9 | 8.47 | 0.23 | A |  |  |  |
| Leg 3 |  |  | 3.0 | 8.06 | 0.51 | A |  |  |  |  |  | 5.4 | 11.22 | 0.66 | B |  |  |  |
| Leg 4 |  |  | 0.1 | 5.61 | 0.05 | A |  |  |  |  |  | 0.8 | 9.41 | 0.22 | A |  |  |  |

There are warnings associated with one or more model runs - see the 'Data Errors and Warnings' tables for each Analysis or Demand Set.
 Del are demand-weighted Av.s. Res Cap indicates the amount by which network flow could be increased before a user-definable threshold (see Analysis Options) is met.

## File summary

File Description

| Title |  |
| :--- | :--- |
| Location |  |
| Site number |  |
| Date | $8 / 12 / 2021$ |
| Version |  |
| Status | (new file) |
| Identifier |  |
| Client |  |
| Jobnumber |  |
| Analyst | KIMLEY-HORN\Jay.VonAhsen |
| Description |  |

## Units

| Distance units | Speed units | Traffic units input | Traffic units results | Flow units | Av. delay units | Total delay units | Rate of delay units |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ft | mph | Veh | Veh | perHour | s | -Min | perMin |

## Analysis Options

| Vehicle length (ft) | $\begin{gathered} \text { Calculate } \\ \mathbf{Q} \\ \text { Percentiles } \end{gathered}$ | Calculate detailed queueing delay | Show lane queues in feet/ metres | Show all PICADY stream intercepts | Calculate residual capacity | Residual capacity criteria type | V/C <br> Threshold | Av. Delay threshold (s) | Q threshold (PCE) | Use iterations with HCM roundabouts | Max number of iterations for roundabouts |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 18.86 | $\checkmark$ |  |  |  | $\checkmark$ | Delay | 0.85 | 36.00 | 20.00 | $\checkmark$ | 500 |

HCM Calibration

| HCM Calibration | Lane type | Num circulating lanes | Num exit lanes | A | B |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Single lane | 1 |  | 1380.00 | -0.00102 |
| 2 | Single lane | 2 |  | 1420.00 | -0.00085 |
| 3 | Nearside | 1 |  | 1420.00 | -0.00091 |
| 4 | Nearside | 2 |  | 1420.00 | -0.00085 |
| 5 | Offside | 1 |  | 1420.00 | -0.00091 |
| 6 | Offside | 2 |  | 1350.00 | -0.00092 |
| 7 | Yielding bypass |  | 1 | 1380.00 | -0.00102 |
| 8 | Yielding bypass |  | 2 | 1420.00 | -0.00085 |
| 9 | Non-yielding bypass |  | 1 | 99999.00 | 0.00000 |

## Demand Set Summary

| ID | Scenario <br> name | Time Period <br> name | Traffic profile <br> type | Start time <br> (HH:mm) | Finish time <br> (HH:mm) | Time segment length <br> (min) | Run <br> automatically |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 2021 | AM | PHF | $08: 00$ | $09: 00$ | 15 | $\checkmark$ |
| D2 | 2021 | PM | PHF | $17: 00$ | $18: 00$ | 15 | $\checkmark$ |

## Analysis Set Details

| ID | Include in report | Network flow scaling factor (\%) | Network capacity scaling factor (\%) |
| :---: | :---: | :---: | :---: |
| A1 | $\checkmark$ | 100.000 | 100.000 |

## 2041, AM

Data Errors and Warnings

| Severity | Area | Item | Description |
| :--- | :--- | :--- | :--- |
| Warning | HCM Model | D1-2021, AM | Demand Set 1: HCM models are most typically used with PHF traffic flow profiles and single time <br> segments. Use of HCM models with other flow profiles is at the user's own risk |
| Warning | HCM Model |  | One or more intersections use HCM methodologies. These methods are not associated with <br> TRL. The user should apply judgement when interpreting the results. |
| Warning | Queue variations | Analysis Options | Q percentiles may be unreliable if the mean queue in any time segment is very low or very high. |

## Intersection Network

## Intersections

| Intersection | Name | Intersection type | Use circulating lanes | Leg order | Int Del (s) | Int LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | untitled | HCM Roundabout |  | $1,2,3,4$ | 8.64 | A |

Intersection Network

| Driving side | Lighting | Res Cap (\%) | First leg reaching threshold | Network delay (s) | Network LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Right | Normal/unknown | 58 | Leg 2 | 8.64 | A |

## Legs

## Legs

| Leg | Name | Description |
| :---: | :---: | :--- |
| $\mathbf{1}$ | untitled |  |
| 2 | untitled |  |
| 3 | untitled |  |
| 4 | untitled |  |

HCM Lanes

| Leg | HCM Lane | Lane type | Number of conflicting lanes | Destination legs |
| :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | $\mathbf{1}$ | Single lane | 1 | $1,2,3,4$ |
| $\mathbf{2}$ | $\mathbf{1}$ | Single lane | 1 | $1,2,3,4$ |
| $\mathbf{3}$ | $\mathbf{1}$ | Single lane | 1 | $1,2,3,4$ |
| $\mathbf{4}$ | $\mathbf{1}$ | Single lane | 1 | $1,2,3,4$ |

## Traffic Demand

## Demand Set Details

| ID | Scenario <br> name | Time Period <br> name | Traffic profile <br> type | Start time <br> (HH:mm) | Finish time <br> (HH:mm) | Time segment length <br> (min) | Run <br> automatically |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D1 | 2041 | AM | PHF | $08: 00$ | $09: 00$ | 15 | $\checkmark$ |


| Vehicle mix varies over turn | Vehicle mix varies over entry | Vehicle mix source | PCE Factor for a Truck (PCE) |
| :---: | :---: | :---: | :---: |
| $\checkmark$ | $\checkmark$ | Truck \%s | 2.00 |

## Demand overview (Traffic)

| Leg | Linked leg | Profile type | Use O-D data | Av. Demand (Veh/hr) | Scaling Factor (\%) |
| :--- | :--- | :--- | :--- | :--- | :--- |


| $\mathbf{1}$ |  | PHF | $\checkmark$ | 586 | 100.000 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{2}$ |  | PHF | $\checkmark$ | 197 | 100.000 |
| $\mathbf{3}$ |  | PHF | $\checkmark$ | 605 | 100.000 |
| $\mathbf{4}$ |  | PHF | $\checkmark$ | 29 | 100.000 |

## Peak Hour Factor Data (Traffic)

| Leg | Hourly volume (Veh/hr) | Peak hour factor | Peak time segment |
| :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 586 | 0.90 | SecondQuarter |
| $\mathbf{2}$ | 197 | 0.90 | SecondQuarter |
| $\mathbf{3}$ | 605 | 0.90 | SecondQuarter |
| $\mathbf{4}$ | 29 | 0.90 | SecondQuarter |

## Origin-Destination Data

Demand (Veh/hr)

|  | To |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ |
|  | $\mathbf{1}$ | 0 | 4 | 578 | 4 |
|  | $\mathbf{2}$ | 15 | 0 | 180 | 2 |
|  | $\mathbf{3}$ | 485 | 68 | 0 | 52 |
|  | $\mathbf{4}$ | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{2 6}$ | 0 |

## Vehicle Mix

Truck \%s

|  | To |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ |
|  | $\mathbf{1}$ | 2 | 2 | 2 | 2 |
|  | $\mathbf{2}$ | 2 | 2 | 2 | 2 |
|  | $\mathbf{3}$ | 2 | 2 | 2 | 2 |
|  | $\mathbf{4}$ | 2 | 2 | 2 | 2 |

## Results

Results Summary for whole modelled period

| Leg | Max V/C | Max Delay (s) | Max Q95 (Veh) | Max LOS | Av. Demand <br> (Veh/hr) | Total Intersection <br> Arrivals (Veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.54 | 9.06 | 3.3 | A | 586 | 586 |
| $\mathbf{2}$ | 0.33 | 9.59 | 1.4 | A | 197 | 197 |
| $\mathbf{3}$ | 0.51 | 8.06 | 3.0 | A | 605 | 605 |
| $\mathbf{4}$ | 0.05 | 5.61 | 0.1 | A | 29 | 29 |

## Main Results for each time segment

08:00-08:15

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) |  | Capacity <br> (Veh/hr) | V/C | Throughput (Veh/hr) | $\begin{aligned} & \text { Throughput } \\ & \text { (exit) } \\ & \text { (Veh/hr) } \end{aligned}$ | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 543 | 136 | 89 | 0.00 | 1233 | 0.440 | 543 | 464 | 2.3 | 7.390 | A |
| 2 | 182 | 46 | 563 | 0.00 | 753 | 0.242 | 182 | 69 | 0.9 | 7.511 | A |


| $\mathbf{3}$ | 560 | 140 | 19 | 0.00 | 1326 | 0.423 | 560 | 726 | 2.1 | 6.799 | A |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 | 27 | 7 | 526 | 0.00 | 783 | 0.034 | 27 | 54 | 0.1 | 4.934 | A |

08:15-08:30

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) | Ped demand (Ped/hr) | Capacity (Veh/hr) | V/C | Throughput (Veh/hr) | Throughput (exit) (Veh/hr) | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 651 | 163 | 107 | 0.00 | 1211 | 0.538 | 651 | 557 | 3.3 | 9.065 | A |
| 2 | 219 | 55 | 676 | 0.00 | 670 | 0.327 | 219 | 82 | 1.4 | 9.593 | A |
| 3 | 672 | 168 | 23 | 0.00 | 1320 | 0.509 | 672 | 871 | 3.0 | 8.063 | A |
| 4 | 32 | 8 | 631 | 0.00 | 702 | 0.046 | 32 | 64 | 0.1 | 5.607 | A |

08:30-08:45

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) | Ped demand (Ped/hr) | Capacity (Veh/hr) | V/C | Throughput (Veh/hr) | Throughput (exit) (Veh/hr) | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 608 | 152 | 100 | 0.00 | 1220 | 0.498 | 608 | 520 | 2.9 | 8.335 | A |
| 2 | 204 | 51 | 631 | 0.00 | 702 | 0.291 | 204 | 77 | 1.2 | 8.673 | A |
| 3 | 627 | 157 | 22 | 0.00 | 1323 | 0.474 | 627 | 813 | 2.6 | 7.525 | A |
| 4 | 30 | 8 | 589 | 0.00 | 733 | 0.041 | 30 | 60 | 0.1 | 5.326 | A |

08:45-09:00

| Leg | Total <br> Demand <br> (Veh/hr) | Intersection <br> Arrivals <br> (Veh) | Circulating <br> flow <br> (Veh/hr) | Ped <br> demand <br> (Ped/hr) | Capacity <br> (Veh/hr) | V/C | Throughput <br> (Veh/hr) | Throughput <br> (exit) <br> (Veh/hr) | Q95 <br> (Veh) | Delay <br> (s) | Unsignalised <br> level of <br> service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 543 | 136 | 89 | 0.00 | 1233 | 0.440 | 543 | 464 | 2.3 | 7.390 | A |
| $\mathbf{2}$ | 182 | 46 | 563 | 0.00 | 753 | 0.242 | 182 | 69 | 0.9 | 7.511 | A |
| $\mathbf{3}$ | 560 | 140 | 19 | 0.00 | 1326 | 0.423 | 560 | 726 | 2.1 | 6.799 | A |
| $\mathbf{4}$ | 27 | 7 | 526 | 0.00 | 783 | 0.034 | 27 | 54 | 0.1 | 4.934 | A |

## Q Variation Results for each time segment

## HCM: Lane Results

Lane Results: 08:00-08:15

| Leg | HCM <br> Lane | Destination <br> legs | Demand <br> $(\mathbf{V e h} / \mathbf{h r})$ | Throughput <br> $(\mathbf{V e h} / \mathbf{h r})$ | Ped flow <br> $(\mathbf{P e d} / \mathbf{h r})$ | Conflicting flow <br> $(\mathbf{V e h} / \mathbf{h r})$ | Capacity <br> $(\mathbf{V e h} / \mathbf{h r})$ | Q95 <br> $(\mathbf{V e h})$ | Delay <br> $(\mathbf{s})$ | V/C | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | $\mathbf{1}$ | $1,2,3,4$ | 543 | 543 | 0.00 | 89 | 1233 | 2.30 | 7.39 | 0.44 | A |
| $\mathbf{2}$ | $\mathbf{1}$ | $1,2,3,4$ | 182 | 182 | 0.00 | 563 | 753 | 0.95 | 7.51 | 0.24 | A |
| $\mathbf{3}$ | $\mathbf{1}$ | $1,2,3,4$ | 560 | 560 | 0.00 | 19 | 1326 | 2.15 | 6.80 | 0.42 | A |
| $\mathbf{4}$ | $\mathbf{1}$ | $1,2,3,4$ | 27 | 27 | 0.00 | 526 | 783 | 0.11 | 4.93 | 0.03 | A |

Lane Results: 08:15-08:30

| Leg | HCM <br> Lane | Destination legs | Demand (Veh/hr) | Throughput (Veh/hr) | Ped flow (Ped/hr) | Conflicting flow (Veh/hr) | Capacity (Veh/hr) | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay <br> (s) | V/C | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 1, 2, 3, 4 | 651 | 651 | 0.00 | 107 | 1211 | 3.33 | 9.06 | 0.54 | A |
| 2 | 1 | 1, 2, 3, 4 | 219 | 219 | 0.00 | 676 | 670 | 1.42 | 9.59 | 0.33 | A |
| 3 | 1 | 1, 2, 3, 4 | 672 | 672 | 0.00 | 23 | 1320 | 3.00 | 8.06 | 0.51 | A |
| 4 | 1 | 1, 2, 3, 4 | 32 | 32 | 0.00 | 631 | 702 | 0.14 | 5.61 | 0.05 | A |

Lane Results: 08:30-08:45

| Leg | HCM <br> Lane | Destination <br> legs | Demand <br> $(\mathbf{V e h} / \mathbf{h r})$ | Throughput <br> $(\mathbf{V e h} / \mathbf{h r})$ | Ped flow <br> $(\mathbf{( P e d} / \mathbf{h r})$ | Conflicting flow <br> $(\mathbf{V e h} / \mathbf{h r})$ | Capacity <br> $(\mathbf{V e h} / \mathbf{h r})$ | Q95 <br> $(\mathbf{V e h})$ | Delay <br> $(\mathbf{s})$ | V/C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | $\mathbf{1}$ | $1,2,3,4$ | 608 | 608 | 0.00 | 100 | 1220 | 2.87 | 8.34 | 0.50 |
| $\mathbf{L}$ | $\mathbf{1}$ | $1,2,3,4$ | 204 | 204 | 0.00 | 631 | 702 | 1.21 | 8.67 | 0.29 |
| $\mathbf{A}$ |  |  |  |  |  |  |  |  |  |  |
| $\mathbf{3}$ | $\mathbf{1}$ | $1,2,3,4$ | 627 | 627 | 0.00 | 22 | 1323 | 2.63 | 7.53 | 0.47 |
| $\mathbf{4}$ | $\mathbf{1}$ | $1,2,3,4$ | 30 | 30 | 0.00 | 589 | 733 | 0.13 | 5.33 | 0.04 |

Lane Results: 08:45-09:00

| Leg | HCM <br> Lane | Destination <br> legs | Demand <br> $(\mathbf{V e h} / \mathbf{h r})$ | Throughput <br> $(\mathbf{V e h} / \mathbf{h r})$ | Ped flow <br> $(\mathbf{P e d} / \mathbf{h r})$ | Conflicting flow <br> $(\mathbf{V e h} / \mathbf{h r})$ | Capacity <br> $(\mathbf{V e h} / \mathbf{h r})$ | Q95 <br> $(\mathbf{V e h})$ | Delay <br> $(\mathbf{s})$ | V/C |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | $\mathbf{1}$ | $1,2,3,4$ | 543 | 543 | 0.00 | 89 | 1233 | 2.30 | 7.39 | 0.44 |
| $\mathbf{L O S}$ |  |  |  |  |  |  |  |  |  |  |

## 2041, PM

Data Errors and Warnings

| Severity | Area | Item | Description |
| :--- | :--- | :--- | :--- |
| Warning | HCM Model | D2-2021, PM | Demand Set 2: HCM models are most typically used with PHF traffic flow profiles and single time <br> segments. Use of HCM models with other flow profiles is at the user's own risk |
| Warning | HCM Model |  | One or more intersections use HCM methodologies. These methods are not associated with <br> TRL. The user should apply judgement when interpreting the results. |
| Warning | Queue variations | Analysis Options | Q percentiles may be unreliable if the mean queue in any time segment is very low or very high. |

## Intersection Network

## Intersections

| Intersection | Name | Intersection type | Use circulating lanes | Leg order | Int Del (s) | Int LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | untitled | HCM Roundabout |  | $1,2,3,4$ | 11.76 | B |

Intersection Network

| Driving side | Lighting | Res Cap (\%) | First leg reaching threshold | Network delay (s) | Network LOS |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Right | Normal/unknown | 28 | Leg 1 | 11.76 | B |

## Traffic Demand

Demand Set Details

| ID | Scenario <br> name | Time Period <br> name | Traffic profile <br> type | Start time <br> (HH:mm) | Finish time <br> (HH:mm) | Time segment length <br> (min) | Run <br> automatically |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| D2 | 2041 | PM | PHF | $17: 00$ | $18: 00$ | 15 | $\checkmark$ |


| Vehicle mix varies over turn | Vehicle mix varies over entry | Vehicle mix source | PCE Factor for a Truck (PCE) |
| :---: | :---: | :---: | :---: |
| $\checkmark$ | $\checkmark$ | Truck \%s | 2.00 |

## Demand overview (Traffic)

| Leg | Linked leg | Profile type | Use O-D data | Av. Demand (Veh/hr) | Scaling Factor (\%) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ |  | PHF | $\checkmark$ | 553 | 100.000 |
| $\mathbf{2}$ |  | PHF | $\checkmark$ | 134 | 100.000 |
| $\mathbf{3}$ |  | PHF | $\checkmark$ | 793 | 100.000 |
| $\mathbf{4}$ |  | PHF | $\checkmark$ | 112 | 100.000 |

Peak Hour Factor Data (Traffic)

| Leg | Hourly volume (Veh/hr) | Peak hour factor | Peak time segment |
| :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 553 | 0.90 | SecondQuarter |
| $\mathbf{2}$ | 134 | 0.90 | SecondQuarter |
| $\mathbf{3}$ | 793 | 0.90 | SecondQuarter |
| $\mathbf{4}$ | 112 | 0.90 | SecondQuarter |

## Origin-Destination Data

Demand (Veh/hr)
$\square$

| $*$ |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From | $\mathbf{1}$ | 0 | 11 | 539 | 3 |
|  | $\mathbf{2}$ | 10 | 0 | 120 | 4 |
|  | $\mathbf{3}$ | 555 | 201 | 0 | 37 |
|  | $\mathbf{4}$ | 4 | 4 | 104 | 0 |

## Vehicle Mix

Truck \%s

|  | To |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| From |  | $\mathbf{1}$ | $\mathbf{2}$ | $\mathbf{3}$ | $\mathbf{4}$ |
|  | $\mathbf{1}$ | $\mathbf{2}$ | 2 | 2 | 2 |
|  | $\mathbf{2}$ | 2 | 2 | 2 | 2 |
|  | $\mathbf{3}$ | 2 | 2 | 2 | 2 |
|  | $\mathbf{4}$ | 2 | 2 | 2 | 2 |

## Results

Results Summary for whole modelled period

| Leg | Max V/C | Max Delay (s) | Max Q95 (Veh) | Max LOS | Av. Demand <br> (Veh/hr) | Total Intersection <br> Arrivals (Veh) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | 0.65 | 13.80 | 5.0 | B | 553 | 553 |
| $\mathbf{2}$ | 0.23 | 8.47 | 0.9 | A | 134 | 134 |
| $\mathbf{3}$ | 0.66 | 11.22 | 5.4 | B | 793 | 793 |
| $\mathbf{4}$ | 0.22 | 9.41 | 0.8 | A | 112 | 112 |

## Main Results for each time segment

17:00-17:15

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) | Ped demand (Ped/hr) | Capacity (Veh/hr) | V/C | Throughput (Veh/hr) | Throughput (exit) (Veh/hr) | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 512 | 128 | 286 | 0.00 | 1005 | 0.510 | 512 | 527 | 3.0 | 9.796 | A |
| 2 | 124 | 31 | 598 | 0.00 | 726 | 0.171 | 124 | 200 | 0.6 | 6.831 | A |
| 3 | 734 | 184 | 16 | 0.00 | 1331 | 0.552 | 734 | 706 | 3.5 | 8.738 | A |
| 4 | 104 | 26 | 709 | 0.00 | 647 | 0.160 | 104 | 41 | 0.6 | 7.427 | A |

17:15-17:30

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) | Ped demand (Ped/hr) | Capacity (Veh/hr) | V/C | Throughput (Veh/hr) | $\begin{aligned} & \text { Throughput } \\ & \text { (exit) } \\ & \text { (Veh/hr) } \end{aligned}$ | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 614 | 154 | 343 | 0.00 | 947 | 0.649 | 614 | 632 | 5.0 | 13.797 | B |
| 2 | 149 | 37 | 718 | 0.00 | 641 | 0.232 | 149 | 240 | 0.9 | 8.466 | A |
| 3 | 881 | 220 | 19 | 0.00 | 1327 | 0.664 | 881 | 848 | 5.4 | 11.224 | B |
| 4 | 124 | 31 | 851 | 0.00 | 558 | 0.223 | 124 | 49 | 0.8 | 9.407 | A |

17:30-17:45

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) | Ped demand (Ped/hr) | Capacity (Veh/hr) | V/C | Throughput (Veh/hr) | $\begin{aligned} & \text { Throughput } \\ & \text { (exit) } \\ & \text { (Veh/hr) } \end{aligned}$ | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 573 | 143 | 320 | 0.00 | 969 | 0.592 | 573 | 590 | 4.0 | 11.903 | B |
| 2 | 139 | 35 | 670 | 0.00 | 674 | 0.206 | 139 | 224 | 0.8 | 7.756 | A |
|  |  |  |  |  |  |  |  |  |  |  |  |


| $\mathbf{3}$ | 822 | 206 | 18 | 0.00 | 1328 | 0.619 | 822 | 791 | 4.5 | 10.103 | B |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{4}$ | 116 | 29 | 794 | 0.00 | 592 | 0.196 | 116 | 46 | 0.7 | 8.540 | A |

17:45-18:00

| Leg | Total Demand (Veh/hr) | Intersection Arrivals (Veh) | Circulating flow (Veh/hr) | Ped demand (Ped/hr) | Capacity (Veh/hr) | V/C | Throughput (Veh/hr) | $\begin{aligned} & \text { Throughput } \\ & \text { (exit) } \\ & \text { (Veh/hr) } \end{aligned}$ | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | Unsignalised level of service |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 512 | 128 | 286 | 0.00 | 1005 | 0.510 | 512 | 527 | 3.0 | 9.796 | A |
| 2 | 124 | 31 | 598 | 0.00 | 726 | 0.171 | 124 | 200 | 0.6 | 6.831 | A |
| 3 | 734 | 184 | 16 | 0.00 | 1331 | 0.552 | 734 | 706 | 3.5 | 8.738 | A |
| 4 | 104 | 26 | 709 | 0.00 | 647 | 0.160 | 104 | 41 | 0.6 | 7.427 | A |

Q Variation Results for each time segment

## HCM: Lane Results

Lane Results: 17:00-17:15

| Leg | HCM <br> Lane | Destination <br> legs | Demand <br> $(\mathbf{V e h} / \mathbf{h r})$ | Throughput <br> $(\mathbf{V e h} / \mathbf{h r})$ | Ped flow <br> $(\mathbf{P e d} / \mathbf{h r})$ | Conflicting flow <br> $(\mathbf{V e h} / \mathbf{h r})$ | Capacity <br> $(\mathbf{V e h} / \mathbf{h r})$ | Q95 <br> $(\mathbf{V e h})$ | Delay <br> $(\mathbf{s})$ | V/C | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | $\mathbf{1}$ | $1,2,3,4$ | 512 | 512 | 0.00 | 286 | 1005 | 2.97 | 9.80 | 0.51 | A |
| $\mathbf{2}$ | $\mathbf{1}$ | $1,2,3,4$ | 124 | 124 | 0.00 | 598 | 726 | 0.61 | 6.83 | 0.17 | A |
| $\mathbf{3}$ | $\mathbf{1}$ | $1,2,3,4$ | 734 | 734 | 0.00 | 16 | 1331 | 3.52 | 8.74 | 0.55 | A |
| $\mathbf{4}$ | $\mathbf{1}$ | $1,2,3,4$ | 104 | 104 | 0.00 | 709 | 647 | 0.57 | 7.43 | 0.16 | A |

Lane Results: 17:15-17:30

| Leg | HCM <br> Lane | Destination <br> legs | Demand <br> $(\mathbf{V e h} / \mathbf{h r})$ | Throughput <br> $(\mathbf{V e h} / \mathbf{h r})$ | Ped flow <br> $(\mathbf{P e d} / \mathbf{h r})$ | Conflicting flow <br> $(\mathbf{V e h} / \mathbf{h r})$ | Capacity <br> $(\mathbf{V e h} / \mathbf{h r})$ | Q95 <br> $(\mathbf{V e h})$ | Delay <br> $\mathbf{( s )}$ | V/C | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | $\mathbf{1}$ | $1,2,3,4$ | 614 | 614 | 0.00 | 343 | 947 | 4.96 | 13.80 | 0.65 | B |
| $\mathbf{2}$ | $\mathbf{1}$ | $1,2,3,4$ | 149 | 149 | 0.00 | 718 | 641 | 0.89 | 8.47 | 0.23 | A |
| $\mathbf{3}$ | $\mathbf{1}$ | $1,2,3,4$ | 881 | 881 | 0.00 | 19 | 1327 | 5.41 | 11.22 | 0.66 | B |
| $\mathbf{4}$ | $\mathbf{1}$ | $1,2,3,4$ | 124 | 124 | 0.00 | 851 | 558 | 0.85 | 9.41 | 0.22 | A |

Lane Results: 17:30-17:45

| Leg | HCM Lane | Destination legs | Demand (Veh/hr) | Throughput (Veh/hr) | Ped flow (Ped/hr) | Conflicting flow (Veh/hr) | Capacity (Veh/hr) | $\begin{gathered} \text { Q95 } \\ \text { (Veh) } \end{gathered}$ | Delay (s) | V/C | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 1 | 1, 2, 3, 4 | 573 | 573 | 0.00 | 320 | 969 | 4.02 | 11.90 | 0.59 | B |
| 2 | 1 | 1, 2, 3, 4 | 139 | 139 | 0.00 | 670 | 674 | 0.77 | 7.76 | 0.21 | A |
| 3 | 1 | 1, 2, 3, 4 | 822 | 822 | 0.00 | 18 | 1328 | 4.55 | 10.10 | 0.62 | B |
| 4 | 1 | 1, 2, 3, 4 | 116 | 116 | 0.00 | 794 | 592 | 0.72 | 8.54 | 0.20 | A |

Lane Results: 17:45-18:00

| Leg | HCM <br> Lane | Destination <br> legs | Demand <br> $(\mathbf{V e h} / \mathbf{h r})$ | Throughput <br> $(\mathbf{V e h} / \mathbf{h r})$ | Ped flow <br> $(\mathbf{( P e d} / \mathbf{h r})$ | Conflicting flow <br> $(\mathbf{V e h} / \mathbf{h r})$ | Capacity <br> $(\mathbf{V e h} / \mathbf{h r})$ | Q95 <br> $(\mathbf{V e h})$ | Delay <br> $(\mathbf{s})$ | V/C | LOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathbf{1}$ | $\mathbf{1}$ | $1,2,3,4$ | 512 | 512 | 0.00 | 286 | 1005 | 2.97 | 9.80 | 0.51 | A |
| $\mathbf{2}$ | $\mathbf{1}$ | $1,2,3,4$ | 124 | 124 | 0.00 | 598 | 726 | 0.61 | 6.83 | 0.17 | A |
| $\mathbf{3}$ | $\mathbf{1}$ | $1,2,3,4$ | 734 | 734 | 0.00 | 16 | 1331 | 3.52 | 8.74 | 0.55 | A |
| $\mathbf{4}$ | $\mathbf{1}$ | $1,2,3,4$ | 104 | 104 | 0.00 | 709 | 647 | 0.57 | 7.43 | 0.16 | A |

(719) 633-2868

FAX (719) 633-5430
E-mail: Isc@lsces.com
Web Site: http://www.Isccs.com

# Transportation Update Memo 

Date: June 8, 2007<br>To: Tim Seibert, NES<br>From: Christopher McGranahan, P.E., PTOE<br>Project: Gunnison Gateway Annexation<br>LSC \#066650

## UPDATED WEEKDAY TRIP GENERATION

The weekday trip generation table that was included in the December 12, 2006 Traffic Impact Analysis (TIA) is attached along with the updated table for the recently revised land use plan.

## Weekday Traffic

The original trip generation table included in the TIA estimated the site would generate about 34,900 trips on the average weekday. The updated trip generation table estimates the updated land use for the site would generate about 32,150 trips on the average weekday. This results in a decrease of about eight percent.

## Weekday Morning Peak-Hour Traffic

The original trip generation table included in the TIA estimated the site would generate about 2,370 trips during the typical weekday morning peak hour. The updated trip generation table estimates the updated land use for the site would generate about 2,200 trips during the typical weekday morning peak hour. This results in a decrease of more than seven percent.

## Weekday Afternoon Peak-Hour Traffic

The original trip generation table included in the TIA estimated the site would generate about 3,485 trips during the typical weekday afternoon peak hour. The updated trip generation table estimates
the updated land use for the site would generate about 3,190 trips during the typical weekday afternoon peak hour. This results in a decrease of between eight and nine percent.

## Summary of Trip Generation Updates

The proposed single-family home and condo/townhome densities were decreased significantly. This is expected to result in a reduction in weekday traffic of about 3,625 trips per day.

The number of spaces available in the Recreational Vehicle Park was increased from 400 to 500. This is expected to result in an increase in weekday traffic of about 400 trips per day.

The addition of an elementary school is expected to result in an increase in weekday traffic of about 150 trips per day. These would be the trips external to the site.

The Business Park component of the site located in TAZs G and H has increased from about 688,700 square feet to about 716,400 square feet. This is expected to result in an increase in weekday traffic of about 330 trips per day.

## Change in Access To/From the West

The original TIA assumed about 1,250 trips per day would use Escalante Drive to access the core of Gunnison. It assumed about 2,100 trips per day would use Georgia Avenue to access the core of Gunnison. If Western State College has issues with improvements to Escalante Drive or additional traffic on Escalante Drive then the traffic distribution assumed in the TIA will need to be revised appropriately.

Georgia Avenue intersects Escalante Drive west of the proposed site. If Georgia Avenue were to remain the primary non-highway access to/from the west it would be difficult to prevent site traffic from using Escalante Drive as the two streets intersect just west of the site. An option is being explored that would make Virginia Street the primary non-highway access to/from the west. This has several benefits over Georgia Avenue including: the intersection of Virginia Street with State Highway 135 is currently signalized while the intersection of Georgia Avenue with State Highway 135 is two-way stop-sign controlled; Virginia Street does not intersection with Escalante Drive, making Escalante Drive much less attractive to non-college traffic; a single-lane roundabout could be implemented at the intersection of Virginia Street and Adams Street to maintain good traffic operations for both streets near the front door of Western State College; a roundabout could be a nice entry feature for Western State College. One negative for this option is that it will require Virginia Street to be constructed through the currently open land west of Adams Street owned by Western State College.

## Proposed Traffic Volumes on Virginia Street

With Virginia Street as the only non-highway east/west connection to the core of Gunnison, it is expected that the 1,250 weekday trips previously assigned to Escalante Drive and the 2,100 weekday trips previously assigned to Georgia Avenue would redirect to Virginia Street. The total weekday trips that would ultimately impact Virigina is expected to be in the range of 3,500 and 5,000 trips per day. It is expected a significant portion of this site traffic on Virginia Street would distribute north and south on Colorado, which currently serves as a bypass around the downtown core. As various developments are proposed in the site it is recommended the traffic operations be monitored at the intersection of Virginia Street and Colorado to determine if any modifications are needed to the existing traffic control.

## Proposed Access Plan on US Highway 50

The site access intersections on US Highway 50 identified in the original TIA were located partly based on CDOT's requirement of half-mile spacing for full-movement intersections. Review comments from the City of Gunnison and their traffic consultant, Bill Fox, have indicated a desire for two additional site access intersections on the west end of the site to extend the existing street grid found in the core of Gunnison to the west. It is likely CDOT will have issues with these additional access intersections.

CDOT has commented in writing that their agreement to half-mile access spacing was under the assumption that all accesses would be City Streets. They prefer not to grant access rights that only serve a campground, trailhead, business park, commercial, etc. I believe what they would like to see is an east/west road south of US Highway 50 that could connect all or most of the access points locally. If we take the position that this is not possible due to floodplain, ground water, topography, etc., we may have to provide evidence of this to CDOT.

## Street Connection Proposed by Steve Westbay

Steve Westbay with the City of Gunnison has proposed a local roadway connection through the site that would connect US Highway 50 and State Highway 135. This route as drawn would be very difficult to achieve based on the existing topography. The alignment proposed is a relatively direct route and has the feeling of a bypass. This may encourage vehicles accessing Crested Butte from east of Gunnison to bypass a majority of the commercial enterprises in Gunnison. It may be more appropriate to have a less direct route that would serve as more of a local access from the middle to the north end of the site to/from the west.


Table 1a - June 2007
Weekday Trip Generation Estimates - Buildout Gunnison Rising - "Authentically Colorado"


# Gunnison Rising - "Authentically Colorado" Master Plan Level Traffic Impact Analysis 

December 12, 2006



LSC TRANSPORTATION CONSULTANTS, INC.

## 516 North Tejon Street

Colorado Springs, CO 80903
(719) 633-2868

FAX (719) 633-5430
E-mail: Isc@lsces.com
Web Site: http://www.Isces.com

December 12, 2006
Mr. Timothy Seibert
N.E.S., Inc.

508 South Tejon Street
Colorado Springs, Colorado 80903

$$
\begin{array}{ll}
\text { RE: } & \text { Gunnison Rising - "Authentically Colorado" } \\
\text { Master Plan Level } \\
\text { Traffic Impact Analysis Report } \\
\text { Gunnison, Colorado } \\
\text { LSC \#066650 }
\end{array}
$$

Dear Mr. Seibert:
In response to your request, LSC Transportation Consultants, Inc. has prepared this Master Plan level traffic impact analysis report for the proposed Gunnison Rising - "Authentically Colorado"mixed-use development. We trust that the report will assist you in annexing this property into the City of Gunnison. Please contact me if you have any questions or need further assistance.

Sincerely,

# Gunnison Rising - "Authentically Colorado" Master Plan Level Traffic Impact Analysis 

## December 12, 2006

Prepared for:<br>Mr. Timothy Seibert<br>N.E.S., Inc.<br>508 South Tejon Street<br>Colorado Springs, CO 80903<br>(719) 471-0073

Prepared by:
LSC Transportation Consultants, Inc.
516 North Tejon Street
Colorado Springs, CO 80903
(719) 633-2868

## TABLE OF CONTENTS

Section Title Page
EXECUTIVE SUMMARY
Proposed Land Use and Access Plan ..... ES-1
Trip Generation ..... ES-1
Weekday and Saturday Traffic Comparison ..... ES-2
Projected Levels of Service ..... ES-2
Traffic Signal Progression Efficiency ..... ES-2
Recommended Roadway Improvements ..... ES-3
Local Neighborhood Traffic Impacts ..... ES-3
CDOT State Highway Access Permit ..... ES-3
TRAFFIC IMPACT ANALYSIS
A INTRODUCTION ..... 1
B LAND USE AND ACCESS PLAN ..... 3
C AREA ROADWAYS ..... 6
D 2007 EXISTING TRAFFIC VOLUMES ..... 8
E TRIP GENERATION ..... 13
F WEEKDAY AND SATURDAY TRAFFIC COMPARISON ..... 16
Existing Traffic Comparison ..... 16
Trip Generation Comparison ..... 16
Comparison Summary ..... 16
G DIRECTIONAL DISTRIBUTION AND TRIP ASSIGNMENT ..... 17
H 2027 BACKGROUND TRAFFIC ..... 21
I 2027 TOTAL TRAFFIC ..... 24
J PROJECTED LEVELS OF SERVICE, TRAFFIC SIGNAL PROGRESSION EFFICIENCY, AND CDOT PERMITS ..... 27
Projected Levels of Service ..... 27
2027 Background Traffic ..... 27
2027 Total Traffic ..... 28
Traffic Signal Progression Efficiency ..... 29
Local Neighborhood Traffic Impacts ..... 37
CDOT State Highway Access Permit ..... 37
K CONCLUSIONS AND RECOMMENDATIONS ..... 38
Trip Generation ..... 38
Weekday and Saturday Traffic Comparison ..... 38
Projected Levels of Service ..... 38
Traffic Signal Progression Efficiency ..... 39
Recommended Roadway Improvements ..... 39
Local Neighborhood Traffic Impacts ..... 39
CDOT State Highway Access Permit ..... 40
APPENDIX A: Traffic Count Reports
APPENDIX B: Level of Service Reports
APPENDIX C: Time/Space Diagrams

## LIST OF TABULATIONS

Table Title Page
1a Weekday Trip Generation Estimates - Buildout ..... 14
1b Saturday Trip Generation Estimates - Buildout ..... 15
2a Levels of Service, October 2006 Existing Traffic Adjusted Upward to Reflect Peak Summer Traffic ..... 30
2b Levels of Service, 2027 Background Traffic ..... 31
2c Levels of Service, 2027 Total Traffic ..... 32
3 Time Horizon for Improvements ..... 33
4 US Highway 50 Progression Efficiency ..... 36
LIST OF ILLUSTRATIONS
FigureTitlePage
1 Vicinity Map ..... 2
2a Site Plan ..... 4
2b Traffic Analysis Zones ..... 5
3a Existing Traffic ..... 9
3b Existing Traffic ..... 10
3c Projected Summer Existing Traffic, Lane Geometry, Traffic Control and Level of Service ..... 11
3d Projected Summer Existing Traffic, Lane Geometry, Traffic Control and Level of Service ..... 12
4 Directional Distribution ..... 18
5a Buildout Site-Generated Traffic ..... 19
5b Buildout Site-Generated Traffic ..... 20
6a 2027 Background Traffic, Lane Geometry, Traffic Control and Level of Service ..... 22
6b 2027 Background Traffic, Lane Geometry, Traffic Control and Level of Service ..... 23
7a 2027 Total Traffic, Lane Geometry, Traffic Control and Level of Service ..... 25
7b 2027 Total Traffic, Lane Geometry, Traffic Control and Level of Service ..... 26
8a 2027 Total Lane Geometry Along Site Frontage ..... 34
8b 2027 Total Lane Geometry for SH 135 Between Virginia Street and US 50 ..... 35

## Executive Summary



## Executive Summary

LSC Transportation Consultants, Inc. has prepared this Master Plan level traffic impact analysis report for the proposed Gunnison Rising - "Authentically Colorado" mixed-use development located along US Highway 50 (US 50) east of the City of Gunnison, Colorado. The property is proposed for annexation into the City of Gunnison.

## PROPOSED LAND USE AND ACCESS PLAN

Buildout of the property is proposed as approximately 1,012 single-family houses, 628 townhouse/condominium units, 233,400 square feet of shopping center space, 688,700 square feet of business park space, a 400-space recreational vehicle park/campground, and a 20-acre equestrian center.

There are numerous site access intersections proposed to US 50, as well as local site access intersections via Georgia Avenue and Escalante Drive. The locations of these site access intersections are shown on the various report figures.

## TRIP GENERATION

Buildout of the site is projected to generate about 34,895 vehicle-trips during a typical weekday, with about half of the vehicles entering and half of the vehicles exiting the site. During the weekday morning peak hour, about 1,250 vehicles would enter and 1,120 vehicles would exit the site. During the weekday afternoon peak hour, about 1,715 vehicles would enter and 1,765 vehicles would exit the site.

Buildout of the site is projected to generate about 33,390 vehicle-trips during a typical Saturday, with about half of the vehicles entering and half of the vehicles exiting the site. During the Saturday mid-day peak hour, about 1,730 vehicles would enter and 1,485 vehicles would exit the site.

## WEEKDAY AND SATURDAY TRAFFIC COMPARISON

The existing and projected site-generated traffic volumes are expected to be higher during the typical weekday than during the typical Saturday. For this reason, the weekday scenario was analyzed in detail.

## PROJECTED LEVELS OF SERVICE

All of the movements at the analyzed signalized intersections are projected to operate at acceptable levels of service (LOS) during the peak hours through the year 2027 with the recommended roadway improvements. A few of the movements at the analyzed stop-sign controlled intersections are projected to operate at LOS E or F during the peak hours with the recommended roadway improvements. Potential mitigation for these LOS E and F intersections is discussed in the report.

## TRAFFIC SIGNAL PROGRESSION EFFICIENCY

Generally speaking, the proposed traffic signals are fairly well spaced, but some are not within 200 feet of the one-half mile spacing preferred by the Colorado Department of Transportation (CDOT), which requires a progression efficiency analysis. The progression efficiencies on US 50 between New York Street and the proposed Gunnison Rising traffic signals are projected to meet or exceed the CDOT requirement of 35 percent.

The progression efficiencies assumed that the section of US 50 between Adams Street and the Residential Village development will be an extension of the existing five-lane urban cross section to the west, with curb and gutter and a posted speed limit of 45 miles per hour (mph). US 50 is proposed as one through lane in each direction with a rural cross section to the east of the Residential Village development, and with shoulders and roadside ditches. Posting this rural section at either 45 or 65 mph would result in a progression efficiency of approximately 41.5 percent. Posting this rural section at 55 mph would result in a progression efficiency of 35 percent.

## RECOMMENDED ROADWAY IMPROVEMENTS

The roadway improvements required to achieve the projected levels of service shown on Tables $2 \mathrm{a}, 2 \mathrm{~b}$, and 2 c are detailed on Table 3, along with a suggested party responsible for funding each roadway improvement. Figures 8 a and 8 b show the majority of the recommended roadway improvements.

## LOCAL NEIGHBORHOOD TRAFFIC IMPACTS

A majority of the site-generated traffic volume is expected to access the site via US 50. Secondary local site access would be to and from the west via Georgia Avenue and Escalante Drive. Escalante Drive is currently a private college street that has no way to restrict non-college traffic. There is little non-college traffic currently using Escalante Drive due to the layout of the existing street system. With an eastern extension of Georgia, it will be more attractive for non-college traffic to use Escalante Drive as an additional east/west route. If Escalante Drive remains private and unimproved, there will likely be less traffic using Escalante than predicted in this analysis. It is expected that traffic capacity will be adequate on Georgia Avenue to accommodate the projected future traffic with or without improvements to Escalante Drive.

From Georgia Avenue and Escalante Drive, it is expected that the site-generated traffic would use Colorado Street to distribute north and south. The site-generated traffic that has an origin or destination east of State Highway 135 (SH 135) is expected to use the local street grid between Colorado Street and SH 135. The site-generated traffic that has an origin or destination on or west of SH 135 is expected to use Colorado Street to access the existing SH 135 traffic signals at Virginia Street, Denver Street, and Spencer Avenue.

## CDOT STATE HIGHWAY ACCESS PERMIT

It is expected that site specific traffic studies will be completed for the various phases of the project in order to obtain any necessary CDOT State Highway Access Permits.

## Traffic Impact Analysis Report



## SECTION A Introduction

LSC Transportation Consultants, Inc. has prepared this Master Plan level traffic impact analysis report for the proposed Gunnison Rising - "Authentically Colorado" mixed-use development. As shown on Figure 1, the site is located along US Highway 50 (US 50) east of the City of Gunnison, Colorado. The property is proposed for annexation into the City of Gunnison.

This report is being prepared for submittal to the City of Gunnison and the Colorado Department of Transportation (CDOT). The report identifies the development's traffic impacts on the surrounding roadway system, as well as the roadway system improvements needed to mitigate the traffic impacts. The intersections included in the analysis were agreed to by the City of Gunnison and CDOT staff during preliminary discussions. It is expected that site specific traffic studies will be completed for the various phases of the project in order to obtain any necessary CDOT State Highway Access Permits.

The report contains the following: a determination of the existing traffic and roadway conditions in the vicinity of the site including the lane geometries, traffic controls, and levels of service; the projected average weekday, weekday peak-hour, average Saturday, and Saturday peak-hour vehicle-trips to be generated by the site; the assignment of the projected traffic volumes to the surrounding roadway system; a projection of the future background and total traffic volumes on the roadway system for the year 2027; the resulting traffic impacts; and the recommended improvements to the surrounding roadway system.


## Land Use and Access Plan

The existing land use in the vicinity of the site is primarily agricultural.

Figure 2a shows the preliminary site plan and the proposed site access intersections. The various traffic analysis zones (TAZ) are shown in Figure 2b. Buildout of the property is proposed as approximately 1,012 single-family houses, 628 townhouse/condominium units, 233,400 square feet of shopping center space, 688,700 square feet of business park space, a 400-space recreational vehicle park/campground, and a 20 -acre equestrian center.



## Area Roadways

The roadways in the vicinity of the site are shown on Figure 1, and are listed below followed by a brief description.

- US Highway 50 (US 50) is locally known as Tomichi Avenue. US 50 is a major east/west route extending across Colorado. Locally, US 50 extends west to the City of Montrose and east to Monarch Pass. In the vicinity of the site, US 50 is classified as a Regional Highway (RA) by CDOT and has a twolane rural cross section with a posted speed limit of 65 miles per hour (mph). To the west of the site, US 50 is a five-lane urban section through the City of Gunnison with a posted speed limit of 35 mph .
- State Highway $\mathbf{1 3 5}$ (SH 135) is locally known as Main Street. SH 135 is a north/south route extending north from US 50 in the City of Gunnison to the City of Crested Butte. In the City of Gunnison, SH 135 is classified as a Urban Arterial (NRB) by CDOT and has a five-lane urban cross section with a posted speed limit varying from 25 to 40 mph . To the north of the City of Gunnison, SH 135 becomes a two-lane rural cross section classified as a Regional Highway (RA) with a posted speed limit of 55 mph .
- County Road 72 (CR 72) is an existing gravel County Road that loops around to form two three-leg intersections with US 50 east of the City of Gunnison. CR 72 serves a low density rural subdivision, and has relatively low traffic volumes.
- Industrial Park Road is an existing gravel County Road that forms a threeleg intersection with US 50 east of the City of Gunnison. Industrial Park Road has a posted speed limit of 20 mph , and serves a number of existing industrial uses that generate relatively low traffic volumes.
- Adams Street is a local north/south City street on the east side of the City of Gunnison, that provides direct access to the south side of Western State College and an existing McDonalds restaurant. There is no posted speed limit on Adams Street. At US 50, Adams Street is stop-sign controlled with no pavement markings. Adams Street is wide enough that right-turning vehicles are not blocked by the queued vehicles wishing to turn left or go straight. The Pioneer Museum is located on the southeast corner of the US 50/Adams Street intersection.
- Colorado Street is a north/south City street that provides access to the west side of Western State College, and serves as traffic relief for the signalized US 50/SH 135 intersection by providing an alternative connection between

US 50 and SH 135. Colorado Street has a bicycle lane and parallel parking on each side of the street.

- Georgia Avenue is an east/west City street extending through much of the City of Gunnison, with parking on both sides of the street for much of its length. Georgia Avenue's eastern terminus is at Western State College. An existing parking lot will need to be relocated in order to allow Georgia Avenue to extend into the Gunnison Rising site.
- Virginia Street is an east/west City street extending through much of the City of Gunnison, with parking on both sides of the street for much of its length. Virginia Street's eastern terminus is at Loveland Street. An existing park prevents extending Virginia Street into the Gunnison Rising site. Virginia Street has one of the few existing traffic signals on SH 135 north of US 50.
- Escalante Drive is a private college street running along the east and north borders of Western State College. Escalante Drive terminates at Georgia Avenue on the east and Colorado Street on the west. Preliminary discussions have occurred with Western State College representatives regarding roadway improvements to Escalante Drive and converting Escalante Drive to a public street. These roadway improvements and conversion would provide relief for Georgia Avenue and US 50 for the site-generated traffic wishing to travel to and from the west.


## 2007 Existing Traffic Volumes

Figures 3 a and 3 b show the existing peak-hour traffic volumes for the analyzed intersections. The traffic volumes were from traffic counts conducted by LSC in September and October 2006. The traffic count reports are attached in Appendix A.

It was agreed with the City of Gunnison and CDOT staff that a summer peakseason adjustment factor would be needed in order to account for the higher summer traffic volumes seen in the City of Gunnison. The peak-hour traffic counts conducted at the SH 135/Spencer Avenue intersection were compared with the traffic counts conducted at this intersectionduring the year 2006 summer season. The following summer peak-season adjustment factors were developed based on a comparison of these two traffic counts.

- US 50 and SH 135 through traffic: The weekday morning peak-hour traffic volumes were increased by 15 percent. The weekday afternoon peak-hour traffic volumes were increased by 30 percent.
- City street local traffic: The weekday morning peak-hour traffic volumes were increased by about five percent. The weekday afternoon peak-hour traffic volumes were increased by about eight percent. The exception was the local streets adjacent to Western State College, which were not adjusted because the Western State College traffic volumes are much lowerduring the summer months.

Figures 3c and 3d show the estimated summer peak-season traffic volumes for the analyzed intersections based on the traffic counts and the summer peak-season adjustment factors. Figures 3c and 3d also show the existing lane geometries, traffic controls, and levels of service for the analyzed intersections.




TRANSPORTATONN.


Estimates of the traffic volumes expected to be generated by the development have been made using the nationally published trip generation rates found in Trip Generation, 6th Edition, 1997 by the Institute of Transportation Engineers (ITE). Table 1a shows the projected average weekday, weekday morning peak-hour, and weekday afternoon peak-hour vehicle-trips to be generated by the development. Table 1b shows the projected average Saturday and Saturday mid-day peak-hour vehicle-trips to be generated by the development.

Buildout of the site is projected to generate about 34,895 vehicle-trips during a typical weekday, with about half of the vehicles entering and half of the vehicles exiting the site. During the weekday morning peak hour, which typically occurs for one hour between 6:30 and 8:30 a.m., about 1,250 vehicles would enter and 1,120 vehicles would exit the site. During the weekday afternoon peak hour, which typically occurs for one hour between 4:00 and 6:00 p.m., about 1,715 vehicles would enter and 1,765 vehicles would exit the site.

Buildout of the site is projected to generate about 33,390 vehicle-trips during a typical Saturday, with about half of the vehicles entering and half of the vehicles exiting the site. During the Saturday mid-day peak hour, which typically occurs for one hour between 12:00 and 2:00 p.m., about 1,730 vehicles would enter and 1,485 vehicles would exit the site.


Table 1b

## Saturday Trip Generation Estimates - Buildout

 Gunnison Rising - "Authentically Colorado"| TAZ ${ }^{(1)}$ | Land <br> Use <br> Code | Land <br> Use Description | Trip <br> Generation <br> Units | Trip Generation Rates ${ }^{(2)}$ |  |  | Total Trips Generated |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Average <br> Saturday <br> Traffic | Saturday <br> Peak Hour |  | Average <br> Saturday <br> Traffic | Saturday <br> Peak Hour |  |
|  |  |  |  |  | In | Out |  | In | Out |
| A | 210 | Single-Family Detached Housing | 624 DU ${ }^{(3)}$ | 10.09 | 0.51 | 0.43 | 6,296 | 317 | 270 |
| B | 230 | Residential Condominium/Townhouse | 426 DU | 5.67 | 0.25 | 0.22 | 2,415 | 108 | 92 |
| C | 416 | Campground/Recreational Vehicle Park ${ }^{(4)}$ | 400 Occupied Spaces | 6.00 | 0.27 | 0.12 | 2,400 | 108 | 48 |
| D | 210 | Single-Family Detached Housing | 388 DU | 10.09 | 0.51 | 0.43 | 3,915 | 197 | 168 |
| E | 230 | Residential Condominium/Townhouse | 202 DU | 5.67 | 0.25 | 0.22 | 1,145 | 51 | 44 |
|  | 820 | Shopping Center | 174.2 KSF ${ }^{(5)}$ | 66.72 | 3.37 | 3.11 | 11,625 | 588 | 543 |
| F | 820 | Shopping Center | 59.2 KSF | 66.72 | 3.37 | 3.11 | 3,952 | 200 | 184 |
| G | 770 | Business Park ${ }^{(6)}$ | 392.3 KSF | 2.28 | 0.23 | 0.19 | 896 | 89 | 73 |
| H | 770 | Business Park | 296.4 KSF | 2.28 | 0.23 | 0.19 | 677 | 67 | 55 |
| I | - | Equestrian Center ${ }^{(7)}$ | 20 Acres | 3.42 | 0.30 | 0.30 | 68 | 6 | 6 |
|  |  | Buildout Total |  |  |  |  | 33,390 | 1,730 | 1,483 |

## Notes:

(1) TAZ = traffic analysis zone (as shown in Figure 2b)
(2) Source: "Trip Generation, 6th Edition, 1997" by the Institute of Transportation Engineers
(3) DU = dwelling unit
(4) The average Saturday traffic rate was estimated by LSC. The Saturday peak-hour traffic rate was assumed to be the same as the weekday afternoon peak-hour rates.
(5) $\mathrm{KSF}=$ thousand square feet
(6) The peak-hour rates were taken as the ratio of the average Saturday traffic rate to the average weekday and peak-hour rates.
(7) Rates estimated by LSC

## Weekday and Saturday Traffic Comparison

## EXISTING TRAFFIC COMPARISON

The weekday and Saturday peak-hour traffic counts at the SH 135/Spencer Avenue intersection were compared in order to determine which time period had the highest traffic volume. The Saturday SH 135 traffic volumes were found to be approximately 85 percent of the weekday SH 135 traffic volumes. The Saturday Spencer Avenue traffic volumes were found to be approximately 82 percent of the weekday Spencer Avenue traffic volumes.

## TRIP GENERATION COMPARISON

Based on the information provided in Section E, the weekday average daily traffic volumes are approximately 4.5 percent higher than the Saturday average daily traffic volumes. The weekday afternoon peak-hour traffic volumes are approximately 8.5 percent higher than the Saturday mid-day peak-hour traffic volumes.

## COMPARISON SUMMARY

The existing traffic volumes and the projected site-generated traffic volumes are expected to be higher during the typical weekday than during the typical Saturday. For this reason, the weekday scenario was analyzed in detail.

## SECTION G

## Directional Distribution and Trip Assignment

The directional distribution of the traffic volumes to be generated by the site is an important factor in determining the development's traffic impacts. There are many factors that determine the distribution including: the site's location with respect to the residential, employment, and activity centers; the site's location with respect to the balance of the City of Gunnison area; the site's proposed land uses; and the roadway system serving the site.

Figure 4 shows the projected directional distribution for the buildout sitegenerated traffic volumes for the year 2027.

The 2027 buildout site-generated traffic volumes on the adjacent roadway system were determined by applying the 2027 distribution percentages (from Figure 4) to the trip generation estimates (from Table 1a). Figures 5a and 5b show the projected 2027 buildout site-generated traffic volumes.


IRANSPITARANTS, NC.



## SECTION H 2027 Background Traffic

Figures 6 a and 6 b show the background traffic volume estimates for the year 2027. Background traffic is the traffic estimated to be on the adjacent roadway system without consideration of the site-generated traffic volumes. The background traffic volumes include the traffic generated by the surrounding developments and the through traffic on the adjacent roadways.

CDOT required that the access intersections be assumed to serve the area north of US 50 east of the CR 72 east intersection. Two access points were shown north of US 50 aligning with the proposed site access intersections. In order to be conservative, it was assumed that a total of 400 single-family houses would be served by these two off-site access points. If this area develops with a more rural density, the traffic generated would be much less than that shown on Figure 6b.

Figures 6 a and 6 b also show the recommended lane geometries, traffic controls, and levels of service at the analyzed intersections.


TRANSPORTATIONC.
CONSLITANS,


Figures 7a and 7b show the projected total traffic volumes for the year 2027. The 2027 total traffic volumes are the sum of the 2027 buildout site-generated traffic volumes (from Figures 5a and 5b) plus the 2027 background traffic volumes (from Figures 6a and 6b).

Figures 7 a and 7 b also show the recommended lane geometries, traffic controls, and levels of service at the analyzed intersections.



# Projected Levels of Service, Traffic Signal Progression Efficiency, and CDOT Permits 

## PROJECTED LEVELS OF SERVICE

Level of service (LOS) is a quantitative measure of the level of congestion or delay at an intersection. Level of service is indicated on a scale from "A" to "F." LOS A is indicative of very little congestion or delay. LOS F is indicative of a high level of congestion or delay.

The Synchro Version 6 software package was used to project the levels of service for the analyzed intersections. Tables $2 \mathrm{a}, 2 \mathrm{~b}$, and 2 c show the projected levels of service for each of the analyzed time periods. The level of service reports are attached in Appendix B.

The roadway improvements required to achieve the levels of service shown on Tables $2 \mathrm{a}, 2 \mathrm{~b}$, and 2 c are detailed on Table 3, along with a suggested party responsible for funding each roadway improvement. Figures 8 a and $8 b$ show the majority of the recommended roadway improvements.

All of the movements at the analyzed signalized intersections are projected to operate at acceptable levels of service during the peak hours through the year 2027 with the recommended roadway improvements. The following movements at the analyzed stop-sign controlled intersections are projected to operate at LOS E or F during the peak hours with the recommended roadway improvements.

## 2027 Background Traffic

US 50/Adams Street: The northbound approach at the intersection is projected to operate at LOS E (with an average delay of 42 seconds per vehicle) during the afternoon peak hour. The southbound shared left-turn/through movement at this intersection is projected to operate at LOS E (with an average delay of 36 seconds
per vehicle) during the morning peak hour. It is unlikely that the City of Gunnison or CDOT would mitigate the LOS E movement, as it is not excessive.

US 50/Colorado Street: The northbound approach at the intersection is projected to operate at LOS F (with an average delay of 50 seconds per vehicle) during the afternoon peak hour. The southbound shared left-turn/through movement at this intersection is projected to operate at LOS F (with an average delay of 60 seconds per vehicle) during the afternoon peak hour. It is unlikely that the City of Gunnison or CDOT would mitigate the LOS F movement, as it is not excessive.

SH 135/Georgia Avenue: The eastbound approach at the intersection is projected to operate at LOS F (with an average delay of 116 seconds per vehicle) during the afternoon peak hour. The westbound approach at the intersection is projected to operate at LOS E (with an average delay of 50 seconds per vehicle) during the afternoon peak hour. This intersection is not a likely candidate for signalization, due to its proximity to the existing traffic signal at the SH 135/Virginia Street intersection. If the SH 135 /Georgia Ave nue intersection were restricted to a right-in/right-out or three-quarter movement, the intersection is projected to operate at acceptable levels of service. The eastbound and westbound left-turn and through movements at this intersection could be served by the additional capacity available at the SH 135/Virginia Street intersection's traffic signal. Other possible mitigation could include converting the SH 135/Virginia Street intersection to right-in/right-out and signalizing the SH 135/Georgia Avenue intersection.

## 2027 Total Traffic

SH 135/Georgia Avenue: The eastbound approach at the intersection is projected to operate at LOS E (with an average delay of 43 seconds per vehicle) during the morning peak hour and LOS F (with an average delay of over 700 seconds per vehicle) during the afternoon peak hour. The westbound approach at the intersection is projected to operate at LOS E (with an average delay of 35 seconds per vehicle) during the morning peak hour and LOS F (with an average delay of over 400 seconds per vehicle) during the afternoon peak hour. This intersection is not a likely candidate for signalization, due to its proximity to the existing traffic signal at the SH 135/Virginia Street intersection. If the SH 135/Georgia Avenue inter-
section were restricted to a right-in/right-out or three-quarter movement, the intersection is projected to operate at acceptable levels of service. The eastbound and westbound left-turn and through movements at this intersection could be served by the additional capacity available at the SH 135/Virginia Street intersection's traffic signal. Other possible mitigation could include converting the SH 135/Virginia Street intersection to right-in/right-out and signalizing the SH 135/Georgia Avenue intersection.

## TRAFFIC SIGNAL PROGRESSION EFFICIENCY

Generally speaking, the proposed traffic signals are fairly well spaced, but some are not within 200 feet of the one-half mile spacing preferred by CDOT. In this situation, the Colorado State Highway Access Code requires a minimum 35 percent progression efficiency. A traffic signal progression efficiency analysis was conducted for US 50 from New York Street through the proposed Gunnison Rising traffic signals. The time/space diagrams for the traffic signal progression efficiency analysis are attached in Appendix C.

As shown on Table 4, the progression efficiencies on US 50 from New York Street through the proposed Gunnison Rising traffic signals are expected to meet or exceed CDOT's 35 percent requirement.

The progression efficiencies shown on Table 4 assume that the section of US 50 between Adams Street and the Residential Village development will be an extension of the five-lane urban cross section to the west, with curb and gutter and a posted speed limit of 45 mph . US 50 is proposed as one through lane in each direction with a rural cross section to the east of the Residential Village development, and with shoulders and roadside ditches. Posting this rural section at either 45 or 65 mph would result in a progression efficiency of approximately 41.5 percent. Posting this rural section at 55 mph would result in a progression efficiency of 35 percent.

October 2006 Existing Traffic Adjusted Upward to Reflect Peak Summer Traffic

## Gunnison Rising - "Authentically Colorado'

| Intersection | Traffic Control | Peak Hour | Seasonally Adjusted Existing Traffic |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Intersection LOS | EB ${ }^{(1)}$ |  |  | WB |  |  | NB |  |  | SB |  |  |
|  |  |  |  | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |
| US Highway 50/ | Traffic Signal | AM | A | B | B | B | B | B | B | A | A | A | A | A | A |
| New York Street ${ }^{(2)}$ |  | PM | A | B | B | B | B | B | B | A | A | A | A | A | A |
| US Highway 50/ | Traffic Signal | AM | A | A | A | A | A | A | A | C | C | C | C | C | C |
| Spruce Street |  | PM | A | A | A | A | A | A | A | C | C | C | C | C | C |
| US Highway 50/ | Traffic Signal | AM | B | A | A | A | B | B | B | C | C | C | C | B | B |
| State Highway 135 |  | PM | B | B | B | B | B | B | B | C | C | C | B | B | B |
| US Highway 50/ | TWSC ${ }^{(3)}$ | AM | - | A | free | free | A | free | free | C | C | C | C | C | A |
| Colorado Street |  | PM | - | A | free | free | A | free | free | C | C | C | C | C | B |
| US Highway 50/ | TWSC | AM | - | A | free | free | A | free | free | B | B | B | C | C | A |
| Adams Street |  | PM | - | A | free | free | A | free | free | C | C | C | C | C | A |
| US Highway 50/ | AWSC ${ }^{(4)}$ | AM | - | A | free | free | - | free | free | - | - | - | A | - | A |
| County Road 72 West |  | PM | - | A | free | free | - | free | free | - | - | - | A | - | A |
| US Highway 50/ | AWSC | AM | - | A | free | - | - | free | free | - | - | - | A | - | A |
| Best Western Access |  | PM | - | A | free | - | - | free | free | - | - | - | A | - | A |
| US Highway 50/ | AWSC | AM | - | A | free | free | - | free | free | - | - | - | A | - | A |
| County Road 72 East |  | PM | - | A | free | free | - | free | free | - | - | - | A | - | A |
| US Highway 50/ | AWSC | AM | - | - | free | free | A | A | - | B | - | B | - | - | - |
| Industrial Park Road |  | PM | - | - | free | free | A | A | - | B | - | B | - | - | - |
| State Highway 135/ | Traffic Signal | AM | A | C | C | C | C | C | C | A | A | A | A | A | A |
| Virginia Street |  | PM | A | C | C | C | C | C | C | A | A | A | A | A | A |
| State Highway 135/ | TWSC | AM | - | B | B | B | B | B | B | A | free | free | A | free | free |
| Georgia Avenue |  | PM | - | D | D | D | C | C | C | A | free | free | A | free | free |
| State Highway 135/ | Traffic Signal | AM | A | C | C | C | C | C | C | A | A | A | A | A | A |
| Spencer Avenue |  | PM | A | C | C | B | C | C | B | A | A | A | A | A | A |
| Colorado Street/ | AWSC | AM | - | A | A | A | A | A | A | A | A | A | A | A | A |
| Georgia Avenue |  | PM | - | A | A | A | A | A | A | A | A | A | A | A | A |
| Colorado Street/ | AWSC | AM | - | - | - | - | A | - | A | - | A | A | A | A | - |
| Escalante Drive |  | PM | - | - | - | - | A | - | A | - | A | A | A | A | - |

Notes:
(1) $\mathrm{EB}=$ eastbound, $\mathrm{WB}=$ westbound, $\mathrm{NB}=$ northbound, $\mathrm{SB}=$ southbound, $\mathrm{LT}=$ left turn, $\mathrm{TH}=$ through, $\mathrm{RT}=$ right turn
(2) US Highway 50 is oriented north/south and New York Street is oriented east/west at this intersection.
(3) TWSC = two-way stop-sign control
(4) AWSC = all-way stop-sign control

## Table 2b

Levels of Service
2027 Background Traffic
Gunnison Rising - "Authentically Colorado"

| Intersection | Traffic Control | Peak Hour | 2027 Background Traffic |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Intersection | EB ${ }^{(1)}$ |  |  | WB |  |  | NB |  |  | SB |  |  |
|  |  |  | LOS | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |
| US Hlghway 50/ | Traffic Signal | AM | A | B | B | B | B | B | B | A | A | A | A | A | A |
| New York Street ${ }^{(2)}$ |  | PM | A | B | B | B | B | B | B | A | A | A | A | A | A |
| US Highway 50/ | Traffic Signal | AM | A | A | A | A | A | A | A | C | C | C | C | C | C |
| Spruce Street |  | PM | A | A | A | A | A | A | A | c | c | c | c | c | c |
| US Highway 50/ | Traffic Signal | AM | B | A | A | A | B | B | B | C | C | C | C | C | C |
| State Highway 135 |  | PM | C | D | A | A | B | B | B | C | C | C | D | C | C |
| US Highway 50/ | TWSC ${ }^{(3)}$ | AM | - | A | free | free | A | free | free | D | D | D | D | D | B |
| Colorado Street |  | PM | - | A | free | free | A | free | free | $F$ (50.1s) | $F$ (50.1s) | $F$ (50.1s) | $F$ (59.9s) | $F$ (59.9s) | B |
| US Highway 50/ | TWSC | AM | - | A | free | free | A | free | free | D | D | D | E (36.4s) | E (36.4s) | B |
| Adams Street |  | PM | - | A | free | free | A | free | free | E (41.5s) | E (41.5s) | E (41.5s) | D | D | B |
| US Highway 50/ | AWSC ${ }^{(4)}$ | AM | - | A | free | - | - | free | free | - | - | - | B | - | B |
| County Road 72 West |  | PM | - | A | free | - | - | free | free | - | - | - | B | - | B |
| US Highway 50/ | AWSC | AM | - | A | free | - | - | free | free | - | - | - | B | - | B |
| Best Western Access |  | PM | - | A | free | - | - | free | free | - | - | - | B | - | B |
| US Highway 50/ | AWSC | AM | - | A | free | free | - | free | free | - | - | - | B | - | B |
| County Road 72 East |  | PM | - | A | free | free | - | free | free | - | - | - | B | - | B |
| US Highway 50/ | AWSC | AM | - | A | free | - | - | free | free | - | - | - | B | - | B |
| Future West Off-Site Access |  | PM | - | A | free | - | - | free | free | - | - | - | C | - | B |
| US Highway 50/ | AWSC | AM | - | A | free | - | - | free | free | - | - | - | B | - | B |
| Future East Off-Site Access |  | PM | - | A | free | - | - | free | free | - | - | - | C | - | B |
| State Highway 135/ | AWSC | AM | - | - | free | free | A | A | - | B | - | B | - | - | - |
| Industrial Park Road |  | PM | - | - | free | free | A | A | - | B | - | B | - | - | - |
| State Highway 135/ | Traffic Signal | AM | A | C | C | C | C | C | C | A | A | A | A | A | A |
| Virginia Street |  | PM | A | B | B | B | B | B | B | A | A | A | A | A | A |
| State Highway 135/ | TWSC | AM | - | D | D | D | C | C | C | A | free | free | A | free | free |
| Georgia Avenue ${ }^{(5)}$ |  | PM | - | F (116.4s) | $F(116.4 s)$ | F (116.4s) | E (49.6s) | E (49.6s) | E (49.6s) | A | free | free | A | free | free |
| State Highway 135/ | Traffic Signal | AM | A | C | C | B | C | C | B | A | A | A | A | A | A |
| Spencer Avenue |  | PM | A | C | C | B | C | C | B | A | A | A | A | A | A |
| State Highway 135/ | TWSC | AM | - | - | - | B | - | - | B | A | free | free | A | free | free |
| Colorado Street |  | PM | - | - | - | B | - | - | B | B | free | free | A | free | free |
| Colorado Street/ | AWSC | AM | - | A | A | A | A | A | A | A | A | A | A | A | A |
| Georgia Avenue |  | PM | - | A | A | A | A | A | A | A | A | A | A | A | A |
| Colorado Street/ | AWSC | AM | - | - | - | - | A | - | A | - | A | A | A | A | - |
| Escalante Drive |  | PM | - | - | - | - | A | - | A | - | A | A | A | A | - |

Notes:
(1) $\mathrm{EB}=$ eastbound, $\mathrm{WB}=$ westbound, $\mathrm{NB}=$ northbound, $\mathrm{SB}=$ southbound, $\mathrm{LT}=$ left turn, $\mathrm{TH}=$ through, $\mathrm{RT}=$ right turn
(2) US Highway 50 is oriented north/south and New York Street is oriented east/west at this intersection.
(3) TWSC = two-way stop-sign control
(4) AWSC = all-way stop-sign control
(5) Potential mitigation could be conversion to a three-quarter or right-in/right-out intersection. Another option would be to signalize this intersection and then convert the SH $135 /$ Virginia intersection to three-quarter or right-in/right-out.

Source: LSC Transportation Consultants, Inc.

| Intersection | Traffic Control | Peak Hour | Table 2cLevels of Service2027 Total TrafficGunnison Rising - "Authentically Colorado" |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | 2027 Total Traffic |  |  |  |  |  |  |  |  |  |  |  |  |
|  |  |  | Intersection | EB ${ }^{(1)}$ |  |  | WB |  |  | NB |  |  | SB |  |  |
|  |  |  | LOS | LT | TH | RT | LT | TH | RT | LT | TH | RT | LT | TH | RT |
| US Highway 50/ | Traffic Signal | AM | A | D | D | D | D |  | D | A | A | A | A | A | A |
| New York Street ${ }^{(2)}$ |  | PM | A | D | D | D | D | D | D | A | A | A | A | A | A |
| US Highway 50/ | Traffic Signal | AM | A | A | A | A | A | A | A | D | D | C | D | D | C |
| Spruce Street |  | PM | B | A | B | A | A | A | A | C | C | C | D | D | C |
| US Highway 50/ | Traffic Signal | AM | B | C | A | A | A | B | B | D | D | D | D | B | B |
| State Highway 135 |  | PM | C | D | B | B | B | D | C | D | D | D | D | C | C |
| US Highway 50/ | Traffic Signal | AM | B | A | A | A | A | A | A | D | D | D | D | D | D |
| Colorado Street |  | PM | B | B | B | B | A | A | A | D | D | D | D | D | D |
| US Highway 50/ | Traffic Signal | AM | A | B | A | A | A | A | A | D | D | D | D | D | D |
| Adams Street |  | PM | A | B | A | A | A | A | A | D | D | D | D | D | D |
| US Highway 50/ | Traffic Signal | AM | A | A | A | A | A | A | A | D | C | C | D | D | D |
| West Commercial Access |  | PM | C | D | A | A | B | C | B | D | C | C | D | D | D |
| US Highway 50/ | AWSC ${ }^{(3)}$ | AM | - | B | free | - | - | free | free | - | - | - | C | - | B |
| Residential Village Access |  | PM | - | B | free | - | - | free | free | - | - | - | D | - | C |
| US Highway 50/ | TWSC ${ }^{(4)}$ | AM | - | A | free | free | A | free | free | C | C | C | C | C | c |
| County Road 72 West |  | PM | - | B | free | free | B | free | free | D | C | c | D | C | c |
| US Highway 50/ | AWSC | AM | - | A | free | - | - | free | free | - | - | - | C | - | C |
| Best Western Access |  | PM | - | B | free | - | - | free | free | - | - | - | C | - | c |
| US Highway 50/ | TWSC | AM | - | A | free | free | A | free | free | C | B | B | C | C | c |
| County Road 72 East |  | PM | - | B | free | free | B | free | free | D | C | C | D | c | c |
| US Highway 50/ | Traffic Signal | AM | B | A | A | A | A | A | A | D | c | c | C | c | c |
| Future West Off-Site Access |  | PM | A | A | A | A | A | A | A | D | D | D | D | D | D |
| US Highway 50 | Traffic Signal | AM | B | A | A | C | A | B | B | C | c | C | D | D | D |
| Future East Off-Site Access |  | PM | C | A | A | C | A | B | B | D | C | C | D | D | D |
| State Highway 135/ | AWSC | AM | - | - | free | free | A | free | - | B | - | B | - | - | - |
| Industrial Park Road |  | PM | - | - | free | free | A | free | - | B | - | B | - | - | - |
| State Highway 135/ | Traffic Signal | AM | B | D | D | D | D | D | D | A | A | A | A | A | A |
| Virginia Street |  | PM | B | D | D | D | C | C | C | A | A | A | A | A | A |
| State Highway 135/ | TWSC | AM | - | E (42.5s) | $E(42.5 \mathrm{~s})$ | $E(42.5 \mathrm{~s})$ | $E(35.18)$ | $E(35.15)$ | E (35.1s) | A | free | free | A | free | free |
| Georgia Avenue ${ }^{(5)}$ |  | PM | - | F (771.6s) | $F(771.6 \mathrm{~s})$ | $F(771.6 \mathrm{~s})$ | $F(401.8 \mathrm{~s})$ | F (401.8s) | F (401.8s) | B | free | free | B | free | free |
| State Highway 135/ | Traffic Signal | AM | B | D | D | D | D | D | D | A | A | B | A | A | A |
| Spencer Avenue |  | PM | B | D | D | C | D | D | c | A | A | B | A | A | A |
| State Highway 135/ | TWSC | AM | - | - | - | B | - | - | B | A | free | free | A | free | free |
| Colorado Street |  | PM | - | - | - | C | - | - | B | B | free | free | A | free | free |
| Colorado Street/ | AWSC | AM | - | A | A | A | A | A | A | A | A | A | A | A | A |
| Georgia Avenue |  | PM | - | B | B | B | B | B | B | B | B | B | B | B | B |
| Colorado Street/ | AWSC | AM | - | - | - | - | A | - | A | - | A | A | A | A | - |
| Escalante Drive |  | PM | - | - | - | - | B | - | B | - | A | A | B | B | - |

Notes:
(1) $\mathrm{EB}=$ eastbound, $\mathrm{WB}=$ westbound, $\mathrm{NB}=$ northbound, $\mathrm{SB}=$ southbound, $\mathrm{LT}=$ left turn, $\mathrm{TH}=$ through, $\mathrm{RT}=$ right turn
(2) US Highway 50 is oriented north/south and New York Street is oriented east/west at this intersection.

SC = al-way stop-sign control
(5) Potential mitigation could be conversion to a three-quarter or right-in/right-out intersection. Another option would be to signalize this intersection and then convert the SH 135 /Virginia intersection to three-quarter or right-in/right-out

Source: LSC Transportation Consultants, Inc.

| ```Table 3 \\ Time Horizon For Improvements Gunnison Rising - "Authentically Colorado"``` |  |  |
| :---: | :---: | :---: |
| Time Horizon | Required Geometry and Traffic Control ${ }^{(1)}$ | Responsibility |
| 2027 Background Traffic ${ }^{(2)}$ | US Highway 50 Improvements |  |
|  | Add WB RT ${ }^{(3)}$ and EB RT deceleration lane at Spruce Street and Adams Street. Add WB RT deceleration lane at Colorado Street. | Others ${ }^{(4)}$ |
|  | Add EB LT deceleration lane and separate SB RT and LT lanes at the east and west off-site access aligning with the Gunnison Rising recreational vehicle park access and east commercial access. | Others |
|  | State Highway 135 Improvements |  |
|  | Add SB RT deceleration lane at Spencer Avenue. Add west leg and convert intersection to three-quarter movement at Colorado Street. | Others |
| 2027 Total Traffic | US Highway 50 Improvements |  |
|  | Convert traffic control from TWSC ${ }^{(5)}$ to traffic signal control at Adams Street. ${ }^{(6)}$ | Others with contribution from Gunnison Rising |
|  | Convert traffic control from TWSC to traffic signal control at Colorado Street. ${ }^{(7)}$ | Others with contribution from Gunnison Rising |
|  | Construct all of the improvements shown of Figure 8a that are not included above as 2027 background improvements. | Gunnison Rising |
|  | State Highway 135 Improvements |  |
|  | Construct all of the improvements shown on Figure 8b. | Gunnison Rising with contribution from Others |
|  | Convert Georgia Avenue intersection to three-quarter or right-in/right-out or signalize Georgia Avenue intersection and convert Virginia Avenue intersection to three-quarter or right-in/right-out. | Gunnison Rising with contribution from Others |
| Notes: <br> (1) To achieve the levels of service shown on Tables $2 b$ and $2 c$ <br> (2) All of the 2027 background traffic improvements were based on the "CDOT State Highway Access Code" requirements, and are not required to achieve acceptable levels of service. <br> (3) $\mathrm{NB}=$ northbound, $\mathrm{SB}=$ southbound, $\mathrm{EB}=$ eastbound, WB = westbound, $\mathrm{RT}=$ right turn, $\mathrm{LT}=$ left turn, $\mathrm{TH}=$ through <br> (4) Others could be future developments and/or state and local funding. <br> (5) TWSC = two-way stop-sign control <br> (6) Adams Street is about one-half mile east of the existing State Highway 135 traffic signal and one-half mile west of the proposed Colorado Rising west commercial access traffic signal. <br> (7) Colorado Street falls between the one-half mile spaced intersections of State Highway 135 and Adams Street. This intersection is critical for the relief of State Highway 135 and the US Highway 50/State Highway 135 intersection. Figure 4 shows the progression efficiency achievable along US Highway 50 can meet or exceed the CDOT requirement of 35 percent with this non-standard traffic signal spacing. |  |  |




| US Highway 50 Progression Efficiency Gunnison Rising - "Authentically Colorado" |  |  |  |
| :---: | :---: | :---: | :---: |
| Timeline | Progression Efficiency From New York Street to the East |  |  |
|  | 45 mph posted speed on US Highway 50 east of the proposed Residential Village access | 55 mph posted speed on US Highway 50 east of the proposed Residential Village access | 65 mph posted speed on US Highway 50 east of the proposed Residential Village access |
| 2027 Background | 41.5 Percent | 35.0 Percent | 41.5 Percent |
| 2027 Total Traffic | 41.5 Percent | 35.0 Percent | 41.5 Percent |

## LOCAL NEIGHBORHOOD TRAFFIC IMPACTS

A majority of the site-generated traffic volume is expected to access the site via US 50. Secondary local site access would be to and from the west via Georgia Avenue and Escalante Drive. Escalante Drive is currently a private college street that has no way to restrict non-college traffic. There is little non-college traffic currently using Escalante Drive due to the layout of the existing street system. With an eastern extension of Georgia Avenue it will be more attractive for non-college traffic to use Escalante Drive as an additional east/west route. If Escalante Drive remains private and unimproved, there will likely be less traffic using Escalante than predicted in this analysis. It is expected that traffic capacity will be adequate on Georgia Avenue to accommodate the projected future traffic with or without improvements to Escalante Drive.

From Georgia Avenue and Escalante Drive, it is expected that the site-generated traffic would use Colorado Street to distribute north and south. The site-generated traffic that has an origin or destination east of SH 135 is expected to use the local street grid between Colorado Street and SH 135. The site-generated traffic that has an origin or destination on or west of SH 135 is expected to use Colorado Street to access the existing SH 135 traffic signals at Virginia Street, Denver Street, and Spencer Avenue.

## CDOT STATE HIGHWAY ACCESS PERMIT

It is expected that site specific traffic studies will be completed for the various phases of the project in order to obtain any necessary CDOT State Highway Access Permits.

## Conclusions and Recommendations

The following conclusions and recommendations were drawn regarding the traffic impacts of the proposed Gunnison Rising - "Authentically Colorado" mixed-use development.

## TRIP GENERATION

Buildout of the site is projected to generate about 34,895 vehicle-trips during a typical weekday, with about half of the vehicles entering and half of the vehicles exiting the site. During the weekday morning peak hour, about 1,250 vehicles would enter and 1,120 vehicles would exit the site. During the weekday afternoon peak hour, about 1,715 vehicles would enter and 1,765 vehicles would exit the site.

Buildout of the site is projected to generate about 33,390 vehicle-trips during a typical Saturday, with about half of the vehicles entering and half of the vehicles exiting the site. During the Saturday mid-day peak hour, about 1,730 vehicles would enter and 1,485 vehicles would exit the site.

## WEEKDAY AND SATURDAY TRAFFIC COMPARISON

The existing and projected site-generated traffic volumes are expected to be higher during the typical weekday than during the typical Saturday. For this reason, the weekday scenario was analyzed in detail.

## PROJECTED LEVELS OF SERVICE

All of the movements at the analyzed signalized intersections are projected to operate at acceptable levels of service (LOS) during the peak hours through the year 2027 with the recommended roadway improvements. A few of the movements at the analyzed stop-sign controlled intersections are projected to operate at LOS E or F during the peak hours with the recommended roadway improvements.

## TRAFFIC SIGNAL PROGRESSION EFFICIENCY

Generally speaking, the proposed traffic signals are fairly well spaced, but some are not within 200 feet of the one-half mile spacing preferred by CDOT, which requires a progression efficiency analysis. The progression efficiencies on US 50 from New York Street through the proposed Gunnison Rising traffic signals are expected to meet or exceed CDOT's requirement of 35 percent.

The progression efficiencies assume that the section of US 50 between Adams Street and the Residential Village development will be an extension of the existing five-lane urban cross section to the west, with curb and gutter and a posted speed limit of 45 mph . US 50 is proposed as one through lane in each direction with a rural cross section to the east of the Residential Village development, and with shoulders and roadside ditches. Posting this rural section at either 45 or 65 mph would result in a progression efficiency of approximately 41.5 percent. Posting this rural section at 55 mph would result in a progression efficiency of 35 percent.

## RECOMMENDED ROADWAY IMPROVEMENTS

The roadway improvements required to achieve the levels of service shown on Tables $2 \mathrm{a}, 2 \mathrm{~b}$, and 2 c are detailed on Table 3, along with a suggested party responsible for funding each roadway improvement. Figures 8 a and $8 b$ show the majority of the recommended roadway improvements.

## LOCAL NEIGHBORHOOD TRAFFIC IMPACTS

A majority of the site-generated traffic volume is expected to access the site via US 50. Secondary local site access would be to and from the west via Georgia Avenue and Escalante Drive. Escalante Drive is currently a private college street that has no way to restrict non-college traffic. There is little non-college traffic currently using Escalante Drive due to the layout of the existing street system. With an eastern extension of Georgia Avenue it will be more attractive for non-college traffic to use Escalante Drive as an additional east/west route. If Escalante Drive remains private and unimproved, there will likely be less traffic using Escalante than predicted in this analysis. It is expected that traffic capacity will be adequate
on Georgia Avenue to accommodate the projected future traffic with or without improvements to Escalante Drive.

From Georgia Avenue and Escalante Drive, it is expected that the site-generated traffic would use Colorado Street to distribute north and south. The site-generated traffic that has an origin or destination east of SH 135 is expected to use the local street grid between Colorado Street and SH 135. The site-generated traffic that has an origin or destination on or west of SH 135 is expected to use Colorado Street to access the existing SH 135 traffic signals at Virginia Street, Denver Street, and Spencer Avenue.

## CDOT STATE HIGHWAY ACCESS PERMIT

It is expected that site specific traffic studies will be completed for the various phases of the project in order to obtain any necessary CDOT State Highway Access Permits.

## Appendix A: Traffic Count Reports

## LSC Transportation Consultants Inc. <br> Intersection Counts

516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
E-mail: Isc@Isccs.com

File Name : New York 22
Site Code : 01003061
Start Date : 10/03/2006
Page No : 1

Groups Printed- Unshifted

|  | Highway 50 North |  |  |  | New York Ave East |  |  |  | $\begin{aligned} & \text { Highway } 50 \\ & \text { South } \end{aligned}$ |  |  |  | New York Ave West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 4 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 26 | 0 | 0 | 1 | 1 | 6 | 0 | 60 |
| 06:45 AM | 2 | 27 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 63 | 3 | 0 | 3 | 1 | 5 | 0 | 107 |
| Total | 6 | 49 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 89 | 3 | 0 | 4 | 2 | 11 | 0 | 167 |


| 07:00 AM | 1 | 36 | 0 | 0 | 2 | 0 | 3 | 0 | 0 | 58 | 0 | 0 | 2 | 1 | 16 | 0 | 119 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07:15 AM | 5 | 52 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 82 | 2 | 0 | 0 | 1 | 13 | 0 | 157 |
| 07:30 AM | 4 | 35 | 1 | 0 | 0 | 1 | 0 | 0 | 1 | 79 | 1 | 0 | 2 | 2 | 16 | 0 | 142 |
| 07:45 AM | 4 | 67 | 4 | 0 | 4 | 1 | 2 | 0 | 0 | 155 | 4 | 0 | 6 | 1 | 19 | 0 | 267 |
| Total | 14 | 190 | 6 | 0 | 7 | 2 | 5 | 0 | 1 | 374 | 7 | 0 | 10 | 5 | 64 | 0 | 685 |
| 08:00 AM | 3 | 75 | 1 | 0 | 2 | 1 | 2 | 0 | 0 | 146 | 8 | 0 | 1 | 4 | 14 | 0 | 257 |
| 08:15 AM | 8 | 73 | 4 | 0 | 4 | 1 | 4 | 0 | 1 | 110 | 2 | 0 | 7 | 1 | 10 | 0 | 225 |
| Grand Total | 31 | 387 | 12 | 0 | 13 | 5 | 11 | 0 | 3 | 719 | 20 | 0 | 22 | 12 | 99 | 0 | 1334 |
| Apprch \% | 7.2 | 90.0 | 2.8 | 0.0 | 44.8 | 17.2 | 37.9 | 0.0 | 0.4 | 96.9 | 2.7 | 0.0 | 16.5 | 9.0 | 74.4 | 0.0 |  |
| Total \% | 2.3 | 29.0 | 0.9 | 0.0 | 1.0 | 0.4 | 0.8 | 0.0 | 0.2 | 53.9 | 1.5 | 0.0 | 1.6 | 0.9 | 7.4 | 0.0 |  |

LSC Transportation Consultants Inc.
Intersection Counts
File Name : New York 22
Site Code : 01003061
Start Date : 10/03/2006
Page No : 2

|  | Highway 50 North |  |  |  |  | New York Ave East |  |  |  |  | Highway 50 South |  |  |  |  | New York Ave West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | $\begin{gathered} \text { Rig } \\ \mathrm{ht} \end{gathered}$ | $\begin{gathered} \hline \mathrm{Thr} \\ \mathrm{u} \\ \hline \end{gathered}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{gathered} \mathrm{Rig} \\ \mathrm{ht} \end{gathered}$ | Thr u | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \\ \hline \end{array}$ | App. Total | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Thr } \\ u \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \text { Rig } \\ \text { ht } \end{array}$ | $\begin{array}{r} \hline \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | Ped | App. Total | Int. Total |



## LSC Transportation Consultants Inc. <br> Intersection Counts

516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
File Name : New York 21
Site Code : 01002062
Start Date : 10/02/2006
Page No : 1
E-mail: Isc@Isccs.com

|  | Highway 50 North |  |  |  | New York Ave East |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { South } \end{gathered}$ |  |  |  | New York Ave West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{gathered} \operatorname{lnt} . \\ \text { Total } \end{gathered}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 11 | 101 | 3 | 0 | 2 | 5 | 1 | 0 | 1 | 76 | 4 | 0 | 3 | 0 | 9 | 0 | 216 |
| 04:30 PM | 14 | 99 | 4 | 0 | 4 | 1 | 7 | 0 | 1 | 86 | 5 | 0 | 3 | 2 | 12 | 0 | 238 |
| 04:45 PM | 3 | 105 | 3 | 0 | 1 | 1 | 3 | 0 | 1 | 103 | 5 | 0 | 3 | 2 | 15 | 0 | 245 |
| Total | 28 | 305 | 10 | 0 | 7 | 7 | 11 | 0 | 3 | 265 | 14 | 0 | 9 | 4 | 36 | 0 | 699 |


| 05:00 PM | 8 | 144 | 8 | 0 | 6 | 5 | 8 | 0 | 1 | 123 | 2 | 0 | 4 | 3 | 12 | 0 | 324 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 05:15 PM | 17 | 126 | 0 | 0 | 2 | 7 | 10 | 0 | 1 | 75 | 4 | 0 | 1 | 2 | 14 | 0 | 259 |
| 05:30 PM | 12 | 106 | 1 | 0 | 4 | 3 | 11 | 0 | 0 | 91 | 5 | 0 | 4 | 4 | 18 | 0 | 259 |
| 05:45 PM | 12 | 122 | 5 | 0 | 1 | 6 | 3 | 0 | 0 | 91 | 2 | 0 | 2 | 4 | 10 | 0 | 258 |
| Total | 49 | 498 | 14 | 0 | 13 | 21 | 32 | 0 | 2 | 380 | 13 | 0 | 11 | 13 | 54 | 0 | 1100 |
| 06:00 PM | 11 | 135 | 3 | 0 | 4 | 7 | 3 | 0 | 0 | 72 | 2 | 0 | 3 | 1 | 18 | 0 | 259 |
| Grand Total | 88 | 938 | 27 | 0 | 24 | 35 | 46 | 0 | 5 | 717 | 29 | 0 | 23 | 18 | 108 | 0 | 2058 |
| Apprch \% | 8.4 | 89.1 | 2.6 | 0.0 | 22.9 | 33.3 | 43.8 | 0.0 | 0.7 | 95.5 | 3.9 | 0.0 | 15.4 | 12.1 | 72.5 | 0.0 |  |
| Total \% | 4.3 | 45.6 | 1.3 | 0.0 | 1.2 | 1.7 | 2.2 | 0.0 | 0.2 | 34.8 | 1.4 | 0.0 | 1.1 | 0.9 | 5.2 | 0.0 |  |

LSC Transportation Consultants Inc.
Intersection Counts
File Name : New York 21
Site Code : 01002062
Start Date : 10/02/2006
Page No : 2


## LSC Transportation Consultants Inc.

Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
File Name : Spruce 1
Site Code : 00915061
Start Date : 09/15/2006
E-mail: Isc@Isccs.com

|  | Spruce St North |  |  |  | Highway 50 East |  |  |  | $\begin{gathered} \text { Spruce St } \\ \text { South } \end{gathered}$ |  |  |  | Highway 50 West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 0 | 0 | 1 | 0 | 0 | 33 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 45 | 0 | 0 | 81 |
| 06:45 AM | 2 | 1 | 1 | 0 | 0 | 46 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 74 | 1 | 0 | 127 |
| Total | 2 | 1 | 2 | 0 | 0 | 79 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 119 | 1 | 0 | 208 |


| $07: 00 \mathrm{AM}$ | 2 | 2 | 3 | 0 | 0 | 52 | 0 | 0 | 0 | 0 | 1 | 0 | 3 | 78 | 1 | 0 | 142 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $07: 15 \mathrm{AM}$ | 1 | 2 | 0 | 0 | 2 | 77 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 91 | 1 | 0 | 177 |
| $07: 30 \mathrm{AM}$ | 4 | 2 | 1 | 0 | 4 | 89 | 3 | 0 | 3 | 1 | 3 | 0 | 1 | 96 | 1 | 0 | 208 |
| $07: 45 \mathrm{AM}$ | 5 | 2 | 5 | 0 | 2 | 103 | 5 | 0 | 1 | 3 | 4 | 0 | 5 | 184 | 5 |  |  |
| Total | 12 | 8 | 9 | 0 | 8 | 321 | 9 | 0 | 5 | 4 | 9 | 0 | 9 | 449 | 8 | 0 | 824 |


| 08:00 AM | 4 | 2 | 3 | 0 | 3 | 91 | 2 | 0 | 2 | 3 | 3 | 0 | 6 | 140 | 6 | 0 | 265 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 08:15 AM | 4 | 3 | 4 | 0 | 1 | 122 | 4 | 0 | 2 | 3 | 6 | 0 | 7 | 102 | 1 | 0 | 259 |
| Grand Total | 22 | 14 | 18 | 0 | 12 | 613 | 18 | 0 | 10 | 10 | 18 | 0 | 22 | 810 | 16 | 0 | 1583 |
| Apprch \% | 40.7 | 25.9 | 33.3 | 0.0 | 1.9 | 95.3 | 2.8 | 0.0 | 26.3 | 26.3 | 47.4 | 0.0 | 2.6 | 95.5 | 1.9 | 0.0 |  |
| Total \% | 1.4 | 0.9 | 1.1 | 0.0 | 0.8 | 38.7 | 1.1 | 0.0 | 0.6 | 0.6 | 1.1 | 0.0 | 1.4 | 51.2 | 1.0 | 0.0 |  |

LSC Transportation Consultants Inc. Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
File Name : Spruce 1
Site Code : 00915061
Phone (719) 633-2868
Start Date : 09/15/2006
E-mail: Isc@|sccs.com

Page No : 2

|  | Spruce St North |  |  |  |  | $\text { Highway } 50$ East |  |  |  |  | Spruce St South |  |  |  |  | Highway 50 West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \hline \text { Ped } \\ \text { s } \end{array}$ | App. <br> Total | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \hline \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. <br> Total | Rig | Thr <br> u | Left | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \\ \hline \end{array}$ | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Thr } \\ \text { u } \\ \hline \end{array}$ | Left | Ped | App. <br> Total | $\begin{array}{r} \ln \mathrm{t} . \\ \text { Total } \end{array}$ |

Peak Hour From 06:30 AM to 08:15 AM - Peak 1 of 1


|  |  |  |
| :---: | :---: | :---: |
|  | 9/15/06 7:30:00 AM 9/15/06 8:15:00 AM <br> Unshifted |  |
|  |  |  |

## LSC Transportation Consultants Inc.

Intersection Counts
516 N. Tejon St.
File Name: Spruce 2
Site Code : 00918062
Colorado Springs, CO 80903
Start Date: 09/18/2006
Phone (719) 633-2868
Page No : 1
E-mail: Isc@Isccs.com

|  | Spruce St <br> North |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { East } \end{gathered}$ |  |  |  | Spruce StSouth |  |  |  | Highway 50West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{array}{r}\text { Int. } \\ \text { Total } \\ \hline\end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 5 | 3 | 2 | 0 | 7 | 139 | 7 | 0 | 3 | 6 | 4 | 0 | 5 | 149 | 5 | 0 | 335 |
| 04:30 PM | 8 | 2 | 6 | 0 | 1 | 161 | 10 | 0 | 2 | 6 | 5 | 0 | 2 | 133 | 8 | 0 | 344 |
| 04:45 PM | 5 | 4 | 10 | 0 | 10 | 147 | 0 | 0 | 6 | 2 | 8 | 0 | 1 | 160 | 4 | 0 | 357 |
| Total | 18 | 9 | 18 | 0 | 18 | 447 | 17 | 0 | 11 | 14 | 17 | 0 | 8 | 442 | 17 | 0 | 1036 |


| 05:00 PM | 19 | 8 | 8 | 0 | 4 | 192 | 6 | 0 | 9 | 7 | 17 | 0 | 4 | 176 | 5 | 0 | 455 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $05: 15 \mathrm{PM}$ | 15 | 2 | 7 | 0 | 8 | 147 | 1 | 0 | 3 | 0 | 16 | 0 | 6 | 137 | 6 | 0 | 348 |
| $05: 30 \mathrm{PM}$ | 11 | 6 | 5 | 0 | 3 | 180 | 0 | 0 | 3 | 0 | 6 | 0 | 4 | 116 | 5 | 0 | 339 |
| $05: 45 \mathrm{PM}$ | 7 | 3 | 8 | 0 | 15 | 170 | 1 | 0 | 2 | 2 | 12 | 0 | 4 | 150 | 13 | 0 | 387 |
| Total | 52 | 19 | 28 | 0 | 30 | 689 | 8 | 0 | 17 | 9 | 51 | 0 | 18 | 579 | 29 | 0 | 1529 |


|  |  | 9 | 9 | 0 | 6 | 158 | 4 | 0 | 1 | 5 | 9 | 0 | 3 | 123 | 5 | 0 | 343 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Grand Total | 81 | 37 | 55 | 0 | 54 | 1294 | 29 | 0 | 29 | 28 | 77 | 0 | 29 | 1144 | 51 | 0 | 2908 |
| Apprch \% | 46.8 | 21.4 | 31.8 | 0.0 | 3.9 | 94.0 | 2.1 | 0.0 | 21.6 | 20.9 | 57.5 | 0.0 | 2.4 | 93.5 | 4.2 | 0.0 |  |
| Total \% | 2.8 | 1.3 | 1.9 | 0.0 | 1.9 | 44.5 | 1.0 | 0.0 | 1.0 | 1.0 | 2.6 | 0.0 | 1.0 | 39.3 | 1.8 | 0.0 |  |

File Name : Spruce 2
Site Code : 00918062
Start Date : 09/18/2006
Page No : 2

|  | $\begin{gathered} \text { Spruce St } \\ \text { North } \end{gathered}$ |  |  |  |  | Highway 50 East |  |  |  |  | Spruce St South |  |  |  |  | Highway 50 West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Rig | $\begin{array}{r} \text { Thr } \\ u \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. <br> Total | Rig ht | $\begin{array}{r\|} \hline \mathrm{Thr} \\ u \\ \hline \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | Ped | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | Thr u | Left | Ped | App. <br> Total | Int. Total |



LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
File Name : Main 1
Site Code : 00913061
Start Date : 09/13/2006
E-mail: Isc@lsccs.com
Page No : 1

|  | Main St North |  |  |  | $\underset{\text { East }}{\text { Highway }} 50$ |  |  |  | Main St South |  |  |  | Highway 50 West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 12 | 0 | 10 | 0 | 15 | 26 | 0 | 0 | 0 | 1 | 1 | 0 | 1 | 23 | 26 | 0 | 115 |
| 06:45 AM | 20 | 4 | 9 | 0 | 15 | 38 | 0 | 0 | 1 | 2 | 1 | 0 | 1 | 48 | 36 | 0 | 175 |
| Total | 32 | 4 | 19 | 0 | 30 | 64 | 0 | 0 | , | 3 | 2 | 0 | 2 | 71 | 62 | 0 | 290 |


| 07:00 AM | 34 | 3 | 14 | 0 | 15 | 35 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 34 | 36 | 0 | 176 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07:15 AM | 27 | 1 | 17 | 0 | 17 | 51 | 2 | 0 | 2 | 2 | 2 | 0 | 0 | 55 | 54 | 0 | 230 |
| 07:30 AM | 40 | 3 | 19 | 0 | 20 | 49 | 1 | 0 | 2 | 3 | 1 | 0 | 0 | 47 | 58 | 0 | 243 |
| 07:45 AM | 43 | 7 | 22 | 0 | 38 | 75 | 0 | 0 | 3 | 6 | 5 | 0 | 2 | 107 | 59 | 0 | 367 |
| Total | 144 | 14 | 72 | 0 | 90 | 210 | 3 | 0 | 7 | 16 | 8 | 0 | 2 | 243 | 207 | 0 | 1016 |
| 08:00 AM | 53 | 4 | 10 | 0 | 28 | 91 | 2 | 0 | 6 | 4 | 2 | 0 | 3 | 78 | 45 | 0 | 326 |
| 08:15 AM | 38 | 5 | 25 | 0 | 14 | 62 | 1 | 0 | 4 | 9 | 2 | 0 | 3 | 67 | 52 | 0 | 282 |
| Grand Total | 267 | 27 | 126 | 0 | 162 | 427 | 6 | 0 | 18 | 32 | 14 | 0 | 10 | 459 | 366 | 0 | 1914 |
| Apprch \% | 63.6 | 6.4 | 30.0 | 0.0 | 27.2 | 71.8 | 1.0 | 0.0 | 28.1 | 50.0 | 21.9 | 0.0 | 1.2 | 55.0 | 43.8 | 0.0 |  |
| Total \% | 13.9 | 1.4 | 6.6 | 0.0 | 8.5 | 22.3 | 0.3 | 0.0 | 0.9 | 1.7 | 0.7 | 0.0 | 0.5 | 24.0 | 19.1 | 0.0 |  |

LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
File Name : Main 1
Site Code : 00913061
Colorado Springs, CO 80903
Start Date: 09/13/2006
Phone (719) 633-2868
Page No : 2



LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
File Name : Main 2
Site Code : 00913062
Start Date : 09/13/2006
Phone (719) 633-2868
Page No : 1
E-mail: Isc@lsccs.com

|  | Main St North |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { East } \end{gathered}$ |  |  |  | Main St South |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { West } \end{gathered}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 65 | 4 | 23 | 0 | 26 | 81 | 4 | 0 | 4 | 2 | 3 | 0 | 4 | 78 | 57 | 0 | 351 |
| 04:30 PM | 73 | 9 | 34 | 0 | 33 | 95 | 4 | 0 |  | 10 | 4 | 0 | 3 | 79 | 53 | 0 | 398 |
| 04:45 PM | 79 | 6 | 28 | 0 | 30 | 96 | 3 | 0 | 3 | 10 | 5 | 0 | 4 | 67 | 64 | 0 | 395 |
| Total | 217 | 19 | 85 | 0 | 89 | 272 | 11 | 0 | 8 | 22 | 12 | 0 | 11 | 224 | 174 | 0 | 1144 |


| $05: 00 \mathrm{PM}$ | 85 | 12 | 52 | 0 | 29 | 108 | 4 | 0 | 3 | 11 | 3 | 0 | 9 | 77 | 73 | 0 |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $05: 15 \mathrm{PM}$ | 71 | 14 | 29 | 0 | 25 | 98 | 5 | 0 | 5 | 9 | 3 | 0 | 5 | 76 | 59 | 0 | 396 |
| $05: 30 \mathrm{PM}$ | 97 | 8 | 38 | 0 | 29 | 97 | 2 | 0 | 6 | 14 | 7 | 0 | 3 | 75 | 60 | 0 | 436 |
| $05: 45 \mathrm{PM}$ | 65 | 10 | 30 | 0 | 31 | 102 | 5 | 0 | 4 | 8 | 6 | 0 | 4 | 78 | 57 | 0 | 400 |
| Total | 318 | 44 | 149 | 0 | 114 | 405 | 16 | 0 | 18 | 42 | 19 | 0 | 21 | 306 | 249 | 0 | 1701 |


| 06:00 PM | 72 | 11 | 22 | 0 | 16 | 98 | 3 | 0 | 6 | 10 | 3 | 0 | 11 | 59 | 53 | 0 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Grand Total | 607 | 74 | 256 | 0 | 219 | 775 | 30 | 0 | 32 | 74 | 34 | 0 | 43 | 589 | 476 | 0 |
| Apprch \% | 64.8 | 7.9 | 27.3 | 0.0 | 21.4 | 75.7 | 2.9 | 0.0 | 22.9 | 52.9 | 24.3 | 0.0 | 3.9 | 53.2 | 43.0 | 0.0 |
| Total \% | 18.9 | 2.3 | 8.0 | 0.0 | 6.8 | 24.2 | 0.9 | 0.0 | 1.0 | 2.3 | 1.1 | 0.0 | 1.3 | 18.4 | 14.8 | 0.0 |

LSC Transportation Consultants Inc. Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
File Name : Main 2
Site Code : 00913062
Phone (719) 633-2868
Start Date : 09/13/2006
Page No : 2
E-mail: Isc@Isccs.com

|  | Main St North |  |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { East } \end{gathered}$ |  |  |  |  | Main St South |  |  |  |  | $\begin{aligned} & \text { Highway } 50 \\ & \text { West } \end{aligned}$ |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{gathered} \hline \text { Rig } \\ \mathrm{ht} \\ \hline \end{gathered}$ | $\begin{array}{r} \hline \text { Thr } \\ u \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{gathered} \mathrm{Rig} \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \\ \hline \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | $\begin{gathered} \mathrm{Thr} \\ \mathrm{u} \end{gathered}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |

Peak Hour From 04:15 PM to 06:00 PM - Peak 1 of 1



## LSC Transportation Consultants Inc.

Intersection Counts
516 N. Tejon St.
File Name : Colorado St 2
Colorado Springs, CO 80903
Phone (719) 633-2868
Site Code : 00000000
Start Date : 09/14/2006
E-mail: Isc@Isccs.com
Page No : 1
Groups Printed- Group 1

|  | Colorado St North |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { East } \\ \hline \end{gathered}$ |  |  |  | $\begin{aligned} & \text { Colorado St } \\ & \text { South } \end{aligned}$ |  |  |  | Highway 50 West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \\ \hline \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 4 | 1 | 3 | 0 | 0 | 26 | 0 | 0 | 0 | 1 | 6 | 0 | 3 | 30 | 1 | 0 | 75 |
| 06:45 AM | 9 | 0 | 0 | 0 | 3 | 38 | 0 | 0 | 0 | 0 | 4 | 0 | 2 | 37 | 3 | 0 | 96 |
| Total | 13 | 1 | 3 | 0 | 3 | 64 | 0 | 0 | 0 | 1 | 10 | 0 | 5 | 67 | 4 | 0 | 171 |


| 07:00 AM | 8 | 2 | 0 | 0 | 3 | 56 | 0 | 0 | 0 | 1 | 0 | 0 | 4 | 27 | 8 | 0 | 109 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $07: 15 \mathrm{AM}$ | 5 | 0 | 2 | 0 | 2 | 45 | 1 | 0 | 0 | 0 | 4 | 0 | 6 | 25 | 13 | 0 | 103 |
| $07: 30 \mathrm{AM}$ | 9 | 0 | 0 | 0 | 1 | 50 | 0 | 0 | 0 | 1 | 5 | 0 | 2 | 47 | 11 | 0 | 126 |
| $07: 45 \mathrm{AM}$ | 10 | 1 | 2 | 0 | 7 | 70 | 0 | 0 | 4 | 1 | 2 | 0 | 0 | 93 | 9 | 0 | 199 |
| Total | 32 | 3 | 4 | 0 | 13 | 221 | 1 | 0 | 4 | 3 | 11 | 0 | 12 | 192 | 41 | 0 | 537 |


| 08:00 AM | 8 | 0 | 3 | 0 | 9 | 64 | 3 | 0 | 2 | 7 | 5 | 0 | 0 | 60 | 10 | 0 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $08: 15 \mathrm{AM}$ | 10 | 0 | 1 | 0 | 3 | 77 | 0 | 0 | 1 | 0 | 3 | 0 | 1 | 73 | 9 | 0 |
| Grand Total | 63 | 4 | 11 | 0 | 28 | 426 | 4 | 0 | 7 | 11 | 29 | 0 | 18 | 392 | 64 | 0 |
| Apprch \% | 80.8 | 5.1 | 14.1 | 0.0 | 6.1 | 93.0 | 0.9 | 0.0 | 14.9 | 23.4 | 61.7 | 0.0 | 3.8 | 82.7 | 13.5 | 0.0 |
| Total \% | 6.0 | 0.4 | 1.0 | 0.0 | 2.6 | 40.3 | 0.4 | 0.0 | 0.7 | 1.0 | 2.7 | 0.0 | 1.7 | 37.1 | 6.1 | 0.0 |

File Name : Colorado St 2
Site Code : 00000000
Start Date : 09/14/2006
Page No : 2


## LSC Transportation Consultants Inc.

 Intersection Counts516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
E-mail: Isc@lsccs.com

File Name : Colorado St 1
Site Code : 00000000
Start Date : 09/13/2006
Page No : 1

Groups Printed- Group 1

|  | Colorado St North |  |  |  | Highway 50 East |  |  |  | Colorado St South |  |  |  | Highway 50 West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 14 | 0 | 11 | 0 | 4 | 62 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 75 | 15 | 0 | 185 |
| 04:30 PM | 19 | 1 | 5 | 0 | 2 | 82 | 2 | 0 | 0 | 1 | 0 | 0 | 3 | 101 | 10 | 0 | 226 |
| 04:45 PM | 19 | 3 | 5 | 0 | 3 | 103 | 0 | 0 | 1 | 0 | 3 | 0 | 1 | 51 | 12 | 0 | 201 |
| Total | 52 | 4 | 21 | 0 | 9 | 247 | 2 | 0 | 2 | 3 | 4 | 0 | 4 | 227 | 37 | 0 | 612 |


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $05: 00 \mathrm{PM}$ | 17 | 2 | 9 | 0 | 2 | 87 | 0 | 0 | 1 | 0 | 0 | 0 | 4 | 101 | 10 | 0 | 233 |
| $05: 15 \mathrm{PM}$ | 20 | 1 | 4 | 0 | 2 | 81 | 0 | 0 | 1 | 0 | 1 | 0 | 3 | 77 | 10 | 0 | 200 |
| $05: 30 \mathrm{PM}$ | 20 | 1 | 6 | 0 | 2 | 67 | 1 | 0 | 0 | 0 | 2 | 0 | 0 | 75 | 6 | 0 | 180 |
| $05: 45 \mathrm{PM}$ | 23 | 0 | 8 | 0 | 11 | 120 | 1 | 0 | 0 | 3 | 1 | 0 | 2 | 91 | 19 |  |  |
| Total | 80 | 4 | 27 | 0 | 17 | 355 | 2 | 0 | 2 | 3 | 4 | 0 | 9 | 344 | 45 | 0 | 892 |


| 06:00 PM | 24 | 4 | 11 | 0 | 3 | 86 | 3 | 0 | 0 | 2 | 2 | 0 | 2 | 67 | 10 | 0 | 214 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Grand Total | 156 | 12 | 59 | 0 | 29 | 688 | 7 | 0 | 4 | 8 | 10 | 0 | 15 | 638 | 92 | 0 | 1718 |
| Apprch \% | 68.7 | 5.3 | 26.0 | 0.0 | 4.0 | 95.0 | 1.0 | 0.0 | 18.2 | 36.4 | 45.5 | 0.0 | 2.0 | 85.6 | 12.3 | 0.0 |  |
| Total \% | 9.1 | 0.7 | 3.4 | 0.0 | 1.7 | 40.0 | 0.4 | 0.0 | 0.2 | 0.5 | 0.6 | 0.0 | 0.9 | 37.1 | 5.4 | 0.0 |  |

File Name : Colorado St 1
Site Code : 00000000
Start Date : 09/13/2006
Page No : 2


## LSC Transportation Consultants Inc. Intersection Counts

516 N. Tejon St.
File Name : Adams 1
Site Code : 00009141
Start Date : 09/14/2006
Phone (719) 633-2868
Page No : 1
E-mail: Isc@|sccs.com

|  | Adams St North |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { East } \end{gathered}$ |  |  |  | Adams St South |  |  |  | Highway 50 West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 15 | 0 | 4 | 0 | 6 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 9 | 0 | 77 |
| 06:45 AM | 4 | 0 | 2 | 0 | 2 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 9 | 0 | 71 |
| Total | 19 | 0 | 6 | 0 | 8 | 53 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 18 | 0 | 148 |


| 07:00 AM | 5 | 0 | 2 | 0 | 2 | 40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 21 | 11 | 0 | 81 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07:15 AM | 10 | 0 | 1 | 0 | 3 | 41 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 11 | 13 | 0 | 79 |
| 07:30 AM | 9 | 0 | 3 | 0 | 3 | 36 | 1 | 0 | 0 | 0 | 1 | 0 | 0 | 29 | 33 | 0 | 115 |
| 07:45 AM | 16 | 0 | 6 | 0 | 6 | 71 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 33 | 46 | 0 | 181 |
| Total | 40 | 0 | 12 | 0 | 14 | 188 | 1 | 0 | 0 | 0 | 1 | 0 | 3 | 94 | 103 | 0 | 456 |


| 08:00 AM | 16 | 0 | 3 | 0 | 6 | 59 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 28 | 35 | 0 | 148 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08:15 AM | 13 | 0 | 6 | 0 | 3 | 52 | 0 | 0 | 1 | 0 | 0 | 0 | 2 | 39 | 32 | 0 | 148 |
| Grand Total | 88 | 0 | 27 | 0 | 31 | 352 | 1 | 0 | 1 | 0 | 1 | 0 | 6 | 205 | 188 | 0 | 900 |
| Apprch \% | 76.5 | 0.0 | 23.5 | 0.0 | 8.1 | 91.7 | 0.3 | 0.0 | 50.0 | 0.0 | 50.0 | 0.0 | 1.5 | 51.4 | 47.1 | 0.0 |  |
| Total \% | 9.8 | 0.0 | 3.0 | 0.0 | 3.4 | 39.1 | 0.1 | 0.0 | 0.1 | 0.0 | 0.1 | 0.0 | 0.7 | 22.8 | 20.9 | 0.0 |  |

LSC Transportation Consultants Inc. Intersection Counts

File Name: Adams 1
Site Code : 00009141
Start Date: 09/14/2006
Page No : 2

|  | Adams St North |  |  |  |  | Highway 50 East |  |  |  |  | Adams St South |  |  |  |  | Highway 50 West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \hline \mathrm{Ped} \\ \mathrm{~s} \end{array}$ | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \mathrm{Thr} \\ u \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \mathrm{Ped} \\ \mathrm{~s} \end{array}$ | App. Total | $\begin{array}{r} \hline \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. <br> Total | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |

Peak Hour From 06:30 AM to 08:15 AM - Peak 1 of 1


|  |  |  |
| :---: | :---: | :---: |
|  | 9/14/06 7:30:00 AM 9/14/06 8:15:00 AM <br> Unshifted |  |
|  |  |  |

LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
File Name : Adams 2
Site Code : 00009142
Start Date : 09/14/2006
Phone (719) 633-2868
Page No : 1
Groups Printed- Unshifted

|  | Adams St North |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { East } \end{gathered}$ |  |  |  | Adams St South |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { West } \end{gathered}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \\ \hline \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 22 | 0 | 4 | 0 | 12 | 51 | 0 | 0 | 0 | 0 | 7 | 0 | 7 | 60 | 10 | 0 | 173 |
| 04:30 PM | 22 | 0 | 3 | 0 | 7 | 54 | 0 | 0 | 0 | 2 | 4 | 0 | 4 | 48 | 9 | 0 | 153 |
| 04:45 PM | 21 | 3 | 8 | 0 | 4 | 52 | 0 | 0 | 2 | 0 | 3 | 0 | 8 | 47 | 14 | 0 | 162 |
| Total | 65 | 3 | 15 | 0 | 23 | 157 | 0 | 0 | 2 | 2 | 14 | 0 | 19 | 155 | 33 | 0 | 488 |
| 05:00 PM | 26 | 0 | 3 | 0 | 2 | 58 | 1 | 0 | 1 | 0 | 4 | 0 | 8 | 60 | 16 | 0 | 179 |
| 05:15 PM | 17 | 2 | 3 | 0 | 4 | 55 | 1 | 0 | 1 | 0 | 1 | 0 | 3 | 58 | 12 | 0 | 157 |
| 05:30 PM | 15 | 1 | 5 | 0 | 6 | 80 | 0 | 0 | 0 | 0 | 5 | 0 | 9 | 54 | 14 | 0 | 189 |
| 05:45 PM | 15 | 0 | 2 | 0 | 1 | 69 | 0 | 0 | 0 | 3 | 14 | 0 | 10 | 63 | 16 | 0 | 193 |
| Total | 73 | 3 | 13 | 0 | 13 | 262 | 2 | 0 | 2 | 3 | 24 | 0 | 30 | 235 | 58 | 0 | 718 |
| 06:00 PM | 11 | 1 | 8 | 0 | 0 | 41 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 19 | 0 | 122 |
| Grand Total | 149 | 7 | 36 | 0 | 36 | 460 | 2 | 0 | 4 | 5 | 38 | 0 | 49 | 432 | 110 | 0 | 1328 |
| Apprch \% | 77.6 | 3.6 | 18.8 | 0.0 | 7.2 | 92.4 | 0.4 | 0.0 | 8.5 | 10.6 | 80.9 | 0.0 | 8.3 | 73.1 | 18.6 | 0.0 |  |
| Total \% | 11.2 | 0.5 | 2.7 | 0.0 | 2.7 | 34.6 | 0.2 | 0.0 | 0.3 | 0.4 | 2.9 | 0.0 | 3.7 | 32.5 | 8.3 | 0.0 |  |

LSC Transportation Consultants Inc. Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
File Name : Adams 2
Site Code : 00009142
Start Date : 09/14/2006
Page No : 2
E-mail: Isc@lsccs.com



LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
File Name: Best Western 1
Site Code : 00000000
Phone (719) 633-2868
E-mail: Isc@lsccs.com
Start Date : 09/19/2006
Page No : 1
Groups Printed- Group 1

|  | Best Western Driveway North |  |  |  | Highway 50East |  |  |  | South |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { West } \end{gathered}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{aligned} & \text { Int. } \\ & \text { Total } \\ & \hline \end{aligned}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 1 | 0 | 1 | 0 | 0 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 2 | 0 | 31 |
| 06:45 AM | 2 | 0 | 0 | 0 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 0 | 44 |
| Total | 3 | 0 | 1 | 0 | 0 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 39 | 2 | 0 | 75 |


| $07: 00 \mathrm{AM}$ | 0 | 0 | 0 | 0 | 0 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 0 | 0 | 26 |
| ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $07: 15 \mathrm{AM}$ | 1 | 0 | 0 | 0 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 31 | 0 | 0 | 69 |
| $07: 30 \mathrm{AM}$ | 3 | 0 | 0 | 0 | 0 | 44 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 23 | 0 | 0 | 70 |
| $07: 45 \mathrm{AM}$ | 4 | 0 | 1 | 0 | 0 | 50 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 22 | 2 | 0 | 79 |
| Total | 8 | 0 | 1 | 0 | 0 | 145 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 88 | 2 | 0 | 244 |


| 08:00 AM | 2 | 0 | 0 | 0 | 0 | 37 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 24 | 1 | 0 | 64 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 08:15 AM | 2 | 0 | 0 | 0 | 0 | 32 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 29 | 0 | 0 | 63 |
| Grand Total | 15 | 0 | 2 | 0 | 0 | 244 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 180 | 5 | 0 | 446 |
| Apprch \% | 88.2 | 0.0 | 11.8 | 0.0 | 0.0 | 100.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 97.3 | 2.7 | 0.0 |  |
| Total \% | 3.4 | 0.0 | 0.4 | 0.0 | 0.0 | 54.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 40.4 | 1.1 | 0.0 |  |

LSC Transportation Consultants Inc.
Intersection Counts
File Name : Best Western 1
Site Code : 00000000
Start Date : 09/19/2006
Page No : 2


|  |  |  |
| :---: | :---: | :---: |
|  | 9/19/06 7:15:00 AM 9/19/06 8:00:00 AM <br> Group 1 |  |
|  |  |  |

LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
File Name: Best Western 2
Site Code : 00000000
Start Date : 09/19/2006
Page No : 1
E-mail: Isc@|sccs.com

|  | Best Western Driveway North |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { East } \end{gathered}$ |  |  |  | South |  |  |  | Highway 50 West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 40 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 31 | 2 | 0 | 73 |
| 04:30 PM | 3 | 0 | 0 | 0 | 1 | 44 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 36 | 4 | 0 | 88 |
| 04:45 PM | 0 | 0 | 0 | 0 | 0 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 2 | 0 | 81 |
| Total | 3 | 0 | 0 | 0 | 1 | 123 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 107 | 8 | 0 | 242 |


| $05: 00 \mathrm{PM}$ | 0 | 0 | 0 | 0 | 0 | 36 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 41 | 1 | 0 | 78 |
| ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $05: 15 \mathrm{PM}$ | 0 | 0 | 0 | 0 | 1 | 30 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 56 | 3 | 0 | 90 |
| $05: 30 \mathrm{PM}$ | 1 | 0 | 0 | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 1 | 0 | 79 |
| $05: 45 \mathrm{PM}$ | 1 | 0 | 0 | 0 | 1 | 36 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 40 | 2 |  |  |
| Total | 2 | 0 | 0 | 0 | 2 | 135 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 181 | 7 | 0 | 327 |


| $06: 00 ~ P M ~$ | 3 | 0 | 0 | 0 | 0 | 26 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 53 | 7 | 0 | 89 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Grand Total | 8 | 0 | 0 | 0 | 3 | 284 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 341 | 22 | 0 | 658 |
| Apprch \% | 100.0 | 0.0 | 0.0 | 0.0 | 1.0 | 99.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 93.9 | 6.1 | 0.0 |  |
| Total \% | 1.2 | 0.0 | 0.0 | 0.0 | 0.5 | 43.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 51.8 | 3.3 | 0.0 |  |

File Name : Best Western 2
Site Code : 00000000
Start Date : 09/19/2006
Page No : 2


LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
File Name : Industrial Site
Site Code : 00920061
Start Date : 09/20/2006
Page No : 1
Groups Printed- Unshifted

|  | Driveway North |  |  |  | $\text { Highway } 50$ East |  |  |  | Industrial Site South |  |  |  | Highway 50 West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 0 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 17 | 0 | 0 | 34 |
| 06:45 AM | 0 | 0 | 0 | 0 | 0 | 20 | 4 | 0 | 0 | 0 | 4 | 0 | 10 | 19 | 0 | 0 | 57 |
| Total | 0 | 0 | 0 | 0 | 0 | 30 | 4 | 0 | 0 | 0 | 4 | 0 | 17 | 36 | 0 | 0 | 91 |


| 07:00 AM | 1 | 0 | 0 | 0 | 0 | 25 | 0 | 0 | 0 | 0 | 7 | 0 | 1 | 20 | 0 | 0 | 54 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07:15 AM | 0 | 0 | 0 | 0 | 0 | 36 | 1 | 0 | 0 | 0 | 5 | 0 | 4 | 18 | 0 | 0 | 64 |
| 07:30 AM | 2 | 0 | 0 | 0 | 0 | 24 | 0 | 0 | 0 | 0 | 3 | 0 | 4 | 23 | 0 | 0 | 56 |
| 07:45 AM | 0 | 0 | 0 | 0 | 0 | 39 | 2 | 0 | 0 | 0 | 4 | 0 | 4 | 25 | 0 | 0 | 74 |
| Total | 3 | 0 | 0 | 0 | 0 | 124 | 3 | 0 | 0 | 0 | 19 | 0 | 13 | 86 | 0 | 0 | 248 |


| 08:00 AM | 0 | 0 | 0 | 0 | 0 | 36 | 2 | 0 | 0 | 0 | 4 | 0 | 0 | 31 | 0 | 0 | 73 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 08:15 AM | 1 | 0 | 0 | 0 | 0 | 34 | 0 | 0 | 1 | 0 | 3 | 0 | 3 | 27 | 0 | 0 | 69 |
| Grand Total | 4 | 0 | 0 | 0 | 0 | 224 | 9 | 0 | 1 | 0 | 30 | 0 | 33 | 180 | 0 | 0 | 481 |
| Apprch \% | 100.0 | 0.0 | 0.0 | 0.0 | 0.0 | 96.1 | 3.9 | 0.0 | 3.2 | 0.0 | 96.8 | 0.0 | 15.5 | 84.5 | 0.0 | 0.0 |  |
| Total \% | 0.8 | 0.0 | 0.0 | 0.0 | 0.0 | 46.6 | 1.9 | 0.0 | 0.2 | 0.0 | 6.2 | 0.0 | 6.9 | 37.4 | 0.0 | 0.0 |  |

File Name : Industrial Site
Site Code : 00920061
Start Date : 09/20/2006
Page No : 2



## LSC Transportation Consultants Inc. <br> Intersection Counts

516 N. Tejon St.
File Name: Industrial Site 2
Site Code : 00009192
Colorado Springs, CO 80903
Start Date : 09/19/2006
Page No : 1
Groups Printed- Unshifted
E-mail: Isc@lsccs.com

|  | Driveway North |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { East } \end{gathered}$ |  |  |  | Industrial Site South |  |  |  | $\begin{gathered} \text { Highway } 50 \\ \text { West } \end{gathered}$ |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 0 | 0 | 0 | 0 | 0 | 37 | 0 | 0 | 0 | 0 | 2 | 0 | 3 | 24 | 1 | 0 | 67 |
| 04:30 PM | 1 | 0 | 0 | 0 | 0 | 39 | 0 | 0 | 0 | 0 | 5 | 0 | 4 | 35 | 1 | 0 | 85 |
| 04:45 PM | 0 | 0 | 0 | 0 | 2 | 26 | 0 | 0 | 1 | 0 | 3 | 0 | 0 | 36 | 0 | 0 | 68 |
| Total | 1 | 0 | 0 | 0 | 2 | 102 | 0 | 0 | 1 | 0 | 10 | 0 | 7 | 95 | 2 | 0 | 220 |


| 05:00 PM | 0 | 0 | 0 | 0 | 0 | 32 | 0 | 0 | 0 | 0 | 2 | 0 | 5 | 30 | 1 | 0 | 70 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 05:15 PM | 0 | 0 | 0 | 0 | 3 | 24 | 0 | 0 | 1 | 0 | 8 | 0 | 2 | 44 | 1 | 0 | 83 |
| 05:30 PM | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 0 | 0 | 0 | 2 | 0 | 1 | 41 | 0 | 0 | 68 |
| 05:45 PM | 0 | 0 | 2 | 0 | 0 | 29 | 0 | 0 | 1 | 0 | 2 | 0 | 0 | 37 | 0 | 0 | 71 |
| Total | 0 | 0 | 2 | 0 | 3 | 109 | 0 | 0 | 2 | 0 | 14 | 0 | 8 | 152 | 2 | 0 | 292 |


| 06:00 PM | 0 | 0 | 0 | 0 | 0 | 24 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 39 | 0 | 0 | 65 |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Grand Total | 1 | 0 | 2 | 0 | 5 | 235 | 0 | 0 | 3 | 0 | 25 | 0 | 16 | 286 | 4 | 0 | 577 |  |
| Apprch \% | 33.3 | 0.0 | 66.7 | 0.0 | 2.1 | 97.9 | 0.0 | 0.0 | 10.7 | 0.0 | 89.3 | 0.0 | 5.2 | 93.5 | 1.3 | 0.0 |  | 0.0 |

File Name : Industrial Site 2
Site Code : 00009192
Start Date : 09/19/2006
Page No : 2

|  | Driveway North |  |  |  |  | Highway 50 East |  |  |  |  | Industrial Site South |  |  |  |  | Highway 50 West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Rig ht | $\begin{array}{r} \hline T h r \\ u \end{array}$ | Left | $\begin{array}{r} \hline \mathrm{Ped} \\ \mathrm{~s} \\ \hline \end{array}$ | App. <br> Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \\ \hline \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} T h r \\ u \\ \hline \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | Thr u | Left | Ped | App. <br> Total | Int. Total |

Peak Hour From 04:15 PM to 06:00 PM - Peak 1 of 1


|  |  |  |
| :---: | :---: | :---: |
|  | 9/19/06 4:30:00 PM <br> 9/19/06 5:15:00 PM <br> Unshifted |  |
|  |  |  |

LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
File Name : Virginia 1
Site Code : 00009131
Start Date : 09/13/2006
Phone (719) 633-2868
Page No : 1
E-mail: Isc@|sccs.com

|  | Main St North |  |  |  | $\begin{gathered} \text { Virginia St } \\ \text { East } \end{gathered}$ |  |  |  | Main St South |  |  |  | Virginia St West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 2 | 21 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 44 | 0 | 0 | 1 | 1 | 1 | 0 | 72 |
| 06:45 AM | 3 | 31 | 3 | 0 | 1 | 0 | 0 | 0 | 2 | 50 | 0 | 0 | 2 | 1 | 5 | 0 | 98 |
| Total | 5 | 52 | 4 | 0 | 1 | 0 | 0 | 0 | 3 | 94 | 0 | 0 | 3 | 2 | 6 | 0 | 170 |


| $07: 00 \mathrm{AM}$ | 5 | 52 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 54 | 1 | 0 | 1 | 3 | 4 | 0 | 122 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $07: 15 \mathrm{AM}$ | 5 | 46 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 70 | 2 | 0 | 2 | 2 | 3 | 0 | 130 |
| $07: 30 \mathrm{AM}$ | 7 | 58 | 3 | 0 | 0 | 3 | 0 | 0 | 2 | 80 | 1 | 0 | 7 | 1 | 5 | 0 | 167 |
| $07: 45 \mathrm{AM}$ | 6 | 65 | 8 | 0 | 1 | 9 | 1 | 0 | 1 | 93 | 3 | 0 | 5 | 11 | 5 | 0 | 208 |
| Total | 23 | 221 | 12 | 0 | 1 | 13 | 1 | 0 | 3 | 297 | 7 | 0 | 15 | 17 | 17 | 0 | 627 |


| $08: 00 \mathrm{AM}$ | 15 | 63 | 4 | 0 | 2 | 6 | 0 | 0 | 2 | 70 | 9 | 0 | 4 | 12 | 5 | 0 | 192 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $08: 15 \mathrm{AM}$ | 13 | 60 | 10 | 0 | 1 | 3 | 3 | 0 | 0 | 69 | 4 | 0 | 7 | 5 | 14 | 0 | 189 |
| Grand Total | 56 | 396 | 30 | 0 | 5 | 22 | 4 | 0 | 8 | 530 | 20 | 0 | 29 | 36 | 42 | 0 | 1178 |
| Apprch \% | 11.6 | 82.2 | 6.2 | 0.0 | 16.1 | 71.0 | 12.9 | 0.0 | 1.4 | 95.0 | 3.6 | 0.0 | 27.1 | 33.6 | 39.3 | 0.0 |  |
| Total \% | 4.8 | 33.6 | 2.5 | 0.0 | 0.4 | 1.9 | 0.3 | 0.0 | 0.7 | 45.0 | 1.7 | 0.0 | 2.5 | 3.1 | 3.6 | 0.0 |  |

LSC Transportation Consultants Inc. Intersection Counts
516 N. Tejon St.
File Name : Virginia 1
Site Code : 00009131
Colorado Springs, CO 80903
Start Date : 09/13/2006
Page No : 2
E-mail: Isc@lsccs.com

|  | Main St North |  |  |  |  | $\begin{gathered} \text { Virginia } \mathrm{St} \\ \text { East } \end{gathered}$ |  |  |  |  | Main St South |  |  |  |  | Virginia St West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Thr } \\ u \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{gathered} \mathrm{Thr} \\ \mathrm{u} \end{gathered}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. <br> Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \hline \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{gathered} \text { Rig } \\ \text { ht } \end{gathered}$ | Thr u | Left | Ped s | App. Total | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |

Peak Hour From 06:30 AM to 08:15 AM - Peak 1 of 1


|  |  |  |
| :---: | :---: | :---: |
|  | 9/13/06 7:30:00 AM 9/13/06 8:15:00 AM <br> Unshifted |  |
|  |  |  |

LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
File Name : Virginia 2
Site Code : 00009132
Start Date : 09/13/2006
Phone (719) 633-2868
Page No : 1
E-mail: Isc@lsccs.com

|  | Main St North |  |  |  | $\begin{aligned} & \text { Virginia St } \\ & \text { East } \end{aligned}$ |  |  |  | Main St South |  |  |  | Virginia St West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \\ \hline \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 13 | 86 | 6 | 0 | 8 | 9 | 2 | 0 | 2 | 78 | 4 | 0 | 7 | 10 | 19 | 0 | 244 |
| 04:30 PM | 15 | 107 | 9 | 0 | 1 | 3 | 3 | 0 | 10 | 79 | 5 | 0 | 5 | 10 | 18 | 0 | 265 |
| 04:45 PM | 13 | 99 | 12 | 0 | 10 | 14 | 3 | 0 | 2 | 103 | 9 | 0 | 9 | 11 | 13 | 0 | 298 |
| Total | 41 | 292 | 27 | 0 | 19 | 26 | 8 | 0 | 14 | 260 | 18 | 0 | 21 | 31 | 50 | 0 | 807 |


|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 05:00 PM | 12 | 141 | 13 | 0 | 11 | 6 | 1 | 0 | 1 | 103 | 5 | 0 | 7 | 5 | 16 | 0 | 321 |
| 05:15 PM | 13 | 109 | 13 | 0 | 8 | 14 | 1 | 0 | 2 | 97 | 4 | 0 | 10 | 5 | 11 | 0 | 287 |
| 05:30 PM | 11 | 125 | 6 | 0 | 4 | 4 | 2 | 0 | 5 | 96 | 2 | 0 | 10 | 7 | 8 | 0 | 280 |
| 05:45 PM | 9 | 105 | 9 | 0 | 4 | 7 | 0 | 0 | 2 | 90 | 4 | 0 | 8 | 12 | 10 | 0 | 260 |
| Total | 45 | 480 | 41 | 0 | 27 | 31 | 4 | 0 | 10 | 386 | 15 | 0 | 35 | 29 | 45 | 0 | 1148 |


| $06: 00 ~ P M ~$ | 14 | 101 | 6 | 0 | 9 | 11 | 2 | 0 | 1 | 73 | 1 | 0 | 8 | 8 | 9 | 0 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Grand Total | 100 | 873 | 74 | 0 | 55 | 68 | 14 | 0 | 25 | 719 | 34 | 0 | 64 | 68 | 104 | 0 |
| Apprch \% | 9.6 | 83.4 | 7.1 | 0.0 | 40.1 | 49.6 | 10.2 | 0.0 | 3.2 | 92.4 | 4.4 | 0.0 | 27.1 | 28.8 | 44.1 | 0.0 |
| Total \% | 4.5 | 39.7 | 3.4 | 0.0 | 2.5 | 3.1 | 0.6 | 0.0 | 1.1 | 32.7 | 1.5 | 0.0 | 2.9 | 3.1 | 4.7 | 0.0 |

LSC Transportation Consultants Inc. Intersection Counts

516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
E-mail: Isc@Isccs.com

File Name: Virginia 2
Site Code : 00009132
Start Date : 09/13/2006
Page No : 2

|  | Main St North |  |  |  |  | Virginia St East |  |  |  |  | Main St South |  |  |  |  | Virginia St West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{gathered} \text { Thr } \\ u \end{gathered}$ | Left | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Thr } \\ u \end{array}$ | Left | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{gathered} \mathrm{Rig} \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \text { Int. } \\ \text { Total } \end{array}$ |

Peak Hour From 04:15 PM to 06:00 PM - Peak 1 of 1


516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
E-mail: Isc@lsccs.com

File Name : Georgia 1
Site Code : 00914061
Start Date : 09/14/2006
Page No : 1

|  | $\begin{aligned} & \text { Main St (SH 135) } \\ & \text { North } \end{aligned}$ |  |  |  | Georgia Ave East |  |  |  | Main St (SH 135) South |  |  |  | Georgia Ave West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 1 | 40 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 45 | 1 | 0 | 1 | 0 | 1 | 0 | 91 |
| 06:45 AM | 5 | 46 | 1 | 0 | 0 | 0 | 0 | 0 | 1 | 61 | 1 | 0 | 0 | 0 | 0 | 0 | 115 |
| Total | 6 | 86 | 2 | 0 | 0 | 1 | 0 | 0 | 1 | 106 | 2 | 0 | 1 | 0 | 1 | 0 | 206 |


| $07: 00 \mathrm{AM}$ | 4 | 34 | 1 | 0 | 2 | 0 | 0 | 0 | 1 | 69 | 2 | 0 | 0 | 1 | 1 | 0 | 115 |
| ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $07: 15 \mathrm{AM}$ | 3 | 51 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 73 | 1 | 0 | 0 | 0 | 2 | 0 |  |
| $07: 30 \mathrm{AM}$ | 6 | 58 | 3 | 0 | 2 | 2 | 0 | 0 | 1 | 72 | 1 | 0 | 2 | 1 | 2 | 0 | 132 |
| $07: 45 \mathrm{AM}$ | 9 | 92 | 7 | 0 | 4 | 0 | 0 | 0 | 1 | 92 | 4 | 0 | 3 | 1 | 1 | 0 | 214 |
| Total | 22 | 235 | 12 | 0 | 9 | 2 | 0 | 0 | 3 | 306 | 8 | 0 | 5 | 3 | 6 | 0 | 611 |


| 08:00 AM | 4 | 79 | 8 | 0 | 4 | 2 | 0 | 0 | 2 | 75 | 2 | 0 | 2 | 1 | 1 | 0 | 180 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 08:15 AM | 4 | 74 | 4 | 0 | 0 | 1 | 1 | 0 | 1 | 82 | 1 | 0 | 4 | 1 | 4 | 0 | 177 |
| Grand Total | 36 | 474 | 26 | 0 | 13 | 6 | 1 | 0 | 7 | 569 | 13 | 0 | 12 | 5 | 12 | 0 | 1174 |
| Apprch \% | 6.7 | 88.4 | 4.9 | 0.0 | 65.0 | 30.0 | 5.0 | 0.0 | 1.2 | 96.6 | 2.2 | 0.0 | 41.4 | 17.2 | 41.4 | 0.0 |  |
| Total \% | 3.1 | 40.4 | 2.2 | 0.0 | 1.1 | 0.5 | 0.1 | 0.0 | 0.6 | 48.5 | 1.1 | 0.0 | 1.0 | 0.4 | 1.0 | 0.0 |  |

LSC Transportation Consultants Inc. Intersection Counts

516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
E-mail: Isc@Isccs.com

File Name : Georgia 1
Site Code : 00914061
Start Date : 09/14/2006
Page No : 2

|  | $\begin{aligned} & \text { Main St (SH 135) } \\ & \text { North } \end{aligned}$ |  |  |  |  | Georgia Ave East |  |  |  |  | Main St (SH 135) <br> South |  |  |  |  | Georgia Ave West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | Rig ht | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Rig ht | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. <br> Total | $\begin{gathered} \mathrm{Rig} \\ \mathrm{ht} \end{gathered}$ | $\begin{array}{r\|} \hline \text { Thr } \\ u \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{gathered} \text { Rig } \\ \text { ht } \\ \hline \end{gathered}$ | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | Left | Ped s | App. <br> Total | Int. Total |



LSC Transportation Consultants Inc. Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
File Name : Georgia 2
Site Code : 00914062
Start Date : 09/14/2006
E-mail: Isc@Isccs.com
Page No : 1
Groups Printed-Unshifted

|  | $\begin{aligned} & \text { Main St (SH 135) } \\ & \text { North } \end{aligned}$ |  |  |  | Georgia Ave East |  |  |  | Main St (SH 135)South |  |  |  | Georgia Ave West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 5 | 99 | 4 | 0 | 6 | 2 | 1 | 0 | 3 | 87 | 1 | 0 | 13 | 2 | 4 | 0 | 227 |
| 04:30 PM | 9 | 110 | 7 | 0 | 7 | 5 | 4 | 0 | 3 | 104 | 4 | 0 | 7 | 1 | 2 | 0 | 263 |
| 04:45 PM | 5 | 124 | 3 | 0 | 5 | 1 | 2 | 0 | 4 | 94 | 5 | 0 | 9 | 1 | 5 | 0 | 258 |
| Total | 19 | 333 | 14 | 0 | 18 | 8 | 7 | 0 | 10 | 285 | 10 | 0 | 29 | 4 | 11 | 0 | 748 |
| 05:00 PM | 6 | 131 | 8 | 0 | 9 | 1 | 3 | 0 | 5 | 122 | 8 | 0 | 10 | 0 | 5 | 0 | 308 |
| 05:15 PM | 7 | 137 | 1 | 0 | 5 | 1 | 1 | 0 | 2 | 112 | 0 | 0 | 4 | 2 | 4 | 0 | 276 |
| 05:30 PM | 6 | 117 | 5 | 0 | 4 | 1 | 1 | 0 | 3 | 118 | 3 | 0 | 3 | 1 | 6 | 0 | 268 |
| 05:45 PM | 3 | 138 | 7 | 0 | 0 | 1 | 4 | 0 | 1 | 118 | 4 | 0 | 2 | 1 | 3 | 0 | 282 |
| Total | 22 | 523 | 21 | 0 | 18 | 4 | 9 | 0 | 11 | 470 | 15 | 0 | 19 | 4 | 18 | 0 | 1134 |
| 06:00 PM | 3 | 126 | 2 | 0 | 0 | 1 | 4 | 0 | 2 | 89 | 3 | 0 | 4 | 0 | 3 | 0 | 237 |
| Grand Total | 44 | 982 | 37 | 0 | 36 | 13 | 20 | 0 | 23 | 844 | 28 | 0 | 52 | 8 | 32 | 0 | 2119 |
| Apprch \% | 4.1 | 92.4 | 3.5 | 0.0 | 52.2 | 18.8 | 29.0 | 0.0 | 2.6 | 94.3 | 3.1 | 0.0 | 56.5 | 8.7 | 34.8 | 0.0 |  |
| Total \% | 2.1 | 46.3 | 1.7 | 0.0 | 1.7 | 0.6 | 0.9 | 0.0 | 1.1 | 39.8 | 1.3 | 0.0 | 2.5 | 0.4 | 1.5 | 0.0 |  |

LSC Transportation Consultants Inc. Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
File Name : Georgia 2
Site Code : 00914062
Start Date : 09/14/2006

Page No : 2
E-mail: Isc@lsccs.com

|  | $\begin{gathered} \text { Main St (SH 135) } \\ \text { North } \end{gathered}$ |  |  |  |  | Georgia Ave East |  |  |  |  | $\begin{aligned} & \text { Main St (SH 135) } \\ & \text { South } \end{aligned}$ |  |  |  |  | Georgia Ave West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | $\begin{array}{r} \text { Rig } \\ \mathrm{ht} \end{array}$ | $\begin{gathered} \mathrm{Thr} \\ \mathrm{u} \end{gathered}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Thr } \\ u \\ \hline \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Thr } \\ u \end{array}$ | Left | Ped | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | Thr u | Left | Ped | App. Total | Int. <br> Total |

Peak Hour From 04:15 PM to 06:00 PM - Peak 1 of 1


LSC Transportation Consultants Inc.
Intersection Counts
File Name: Spencer 32
Site Code : 00010031
Start Date : 10/03/2006
Page No : 1
Groups Printed- Unshifted

|  | Highway 135 North |  |  |  | $\begin{gathered} \text { Spencer St } \\ \text { East } \end{gathered}$ |  |  |  | $\begin{aligned} & \text { Highway } 135 \\ & \text { South } \end{aligned}$ |  |  |  | Spencer StWest |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 2 | 21 | 1 | 0 | 0 | 1 | 0 | 0 | 2 | 31 | 1 | 0 | 3 | 1 | 7 | 0 | 70 |
| 06:45 AM | 4 | 47 | 1 | 0 | 1 | 2 | 1 | 0 | 4 | 38 | 3 | 0 | 8 | 1 | 5 | 0 | 115 |
| Total | 6 | 68 | 2 | 0 | 1 | 3 | 1 | 0 | 6 | 69 | 4 | 0 | 11 | 2 | 12 | 0 | 185 |


| 07:00 AM | 7 | 50 | 1 | 0 | 0 | 0 | 2 | 0 | 3 | 47 | 1 | 0 | 9 | 2 | 12 | 0 | 134 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07:15 AM | 8 | 38 | 2 | 0 | 2 | 1 | 3 | 0 | 2 | 98 | 1 | 0 | 7 | 4 | 12 | 0 | 178 |
| 07:30 AM | 18 | 66 | 2 | 0 | 5 | 2 | 1 | 0 | 2 | 52 | 8 | 0 | 3 | 3 | 11 | 0 | 173 |
| 07:45 AM | 17 | 96 | 5 | 0 | 3 | 2 | 3 | 0 | 5 | 61 | 5 | 0 | 11 | 11 | 18 | 0 | 237 |
| Total | 50 | 250 | 10 | 0 | 10 | 5 | 9 | 0 | 12 | 258 | 15 | 0 | 30 | 20 | 53 | 0 | 722 |
| 08:00 AM | 27 | 86 | 6 | 0 | 2 | 7 | 10 | 0 | 6 | 66 | 14 | 0 | 10 | 9 | 9 | 0 | 252 |
| 08:15 AM | 41 | 72 | 7 | 0 | 6 | 14 | 7 | 0 | 5 | 51 | 13 | 0 | 5 | 9 | 8 | 0 | 238 |
| Grand Total | 124 | 476 | 25 | 0 | 19 | 29 | 27 | 0 | 29 | 444 | 46 | 0 | 56 | 40 | 82 | 0 | 1397 |
| Apprch \% | 19.8 | 76.2 | 4.0 | 0.0 | 25.3 | 38.7 | 36.0 | 0.0 | 5.6 | 85.5 | 8.9 | 0.0 | 31.5 | 22.5 | 46.1 | 0.0 |  |
| Total \% | 8.9 | 34.1 | 1.8 | 0.0 | 1.4 | 2.1 | 1.9 | 0.0 | 2.1 | 31.8 | 3.3 | 0.0 | 4.0 | 2.9 | 5.9 | 0.0 |  |

File Name : Spencer 32
Site Code : 00010031
Start Date : 10/03/2006
Page No : 2


LSC Transportation Consultants Inc.
Intersection Counts

516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
E-mail: Isc@lsccs.com

File Name: SH135-spencer noon
Site Code : 00000000
Start Date : 09/30/2006
Page No : 1

|  | $\begin{aligned} & \text { SH } 135 \\ & \text { North } \end{aligned}$ |  |  |  | Spencer East |  |  |  | $\begin{aligned} & \text { SH } 135 \\ & \text { South } \end{aligned}$ |  |  |  | Spencer West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{array}{r} \text { Int. } \\ \text { Total } \\ \hline \end{array}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 12:00 PM | 9 | 42 | 7 | 0 | 11 | 12 | 23 | 0 | 12 | 44 | 9 | 0 | 16 | 13 | 15 | 0 | 213 |
| 12:15 PM | 10 | 58 | 11 | 0 | 3 | 13 | 13 | 0 | 20 | 66 | 11 | 0 | 17 | 8 | 7 | 0 | 237 |
| 12:30 PM | 12 | 49 | 15 | 0 | 11 | 7 | 18 | 0 | 21 | 58 | 5 | 0 | 20 | 6 | 10 | 0 | 232 |
| 12:45 PM | 8 | 70 | 6 | 0 | 8 | 8 | 14 | 0 | 12 | 73 | 13 | 0 | 12 | 15 | 11 | 0 | 250 |
| Total | 39 | 219 | 39 | 0 | 33 | 40 | 68 | 0 | 65 | 241 | 38 | 0 | 65 | 42 | 43 | 0 | 932 |


| 01:00 PM | 8 | 62 | 6 | 0 | 6 | 6 | 15 | 0 | 16 | 48 | 10 | 0 | 10 | 14 | 12 | 0 | 213 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 01:15 PM | 12 | 61 | 8 | 0 | 12 | 11 | 10 | 0 | 24 | 55 | 18 | 0 | 14 | 10 | 8 | 0 | 243 |
| 01:30 PM | 11 | 64 | 13 | 0 | 13 | 7 | 15 | 0 | 20 | 75 | 13 | 0 | 16 | 4 | 7 | 0 | 258 |
| 01:45 PM | 17 | 56 | 14 | 0 | 12 | 5 | 13 | 0 | 23 | 66 | 5 | 0 | 7 | 7 | 16 | 0 | 241 |
| Total | 48 | 243 | 41 | 0 | 43 | 29 | 53 | 0 | 83 | 244 | 46 | 0 | 47 | 35 | 43 | 0 | 955 |
| Grand Total | 87 | 462 | 80 | 0 | 76 | 69 | 121 | 0 | 148 | 485 | 84 | 0 | 112 | 77 | 86 | 0 | 1887 |
| Apprch \% | 13.8 | 73.4 | 12.7 | 0.0 | 28.6 | 25.9 | 45.5 | 0.0 | 20.6 | 67.6 | 11.7 | 0.0 | 40.7 | 28.0 | 31.3 | 0.0 |  |
| Total \% | 4.6 | 24.5 | 4.2 | 0.0 | 4.0 | 3.7 | 6.4 | 0.0 | 7.8 | 25.7 | 4.5 | 0.0 | 5.9 | 4.1 | 4.6 | 0.0 |  |

LSC Transportation Consultants Inc.
Intersection Counts
File Name : SH135-spencer noon
Site Code : 00000000
Start Date : 09/30/2006
Page No : 2


## LSC Transportation Consultants Inc.

Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
E-mail: Isc@lsccs.com
File Name: Spencer 31
Site Code : 00010022
Start Date : 10/02/2006
Page No : 1

|  | $\begin{gathered} \text { Highway } 135 \\ \text { North } \end{gathered}$ |  |  |  | $\begin{gathered} \text { Spencer St } \\ \text { East } \end{gathered}$ |  |  |  | $\begin{aligned} & \text { Highway } 135 \\ & \text { South } \end{aligned}$ |  |  |  | Spencer St West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{gathered} \text { Int. } \\ \text { Total } \end{gathered}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 6 | 62 | 3 | 0 | 13 | 7 | 15 | 0 | 16 | 67 | 8 | 0 | 5 | 18 | 8 | 0 | 228 |
| 04:30 PM | 12 | 74 | 5 | 0 | 10 | 21 | 14 | 0 | 14 | 76 | 8 | 0 | 14 | 10 | 7 | 0 | 265 |
| 04:45 PM | 17 | 82 | 12 | 0 | 13 | 11 | 14 | 0 | 16 | 53 | 3 | 0 | 5 | 11 | 13 | 0 | 250 |
| Total | 35 | 218 | 20 | 0 | 36 | 39 | 43 | 0 | 46 | 196 | 19 | 0 | 24 | 39 | 28 | 0 | 743 |


| $05: 00 ~ P M ~$ | 19 | 65 | 8 | 0 | 17 | 17 | 16 | 0 | 18 | 93 | 14 | 0 | 14 | 12 | 17 | 0 | 310 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $05: 15 \mathrm{PM}$ | 18 | 69 | 7 | 0 | 8 | 17 | 16 | 0 | 11 | 94 | 11 | 0 | 14 | 6 | 16 | 0 | 287 |
| $05: 30 \mathrm{PM}$ | 17 | 82 | 9 | 0 | 16 | 17 | 17 | 0 | 7 | 73 | 7 | 0 | 11 | 12 | 16 | 0 | 284 |
| $05: 45 \mathrm{PM}$ | 9 | 69 | 10 | 0 | 8 | 14 | 19 | 0 | 10 | 67 | 10 | 0 | 18 | 18 | 20 | 0 | 272 |
| Total | 63 | 285 | 34 | 0 | 49 | 65 | 68 | 0 | 46 | 327 | 42 | 0 | 57 | 48 | 69 | 0 | 1153 |


| $06: 00 \mathrm{PM}$ | 11 | 96 | 15 | 0 | 8 | 17 | 13 | 0 | 7 | 78 | 10 | 0 | 5 | 12 | 6 | 0 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Grand Total | 109 | 599 | 69 | 0 | 93 | 121 | 124 | 0 | 99 | 601 | 71 | 0 | 86 | 99 | 103 | 0 |
| Apprch \% | 14.0 | 77.1 | 8.9 | 0.0 | 27.5 | 35.8 | 36.7 | 0.0 | 12.8 | 78.0 | 9.2 | 0.0 | 29.9 | 34.4 | 35.8 | 0.0 |
| Total \% | 5.0 | 27.6 | 3.2 | 0.0 | 4.3 | 5.6 | 5.7 | 0.0 | 4.6 | 27.6 | 3.3 | 0.0 | 4.0 | 4.6 | 4.7 | 0.0 |

File Name : Spencer 31
Site Code : 00010022
Start Date : 10/02/2006
Page No : 2


|  |  |  |
| :---: | :---: | :---: |
|  | $10 / 2 / 06$ 5:00:00 PM $10 / 2 / 06$ 5:45:00 PM <br> Unshifted |  |
|  |  |  |

LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
File Name : Colorado 2
Site Code : 01004061
Phone (719) 633-2868
Start Date : 10/04/2006
Page No : 1
E-mail: Isc@Isccs.com

|  | Colorado St North |  |  |  | Georgia Ave East |  |  |  | $\begin{gathered} \text { Colorado St } \\ \text { South } \end{gathered}$ |  |  |  | Georgia AveWest |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 0 | 4 | 4 | 0 | 1 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 06:45 AM | 0 | 5 | 1 | 0 | 2 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 3 | 0 | 0 | 17 |
| Total | 0 | 9 | 5 | 0 | 3 | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 3 | - | 0 | 30 |


| $07: 00 \mathrm{AM}$ | 0 | 4 | 3 | 0 | 3 | 0 | 1 | 0 | 1 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 20 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| $07: 15 \mathrm{AM}$ | 0 | 9 | 4 | 0 | 1 | 1 | 1 | 0 | 1 | 10 | 0 | 0 | 0 | 0 | 1 | 0 | 28 |
| $07: 30 \mathrm{AM}$ | 0 | 8 | 4 | 0 | 2 | 2 | 0 | 0 | 3 | 16 | 0 | 0 | 1 | 1 | 1 | 0 | 38 |
| $07: 45 \mathrm{AM}$ | 2 | 12 | 24 | 0 | 1 | 2 | 1 | 0 | 5 | 18 | 1 | 0 | 0 | 5 | 0 | 0 | 71 |
| Total | 2 | 33 | 35 | 0 | 7 | 5 | 3 | 0 | 10 | 52 | 1 | 0 | 1 | 6 | 2 | 0 | 157 |


| 08:00 AM | 0 | 9 | 21 | 0 | 3 | 0 | 2 | 0 | 2 | 21 | 3 | 0 | 0 | 4 | 0 | 0 | 65 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 08:15 AM | 0 | 9 | 7 | 0 | 5 | 0 | 0 | 0 | 5 | 10 | 1 | 0 | 0 | 5 | 0 | 0 | 42 |
| Grand Total | 2 | 60 | 68 | 0 | 18 | 5 | 5 | 0 | 17 | 93 | 5 | 0 | 1 | 18 | 2 | 0 | 294 |
| Apprch \% | 1.5 | 46.2 | 52.3 | 0.0 | 64.3 | 17.9 | 17.9 | 0.0 | 14.8 | 80.9 | 4.3 | 0.0 | 4.8 | 85.7 | 9.5 | 0.0 |  |
| Total \% | 0.7 | 20.4 | 23.1 | 0.0 | 6.1 | 1.7 | 1.7 | 0.0 | 5.8 | 31.6 | 1.7 | 0.0 | 0.3 | 6.1 | 0.7 | 0.0 |  |

LSC Transportation Consultants Inc.
Intersection Counts
File Name : Colorado 2
Site Code : 01004061
Start Date : 10/04/2006
Page No : 2

|  | Colorado St North |  |  |  |  | Georgia Ave East |  |  |  |  | Colorado St South |  |  |  |  | Georgia Ave West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | Rig | $\begin{array}{r} \text { Thr } \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \mathrm{Rig} \\ \mathrm{ht} \end{array}$ | $\begin{array}{r} \text { Thr } \\ u \\ \hline \end{array}$ | Left | Ped | App. Total | $\begin{array}{r\|} \hline \text { Rig } \\ \text { ht } \\ \hline \end{array}$ | Thr u | Left | Ped | App. Total | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |



|  |  |  |
| :---: | :---: | :---: |
|  |  |  |
|  |  |  |

LSC Transportation Consultants Inc. Intersection Counts
516 N. Tejon St.
File Name : Colorado 1
Site Code : 01003062
Colorado Springs, CO 80903
Start Date : 10/03/2006
Page No : 1
E-mail: Isc@lsccs.com

|  | Colorado St North |  |  |  | Georgia Ave East |  |  |  | Colorado St South |  |  |  | Georgia Ave West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Int. Total |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 3 | 19 | 4 | 0 | 5 | 6 | 2 | 0 | 0 | 10 | 0 | 0 | 0 | 4 | 3 | 0 | 56 |
| 04:30 PM | 1 | 25 | 4 | 0 | 8 | 2 | 0 | 0 | 0 | 10 | 1 | 0 | 2 | 0 | 1 | 0 | 54 |
| 04:45 PM | 1 | 20 | 5 | 0 | 10 | 7 | 1 | 0 | 1 | 19 | 1 | 0 | 0 | 2 | 1 | 0 | 68 |
| Total | 5 | 64 | 13 | 0 | 23 | 15 | 3 | 0 | 1 | 39 | 2 | 0 | 2 | 6 | 5 | 0 | 178 |


| 05:00 PM | 2 | 23 | 9 | 0 | 9 | 10 | 3 | 0 | 1 | 21 | 2 | 0 | 0 | 5 | 0 | 0 | 85 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 05:15 PM | 3 | 21 | 8 | 0 | 9 | 3 | 2 | 0 | 1 | 14 | 0 | 0 | 1 | 3 | 1 | 0 | 66 |
| 05:30 PM | 1 | 22 | 6 | 0 | 15 | 5 | 1 | 0 | 1 | 21 | 0 | 0 | 2 | 3 | 1 | 0 | 78 |
| 05:45 PM | 3 | 32 | 10 | 0 | 15 | 4 | 1 | 0 | 1 | 11 | 0 | 0 | 0 | 0 | 1 | 0 | 78 |
| Total | 9 | 98 | 33 | 0 | 48 | 22 | 7 | 0 | 4 | 67 | 2 | 0 | 3 | 11 | 3 | 0 | 307 |


| 06:00 PM | 0 | 30 | 8 | 0 | 7 | 5 | 1 | 0 | 2 | 14 | 2 | 0 | 1 | 3 | 1 | 0 | 74 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Grand Total | 14 | 192 | 54 | 0 | 78 | 42 | 11 | 0 | 7 | 120 | 6 | 0 | 6 | 20 | 9 | 0 | 559 |
| Apprch \% | 5.4 | 73.8 | 20.8 | 0.0 | 59.5 | 32.1 | 8.4 | 0.0 | 5.3 | 90.2 | 4.5 | 0.0 | 17.1 | 57.1 | 25.7 | 0.0 |  |
| Total \% | 2.5 | 34.3 | 9.7 | 0.0 | 14.0 | 7.5 | 2.0 | 0.0 | 1.3 | 21.5 | 1.1 | 0.0 | 1.1 | 3.6 | 1.6 | 0.0 |  |

LSC Transportation Consultants Inc.
Intersection Counts
File Name : Colorado 1
Site Code : 01003062
Start Date : 10/03/2006
Page No : 2



LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
Phone (719) 633-2868
File Name : Escalante 2
Site Code : 00000000
Start Date : 10/04/2006
Page No : 1
E-mail: Isc@lsccs.com

|  | Colorado St North |  |  |  | Escalante Dr. East |  |  |  | Colorado St South |  |  |  | West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{aligned} & \text { Int. } \\ & \text { Total } \end{aligned}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 06:30 AM | 0 | 7 | 1 | 0 | 1 | 0 | 0 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 13 |
| 06:45 AM | 0 | 8 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 14 |
| Total | 0 | 15 | 1 | 0 | 2 | 0 | 1 | 0 | 2 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 27 |


| 07:00 AM | 0 | 7 | 3 | 0 | 4 | 0 | 1 | 0 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 20 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 07:15 AM | 0 | 6 | 9 | 0 | 1 | 0 | 2 | 0 | 13 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 35 |
| 07:30 AM | 0 | 6 | 13 | 0 | 2 | 0 | 2 | 0 | 17 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 49 |
| 07:45 AM | 0 | 18 | 23 | 0 | 1 | 0 | 2 | 0 | 39 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 96 |
| Total | 0 | 37 | 48 | 0 | 8 | 0 | 7 | 0 | 71 | 29 | 0 | 0 | 0 | 0 | 0 | 0 | 200 |


| 08:00 AM | 0 | 17 | 16 | 0 | 2 | 0 | 4 | 0 | 20 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 67 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 08:15 AM | 0 | 7 | 16 | 0 | 2 | 0 | 4 | 0 | 26 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 61 |
| Grand Total | 0 | 76 | 81 | 0 | 14 | 0 | 16 | 0 | 119 | 49 | 0 | 0 | 0 | 0 | 0 | 0 | 355 |
| Apprch \% | 0.0 | 48.4 | 51.6 | 0.0 | 46.7 | 0.0 | 53.3 | 0.0 | 70.8 | 29.2 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |
| Total \% | 0.0 | 21.4 | 22.8 | 0.0 | 3.9 | 0.0 | 4.5 | 0.0 | 33.5 | 13.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |  |

LSC Transportation Consultants Inc.
Intersection Counts
File Name : Escalante 2
Site Code : 00000000
Start Date : 10/04/2006
Page No : 2



LSC Transportation Consultants Inc.
Intersection Counts
516 N. Tejon St.
Colorado Springs, CO 80903
File Name : Escalante 1
Site Code : 00010032
Phone (719) 633-2868
Start Date : 10/03/2006
Page No : 1
E-mail: Isc@lsccs.com
Groups Printed- Unshifted

|  | Colorado St North |  |  |  | $\begin{aligned} & \text { Escalante Dr } \\ & \text { East } \end{aligned}$ |  |  |  | $\begin{gathered} \text { Colorado St } \\ \text { South } \end{gathered}$ |  |  |  | West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | Right | Thru | Left | Peds | $\begin{gathered} \text { Int. } \\ \text { Total } \end{gathered}$ |
| Factor | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 | 1.0 |  |
| 04:15 PM | 0 | 12 | 4 | 0 | 11 | 0 | 26 | 0 | 14 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 76 |
| 04:30 PM | 0 | 15 | 3 | 0 | 12 | 0 | 16 | 0 | 11 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 67 |
| 04:45 PM | 0 | 12 | 11 | 0 | 13 | 0 | 23 | 0 | 11 | 20 | 0 | 0 | 0 | 0 | 0 | 0 | 90 |
| Total | 0 | 39 | 18 | 0 | 36 | 0 | 65 | 0 | 36 | 39 | 0 | 0 | 0 | 0 | 0 | 0 | 233 |


| 114 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | :--- | ---: | ---: | ---: |
| $05: 00 \mathrm{PM}$ | 0 | 21 | 8 | 0 | 20 | 0 | 26 | 0 | 25 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 114 |
| $05: 15 \mathrm{PM}$ | 0 | 17 | 5 | 0 | 13 | 0 | 20 | 0 | 13 | 14 | 0 | 0 | 0 | 0 | 0 | 0 | 82 |
| $05: 30 \mathrm{PM}$ | 0 | 11 | 12 | 0 | 10 | 0 | 28 | 0 | 10 | 22 | 0 | 0 | 0 | 0 | 0 | 0 | 93 |
| $05: 45 \mathrm{PM}$ | 0 | 19 | 14 | 0 | 14 | 1 | 18 | 0 | 22 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 100 |
| Total | 0 | 68 | 39 | 0 | 57 | 1 | 92 | 0 | 70 | 62 | 0 | 0 | 0 | 0 | 0 | 0 | 389 |


| $06: 00 ~ P M ~$ | 0 | 16 | 5 | 0 | 13 | 0 | 18 | 0 | 12 | 16 | 0 | 0 | 0 | 0 | 0 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| Grand Total | 0 | 123 | 62 | 0 | 106 | 1 | 175 | 0 | 118 | 117 | 0 | 0 | 0 | 0 | 0 |
| 0 | 0 | 702 |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Apprch \% | 0.0 | 66.5 | 33.5 | 0.0 | 37.6 | 0.4 | 62.1 | 0.0 | 50.2 | 49.8 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total \% | 0.0 | 17.5 | 8.8 | 0.0 | 15.1 | 0.1 | 24.9 | 0.0 | 16.8 | 16.7 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| 0.0 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

LSC Transportation Consultants Inc.
Intersection Counts
File Name : Escalante 1
Site Code : 00010032
Start Date : 10/03/2006
Page No : 2

|  | Colorado St North |  |  |  |  | Escalante Dr East |  |  |  |  | Colorado St South |  |  |  |  | West |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start <br> Time | $\begin{aligned} & \text { Rig } \\ & \text { ht } \end{aligned}$ | Thr | Left | $\begin{array}{\|r\|} \hline \text { Ped } \\ \mathrm{s} \\ \hline \end{array}$ | App. <br> Total | $\begin{aligned} & \text { Rig } \\ & \text { ht } \end{aligned}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | $\begin{array}{r} \hline \text { Ped } \\ \mathrm{s} \end{array}$ | App. <br> Total | $\begin{array}{r} \text { Rig } \\ \text { ht } \end{array}$ | Thr u | Left | $\begin{array}{r} \text { Ped } \\ \mathrm{s} \end{array}$ | App. Total | $\begin{array}{r} \text { Rig } \\ \text { ht } \end{array}$ | $\begin{array}{r} \mathrm{Thr} \\ \mathrm{u} \end{array}$ | Left | Ped | App. Total | Int. <br> Total |

Peak Hour From 04:15 PM to 06:00 PM - Peak 1 of 1



## Appendix B: Level of Service Reports

|  | 4 |  |  |  | 4 |  | * | $\dagger$ | P |  | $\downarrow$ | $\cdots$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | ${ }^{7}$ |  | 4 | F | \% | 个t |  | * | 44 | \% |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| Lane Util Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 0.95 |  | 100 | 0.95 | 1.00 |
| Frt |  | 1.00 | 0.85 |  | 1.00 | 0.85 | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.85 |
| Fit Protected |  | 0.96 | 100 |  | 0.97 | 100 | 0.95 | 1.00 |  | 0.95 | 100 | 1.00 |
| Satd. Flow (prot) |  | 1786 | 1583 |  | 1806 | 1583 | 1770 | 3436 |  | 1770 | 3438 | 1583 |
| Flt Permitted |  | 0.74 | 1.00 |  | 0.82 | 100 | 0.57 | 1.00 |  | 0.43 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1383 | 1583 |  | 1519 | 1583 | 1054 | 3436 |  | 793 | 3438 | 1583 |
| Volume (vph) | 62 | 8 | 6 | 8 | 4 | 11 | 16 | 565 | 2 | 11 | 290 | 20 |
| Peak-hour factor, PHF | 0.85 | 0.65 | 0.65 | 0.65 | 0.60 | 0.70 | 0.75 | 0.95 | 0.60 | 0.70 | 0.95 | 0.75 |
| Adj Flow (vph) | 73 | 12 | 9 | 12 | 7 | 16 | 21 | 595 | 3 | 16 | 305 | 27 |
| RTOR Reduction (vph) | 0 | 0 | 7 | 0 | 0 | 13 | 0 | 0 | 0 | 0 | 0 | 10 |
| Lane Group Flow (vph) | 0 | 85 | 2 | 0 | 19 | 3 | 21 | 598 | 0 | 16 | 305 | 17 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 5\% | 2\% | 2\% | 5\% | 2\% |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Perm |  |  | Perm |  | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  |  | 6 |  | 6 |
| Actuated Green, G (s) |  | 8.1 | 8.1 |  | 8.1 | 8.1 | 29.1 | 29.1 |  | 29.1 | 29.1 | 29.1 |
| Effective Green, g (s) |  | 9.1 | 9.1 |  | 91 | 9.1 | 31.1 | 31.1 |  | 31.1 | 31.1 | 31.1 |
| Actuated g/C Ratio |  | 0.19 | 0.19 |  | 0.19 | 0.19 | 0.65 | 0.65 |  | 0.65 | 0.65 | 0.65 |
| Clearance Time (s) |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 261 | 299 |  | 287 | 299 | 680 | 2217 |  | 512 | 2218 | 1021 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  | c0.17 |  |  | 0.09 |  |
| v/s Ratio Perm |  | co. 06 | 0.00 |  | 0.01 | 0.00 | 0.02 |  |  | 0.02 |  | 0.01 |
| v/c Ratio |  | 0.33 | 0.01 |  | 0.07 | 0.01 | 0.03 | 0.27 |  | 0.03 | 0.14 | 0.02 |
| Uniform Delay, d1 |  | 16.9 | 15.9 |  | 16.1 | 15.9 | 31 | 3.7 |  | 3.1 | 3.3 | 3.1 |
| Progression Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.7 | 00 |  | 0.1 | 0.0 | 0.1 | 0.3 |  | 0.1 | 01 | 0.0 |
| Delay (s) |  | 17.6 | 15.9 |  | 16.2 | 15.9 | 3.2 | 4.0 |  | 3.2 | 3.5 | 3.1 |
| Level of Service |  | B | B |  | B | B | A | A |  | A | A | A |
| Approach Delay (s) |  | 17.5 |  |  | 16.0 |  |  | 3.9 |  |  | 3.4 |  |
| Approach LOS |  | B |  |  | B |  |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 5.3 |  | HCM Le | el of S | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.28 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 48.2 |  | Sum of | st tim |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 32.9\% |  | ICU Lev | of Se | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | ${ }^{*}$ | " |  | 4 | 7 | ${ }^{*}$ | 中 |  | ${ }^{1}$ | 44 | \% |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| Lane Util Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 0.95 |  | 1.00 | 0.95 | 1.00 |
| Frt |  | 1.00 | 0.85 |  | 1.00 | 0.85 | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.85 |
| Fit Protected |  | 0.96 | 1.00 |  | 0.97 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1793 | 1583 |  | 1810 | 1583 | 1770 | 3436 |  | 1770 | 3438 | 1583 |
| Fit Permitted |  | 0.73 | 1.00 |  | 0.78 | 1.00 | 0.39 | 1.00 |  | 0.46 | 1.00 | 100 |
| Satd. Flow (perm) |  | 1357 | 1583 |  | 1461 | 1583 | 722 | 3436 |  | 853 | 3438 | 1583 |
| Volume (vph) | 58 | 14 | 12 | 35 | 23 | 14 | 14 | 495 | 2 | 15 | 650 | 53 |
| Peak-hour factor, PHF | 0.85 | 0.70 | 0.70 | 0.85 | 0.80 | 0.70 | 0.70 | 0.95 | 0.60 | 0.75 | 0.95 | 0.85 |
| Adj. Flow (vph) | 68 | 20 | 17 | 41 | 29 | 20 | 20 | 521 | 3 | 20 | 684 | 62 |
| RTOR Reduction (vph) | 0 | 0 | 14 | 0 | 0 | 16 | 0 | 0 | 0 | 0 | 0 | 22 |
| Lane Group Flow (vph) | 0 | 88 | 3 | 0 | 70 | 4 | 20 | 524 | 0 | 20 | 684 | 40 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 5\% | 2\% | 2\% | 5\% | 2\% |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Perm |  |  | Perm |  | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  |  | . |  | 6 |
| Actuated Green, G (s) |  | 8.3 | 8.3 |  | 8.3 | 8.3 | 29.1 | 29.1 |  | 29.1 | 29.1 | 29.1 |
| Effective Green, g ( s ) |  | 9.3 | 9.3 |  | 9.3 | 9.3 | 31.1 | 31.1 |  | 31.1 | 31.1 | 31.1 |
| Actuated g/C Ratio |  | 0.19 | 0.19 |  | 0.19 | 0.19 | 0.64 | 0.64 |  | 0.64 | 0.64 | 0.64 |
| Clearance Time (s) |  | 5.0 | 5.0 |  | 5.0 | 5.0 | 6.0 | 6.0 |  | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 261 | 304 |  | 281 | 304 | 464 | 2208 |  | 548 | 2209 | 1017 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  | 0.15 |  |  | c0. 20 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | c0. 06 | 0.00 |  | 0.05 | 0.00 | 0.03 |  |  | 0.02 |  | 0.03 |
| v/c Ratio |  | 0.34 | 0.01 |  | 0.25 | 0.01 | 0.04 | 0.24 |  | 0.04 | 0.31 | 0.04 |
| Uniform Delay, d1 |  | 16.9 | 15.8 |  | 16.6 | 15.8 | 3.2 | 3.6 |  | 3.2 | 3.9 | 3.2 |
| Progression Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 0.8 | 0.0 |  | 0.5 | 0.0 | 0.2 | 0.3 |  | 0.1 | 0.4 | 0.1 |
| Delay (s) |  | 17.7 | 15.8 |  | 17.1 | 15.8 | 3.4 | 3.9 |  | 3.3 | 4.2 | 3.2 |
| Level of Service |  | B | B |  | B | B | A | A |  | A | A | A |
| Approach Delay (s) |  | 17.4 |  |  | 16.8 |  |  | 3.9 |  |  | 4.1 |  |
| Approach LOS |  | B |  |  | B |  |  | A |  |  | A |  |
| htersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 5.7 |  | HCM Le | el of S | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.32 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 48.4 |  | Sum of | st time |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 35.2\% |  | ICU Lev | of Se | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

LSC, Inc.


C Critical Lane Group

c Critical Lane Group



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL |  | SBE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | ${ }^{4}$ | $\uparrow$ |  | 7 | 49 |  |  | 4 | 7 |  | 4 | * |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 |  | 4.0 | 4.0 |  |  | 4.0 | 4.0 |  | 4.0 | 4.0 |
| Lane Util Factor | 1.00 | 0.95 |  | 1.00 | 0.95 |  |  | 1.00 | 100 |  | 1.00 | 1.00 |
| Frt | 1.00 | 0.99 |  | 1.00 | 1.00 |  |  | 1.00 | 0.85 |  | 1.00 | 0.85 |
| Flt Protected | 0.95 | 100 |  | 0.95 | 100 |  |  | 0.97 | 1.00 |  | 0.97 | 100 |
| Satd. Flow (prot) | 1770 | 3300 |  | 1770 | 3303 |  |  | 1809 | 1583 |  | 1810 | 1583 |
| Flt Permitted | 0.47 | 1.00 |  | 0.39 | 1.00 |  |  | 0.81 | 1.00 |  | 0.81 | 1.00 |
| Satd. Flow (perm) | 869 | 3300 |  | 727 | 3303 |  |  | 1506 | 1583 |  | 1510 | 1583 |
| Volume (vph) | 14 | 600 | 20 | 15 | 465 | 11 | 17 | 11 | 8 | 14 | 10 | 18 |
| Peak-hour factor, PHF | 0.70 | 0.95 | 0.75 | 0.75 | 0.95 | 0.70 | 0.75 | 0.70 | 0.65 | 0.70 | 0.70 | 0.75 |
| Adj. Flow (vph) | 20 | 632 | 27 | 20 | 489 | 16 | 23 | 16 | 12 | 20 | 14 | 24 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 2 | 0 | 0 | 0 | 10 | , | 0 | 21 |
| Lane Group Flow (vph) | 20 | 657 | 0 | 20 | 503 | 0 | 0 | 39 | 2 | 0 | 34 | 3 |
| Heavy Vehicles (\%). | 2\% | 9\% | 2\% | 2\% | 9\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Tun Type | pm+pt |  |  | pm+pt |  |  | Perm |  | Perm | Perm |  | Perm |
| Protected Phases | 7 | 4 |  | , | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) | 35.3 | 34.3 |  | 35.3 | 34.3 |  |  | 6.9 | 6.9 |  | 6.9 | 6.9 |
| Effective Green, g (s) | 37.3 | 36.3 |  | 37.3 | 36.3 |  |  | 7.9 | 7.9 |  | 7.9 | 79 |
| Actuated g/C Ratio | 0.65 | 0.63 |  | 0.65 | 0.63 |  |  | 0.14 | 0.14 |  | 0.14 | 0.14 |
| Clearance Time (s) | 4.0 | 6.0 |  | 4.0 | 6.0 |  |  | 5.0 | 5.0 |  | 5.0 | 5.0 |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 | 3.0 |  | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 582 | 2094 |  | 492 | 2096 |  |  | 208 | 219 |  | 209 | 219 |
| v/s Ratio Prot | 0.00 | c0.20 |  | c0.00 | 0.15 |  |  |  |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.02 |  |  | 0.03 |  |  |  | c0.03 | 0.00 |  | 0.02 | 0.00 |
| V/c Ratio | 0.03 | 0.31 |  | 0.04 | 0.24 |  |  | 0.19 | 0.01 |  | 0.16 | 0.02 |
| Uniform Delay, d1 | 3.5 | 4.8 |  | 3.5 | 4.5 |  |  | 21.8 | 21.3 |  | 217 | 21.3 |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.0 | 0.4 |  | 0.0 | 0.3 |  |  | 0.4 | 0.0 |  | 0.4 | 0.0 |
| Delay (s) | 3.5 | 5.2 |  | 3.5 | 4.8 |  |  | 22.2 | 21.3 |  | 22.1 | 21.3 |
| Level of Service | A | A |  | A | A |  |  | C | C |  | C | C |
| Approach Delay (s) |  | 5.1 |  |  | 4.7 |  |  | 22.0 |  |  | 21.8 |  |
| Approach LOS |  | A |  |  | A |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 6.4 |  | HCM Lev | el of S | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratioActuated Cycle Length (s) |  |  | 0.29 |  |  |  |  |  |  |  |  |  |
|  |  |  | 57.2 |  | Sum of | st time |  |  | 12.0 |  |  |  |
|  |  |  | 33.9\% |  | ICU Level of Service |  |  |  | A |  | $\square+$ |  |
| Intersection Capacity UtilizationAnalysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | * | 4 | " | ${ }^{*}$ | 4 | 7 |  | $\uparrow$ | 7 |  | $\uparrow$ |  |
| Ideal Flow (vphpl). | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |
| Lane Util. Factor | 1.00 | 0.95 | 100 | 1.00 | 0.95 | 1.00 |  | 1.00 | 100 |  | 1.00 | 10 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |  | 1.00 | 0.85 |  | 1.00 | 0.85 |
| Filt Protected | 0.95 | 100 | 1.00 | 0.95 | 1.00 | 1.00 |  | 0.97 | 1.00 |  | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3312 | 1583 | 1770 | 3312 | 1583 |  | 1808 | 1583 |  | 1808 | 1583 |
| Fit Permitted | 0.41 | 100 | 1.00 | 0.35 | 1.00 | 1.00 |  | 0.79 | 1.00 |  | 0.79 | 1.0 |
| Satd. Flow (perm) | 770 | 3312 | 1583 | 651 | 3312 | 1583 |  | 1472 | 1583 |  | 1472 | 1583 |
| Volume (vph) | 20 | 700 | 30 | 20 | 575 | 40 | 25 | 15 | 15 | 25 | 15 | 25 |
| Peak-hour factor, PHF | 0.80 | 0.95 | 0.85 | 0.80 | 0.95 | 0.85 | 0.80 | 0.75 | 0.75 | 0.80 | 0.75 | 0.80 |
| Adj. Flow (vph) | 25 | 737 | 35 | 25 | 605 | 47 | 31 | 20 | 20 | 31 | 20 | 3 |
| RTOR Reduction (vph) | 0 | 0 | 13 | 0 | 0 | 18 | 0 | 0 | 17 | 0 | 1 | 2 |
| Lane Group Flow (vph) | 25 | 737 | 22 | 25 | 605 | 29 | 0 | 51 | 3 | 0 | 51 |  |
| Heavy Vehicles (\%) | 2\% | 9\% | 2\% | 2\% | 9\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | $\mathrm{pm}+\mathrm{pt}$ |  | Perm | pm+pt |  | Perm | Perm |  | Perm | Perm |  | Perr |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  |  |
| Actuated Green, G (s) | 36.5 | 34.4 | 34.4 | 36.5 | 34.4 | 34.4 |  | 7.4 | 7.4 |  | 7.4 | 7. |
| Effective Green, g (s) | 38.5 | 36.4 | 36.4 | 38.5 | 36.4 | 36.4 |  | 8.4 | 8.4 |  | 8.4 | 8. |
| Actuated g/C Ratio | 0.65 | 0.62 | 0.62 | 0.65 | 0.62 | 0.62 |  | 0.14 | 0.14 |  | 0.14 | 0.1 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 |  | 5.0 | 5.0 |  | 5.0 | 5. |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 539 | 2047 | 978 | 465 | 2047 | 978 |  | 210 | 226 |  | 210 | 22 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | 0.00 | c0.22 |  | c0.00 | 0.18 |  |  |  |  |  |  |  |
| v/s Ratio Perm | 0.03 |  | 0.01 | 0.03 |  | 0.02 |  | c0.03 | 0.00 |  | 0.03 | 0.0 |
| v/c Ratio | 0.05 | 0.36 | 0.02 | 0.05 | 0.30 | 0.03 |  | 0.24 | 0.01 |  | 0.24 | 0.0 |
| Uniform Delay, d1 | 3.6 | 5.5 | 4.4 | 3.6 | 5.3 | 4.4 |  | 22.4 | 217 |  | 22.4 | 21. |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.0 |
| Incremental Delay, d2 | 0.0 | 0.5 | 0.0 | 0.0 | 0.4 | 0.1 |  | 06 | 0.0 |  | 0.6 | 0.0 |
| Delay (s) | 3.6 | 6.0 | 4.4 | 3.7 | 5.6 | 4.4 |  | 23.0 | 21.7 |  | 23.0 | 21. |
| Level of Service | A | A | A | A | A | A |  | c | C |  | C |  |
| Approach Delay (s) |  | 5.9 |  |  | 5.5 |  |  | 22.7 |  |  | 22.5 |  |
| Approach LOS |  | A |  |  | A |  |  | C |  |  | C |  |

Intersection Summary
HCM Average Control Delay
HCM Volume to Capacity ratio
Actuated Cycle Length (s)
Intersection Capacity Utilization

| 7.3 |
| ---: |
| 0.33 |
| 58.9 |
| $36.0 \%$ |
| 15 |

C Critical Lane Group

|  | 7 |  |  | 7 |  |  |  | $\dagger$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{4}$ | 舟 | $\overline{7}$ | ${ }^{*}$ | ¢4 | 7 |  | $\uparrow$ | 7 |  | 4 | * |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |
| Lane Utill Factor | 100 | 0.95 | 100 | 1.00 | 0.95 | 1.00 |  | 100 | 100 |  | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |  | 1.00 | 0.85 |  | 1.00 | 0.85 |
| Fit Protected | 0.95 | 100 | 1.00 | 0.95 | 100 | 100 |  | 0.96 | 100 |  | 0.97 | 1.00 |
| Satd. Flow (prot) | 1770 | 3312 | 1583 | 1770 | 3312 | 1583 |  | 1791 | 1583 |  | 1802 | 1583 |
| Flt Permitted | 0.21 | 1.00 | 1.00 | 0.32 | 100 | 1.00 |  | 0.70 | 1.00 |  | 0.74 | 1.00 |
| Satd. Flow (perm) | 394 | 3312 | 1583 | 602 | 3312 | 1583 |  | 1299 | 1583 |  | 1373 | 1583 |
| Volume (vph) | 40 | 800 | 25 | 15 | 975 | 50 | 70 | 15 | 25 | 60 | 30 | 70 |
| Peak-hour factor, PHF | 0.85 | 0.95 | 0.80 | 0.75 | 0.95 | 0.85 | 0.85 | 0.75 | 0.80 | 0.85 | 0.85 | 0.85 |
| Adj. Flow (vph) | 47. | 842 | 31 | 20 | 1026 | 59 | 82 | 20 | 31 | 71 | 35 | 82 |
| RTOR Reduction (vph) | 0 | 0 | 11 | 0 | 0 | 24 | 0 | 0 | 26 | 0 | 0 | 68 |
| Lane Group Flow (vph) | 47. | 842 | 20 | 20 | 1026 | 35 | 0 | 102 | 5 | 0 | 106 | 14 |
| Heavy Vehicles (\%) | 2\% | 9\% | 2\% | 2\% | 9\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | pm+pt |  | Perm | pm+pt |  | Perm | Perm |  | Perm | Perm |  | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) | 42.3 | 38.7 | 38.7 | 37.3 | 36.2 | 36.2 |  | 9.9 | 9.9 |  | 9.9 | 9.9 |
| Effective Green, g (s) | 44.3 | 40.7 | 40.7 | 39.3 | 38.2 | 38.2 |  | 10.9 | 10.9 |  | 10.9 | 10.9 |
| Actuated g/C Ratio | 0.68 | 0.63 | 0.63 | 0.61 | 0.59 | 0.59 |  | 0.17 | 0.17 |  | 0.17 | 0.17 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 |  | 5.0 | 5.0 |  | 50 | 5.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 346 | 2083 | 996 | 386 | 1955 | 935 |  | 219 | 267 |  | 231 | 267 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | c0.01 | 0.25 |  | 0.00 | c0.31 |  |  |  |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.09 |  | 0.01 | 0.03 |  | 0.02 |  | c0.08 | 0.00 |  | 0.08 | 0.01 |
| $v / \mathrm{R}$ Ratio | 0.14 | 0.40 | 0.02 | 0.05 | 0.52 | 0.04 |  | 0.47 | 0.02 |  | 0.46 | 0.05 |
| Uniform Delay d1 | 4.1 | 6.0 | 4.5 | 5.1 | 79 | 5.5 |  | 24.3 | 22.4 |  | 24.2 | 22.6 |
| Progression Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.2 | 0.6 | 0.0 | 0.1 | 1.0 | 0.1 |  | 1.6 | 0.0 |  | 14 | 0.1 |
| Delay (s) | 4.3 | 6.6 | 4.5 | 5.1 | 8.9 | 5.6 |  | 25.8 | 22.5 |  | 25.7 | 22.6 |
| Level of Service | A | A | A | A | A | A |  | C | C |  | C | C |
| Approach Delay (s) |  | 6.4 |  |  | 8.6 |  |  | 25.1 |  |  | 24.4 |  |
| Approach LOS |  | A |  |  | A |  |  | C |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 9.9 |  | HCM Lev | el of S | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.53 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 64.7 |  | Sum of lo | ost time |  |  | 16.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 51.5\% |  | ICU Leve | of Ser | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


|  | 4 |  |  | 7 |  |  | 4 | 4 | P |  | * | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movenent | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }_{1}$ | 坐4 | 7 | * | ¢4 | 1 |  | $\uparrow$ | $\overrightarrow{7}$ |  | $\pm$ | F |
| Ideal Flow (vphpl), | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |
| Lane Utill Factor | 1.00 | 0.95 | 100 | 1.00 | 0.95 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |  | 1.00 | 0.85 |  | 1.00 | 0.85 |
| Fit Protected | 0.95 | 1.00 | 1.00 | 0.95 | 100 | 1.00 |  | 0.97 | 1.00 |  | 0.96 | 1.00 |
| Satd. Flow (prot) | 1770 | 3343 | 1583 | 1770 | 3343 | 1583 |  | 1809 | 1583 |  | 1786 | 1583 |
| Fit Permitted | 0.30 | 100 | 1.00 | 0.23 | 1.00 | 100 |  | 0.80 | 1.00 |  | 0.72 | 1.00 |
| Satd. Flow (perm) | 561 | 3343 | 1583 | 435 | 3343 | 1583 |  | 1493 | 1583 |  | 1344 | 1583 |
| Volume (vph) | 20 | 990 | 30 | 30 | 800 | 105 | 25 | 15 | 30 | 115 | 15 | 25 |
| Peak-hour factor, PHF | 0.80 | 0.95 | 0.85 | 0.85 | 0.95 | 0.95 | 0.85 | 0.75 | 0.85 | 0.95 | 0.75 | 0.80 |
| Adj. Flow (vph) | 25 | 1042 | 35 | 35 | 842 | 111 | 29 | 20 | 35 | 121 | 20 | 31 |
| RTOR Reduction (vph) | 0 | 0 | 11 | 0 | 0 | 34 | 0 | 0 | 29 | 0 | 0 | 26 |
| Lane Group Flow (vph) | 25 | 1042 | 24 | 35 | 842 | 77 | 0 | 49 | 6 | 0 | 141 | 5 |
| Heavy Vehicles (\%) | 2\% | 8\% | 2\% | 2\% | 8\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | pm+pt |  | Perm | pm+pt |  | Perm | Perm |  | Perm | Perm |  | Perm |
| Protected Phases | 7 | 4 |  | 3 | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) | 70.0 | 66.4 | 66.4 | 70.0 | 66.4 | 66.4 |  | 15.0 | 15.0 |  | 15.0 | 15.0 |
| Effective Green, g (s) | 74.0 | 69.4 | 69.4 | 74.0 | 69.4 | 69.4 |  | 17.0 | 17.0 |  | 17.0 | 17.0 |
| Actuated g/C Ratio | 0.74 | 0.69 | 0.69 | 0.74 | 0.69 | 0.69 |  | 0.17 | 0.17 |  | 0.17 | 0.17 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 471 | 2320 | 1099 | 383 | 2320 | 1099 |  | 254 | 269 |  | 228 | 269 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | 0.00 | c0.31 |  | c0.00 | 0.25 |  |  |  |  |  |  |  |
| v/s Ratio Perm | 0.04 |  | 0.02 | 0.06 |  | 0.05 |  | 0.03 | 0.00 |  | co. 10 | 0.00 |
| V/c Ratio | 0.05 | 0.45 | 0.02 | 0.09 | 0.36 | 0.07 |  | 0.19 | 0.02 |  | 0.62 | 0.02 |
| Uniform Delay d1 | 3.7 | 6.8 | 4.8 | 4.0 | 6.3 | 4.9 |  | 35.6 | 34.6 |  | 38.5 | 34.6 |
| Progression Factor | 0.85 | 0.95 | 0.55 | 0.18 | 0.17 | 0.04 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.0 | 0.6 | 0.0 | 0.1 | 0.4 | 0.1 |  | 0.4 | 0.0 |  | 4.9 | 0.0 |
| Delay (s) | 3.2 | 7.1 | 2.7 | 0.8 | 1.5 | 0.3 |  | 36.0 | 34.6 |  | 43.4 | 34.6 |
| Level of Service | A | A | A | A | A | A |  | D | C |  | D | C |
| Approach Delay (s) |  | 6.8 |  |  | 1.3 |  |  | 35.4 |  |  | 41.8 |  |
| Approach LOS |  | A |  |  | A |  |  | D |  |  | D |  |
| lntersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 8.1 |  | HCM Lev | el of Se | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.46 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 100.0 |  | Sum of lo | st time |  |  | 9.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 47.9\% |  | CU Leve | of Ser | vice |  | A |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |



| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 | 2 | 6 | 6 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Actuated Green, G (s) | 64.7 | 61.4 | 61.4 | 62.3 | 60.2 | 60.2 | 21.5 | 21.5 | 21.5 | 21.5 |
| Effective Green, g(s) | 68.7 | 64.4 | 64.4 | 66.3 | 63.2 | 63.2 | 23.5 | 23.5 | 23.5 | 23.5 |
| Actuated g/C Ratio | 0.69 | 0.64 | 0.64 | 0.66 | 0.63 | 0.63 | 0.24 | 0.24 | 0.24 | 0.24 |
| Clearance Time (s) | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 5.0 | 5.0 | 5.0 | 5.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 217 | 2153 | 1019 | 270 | 2113 | 1000 | 221 | 372 | 285 | 372 |
| v/s Ratio Prot | c0.01 | 0.35 |  | 0.01 | c0.43 |  |  |  |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.14 |  | 0.01 | 0.11 |  | 0,06 | 0.10 | 0.01 | c0.19 | 0.01 |
| v/c Ratio | 0.22 | 0.55 | 0.02 | 0.17 | 0.67 | 0.10 | 0.44 | 0.03 | 0.81 | 0.05 |
| Uniform Delay, d1 | 8.5 | 9.8 | 6.4 | 7.0 | 11.8 | 7.2 | 32.7 | 29.5 | 36.1 | 29.6 |
| Progression Factor | 0.83 | 1.02 | 0.85 | 0.17 | 0.14 | 0.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.5 | 1.0 | 0.0 | 01 | 0.7 | 0.1 | 1.4 | 0.0 | 15.3 | 0.1 |
| Delay (s) | 7.5 | 11.0 | 5.5 | 1.3 | 2.4 | 0.1 | 34.1 | 29.5 | 51.4 | 29.7 |
| Level of Service | A | B | A | A | A | A | C | C | D |  |
| Approach Delay (s) |  | 10.7 |  |  | 2.1 |  | 32.5 |  | 45.9 |  |
| Approach LOS |  | B |  |  | A |  | C |  | D |  |

htersection Summary

| HCM Average Control Delay | 10.8 | HCM Level of Service | B |
| :---: | :---: | :---: | :---: |
| HCM Volume to Capacity ratio | 0.71 |  |  |
| Actuated Cycle Length (s) | 100.0 | Sum of lost time (s) | 12.0 |
| Intersection Capacity Utilization | 62.5\% | ICU Level of Service | B |
| Analysis Period (min) | 15 |  |  |

c Critical Lane Group

c Critical Lane Group

HCM Signalized Intersection Capacity Analysis 10：US 50 \＆SH 135

Seasonally Adjusted Existing Traffic PM Peak Hour

| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \％ | 性 |  | ${ }^{*}$ | 个t |  |  | $\uparrow$ | 「 | ${ }^{K}$ | 个 P |  |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Lane Util．Factor | 1.00 | 0.95 |  | 1.00 | 0，95 |  |  | 1.00 | 1.00 | 1.00 | 0.95 |  |
| Frt | 1.00 | 0.99 |  | 1.00 | 0.97 |  |  | 1.00 | 0.85 | 1.00 | 0.87 |  |
| Flt Protected | 0.95 | 1.00 |  | 0.95 | 1.00 |  |  | 0.98 | 1.00 | 0.95 | 100 |  |
| Satd．Flow（prot） | 1703 | 3294 |  | 1770 | 3221 |  |  | 1833 | 1583 | 1703 | 2970 |  |
| Fit Permitted | 0.26 | 100 |  | 0.49 | 100 |  |  | 0.75 | 1.00 | 0.57 | 1.00 |  |
| Satd．Flow（perm） | 465 | 3294 |  | 916 | 3221 |  |  | 1390 | 1583 | 1014 | 2970 |  |
| Volume（vph） | 320 | 400 | 23 | 17. | 525 | 150 | 21 | 45 | 19 | 190 | 50 | 410 |
| Peak－hour factor，PHF | 0.95 | 0.95 | 0.80 | 0.75 | 0.95 | 0.95 | 0.80 | 0.85 | 0.75 | 0.95 | 0.85 | 0.95 |
| Adj．Flow（vph） | 337 | 421 | 29 | 23 | 553 | 158 | 26 | 53 | 25 | 200 | 59 | 432 |
| RTOR Reduction（vph） | 0 | 4 | 0 | 0 | 26 | 0 | 0 | 0 | 21 | 0 | 291 |  |
| Lane Group Flow（vph） | 337 | 446 | 0 | 23 | 685 | 0 | 0 | 79 | 4 | 200 | 200 |  |
| Heavy Vehicles（\％） | 6\％ | 9\％ | 2\％ | 2\％ | 9\％ | 6\％ | 2\％ | 2\％ | 2\％ | 6\％ | 2\％ | 6\％ |
| Turn Type | pm＋pt |  |  | pm＋pt |  |  | pm＋pt |  | Perm | m＋pt |  |  |
| Protected Phases | 7 | 4 |  | ， | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  | 2 | 6 |  |  |
| Actuated Green，G（s） | 40.5 | 34.0 |  | 31.0 | 28.5 |  |  | 9.0 | 9.0 | 21.0 | 21.0 |  |
| Effective Green， $\mathrm{g}(\mathrm{s})$ | 43.5 | 37.0 |  | 35.0 | 31.5 |  |  | 12.1 | 12.1 | 24.1 | 24.1 |  |
| Actuated g／C Ratio | 0.59 | 0.50 |  | 0.48 | 0.43 |  |  | 0.16 | 0.16 | 0.33 | 0.33 |  |
| Clearance Time（s） | 5.1 | 6.0 |  | 4.0 | 6.0 |  |  | 6.1 | 6.1 | 5.1 | 6.1 |  |
| Vehicle Extension（s） | 3.0 | 3.0 |  | 3.0 | 3.0 |  |  | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Lane Grp Cap（vph） | 426 | 1656 |  | 476 | 1379 |  |  | 229 | 260 | 416 | 973 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | c0．10 | 0.14 |  | 0.00 | 0.21 |  |  |  |  | c0．06 | 0.07 |  |
| v／s Ratio Perm | c0．37 |  |  | 0.02 |  |  |  | 0.06 | 0.00 | c0． 10 |  |  |
| v／c Ratio | 0.79 | 0.27 |  | 0.05 | 0.50 |  |  | 0.34 | 0.02 | 0.48 | 0.21 |  |
| Uniform Delay，d1 | 9.3 | 10.5 |  | 10.3 | 15.3 |  |  | 27.2 | 25.8 | 18.9 | 17.8 |  |
| Progression Factor | 1.00 | 1.00 |  | 1.00 | 1.00 |  |  | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay，d2 | 9.7 | 0.4 |  | 0.0 | 1.3 |  |  | 0.9 | 0.0 | 0.9 | 0.1 |  |
| Delay（s） | 19.0 | 10.9 |  | 10.3 | 16.6 |  |  | 28.1 | 25.8 | 19.8 | 18.0 |  |
| Level of Service | B | B |  | B | B |  |  | C | C | B | B |  |
| Approach Delay（s） |  | 14.4 |  |  | 16.4 |  |  | 27.6 |  |  | 18.5 |  |
| Approach LOS |  | B |  |  | B |  |  | C |  |  | B |  |

lntersection Summary

| HCM Average Control Delay | 16.8 | HCM Level of Service | B |
| :---: | :---: | :---: | :---: |
| HCM Volume to Capacity ratio | 0.67 |  |  |
| Actuated Cycle Length（s） | 73.6 | Sum of lost time（s） | 6.0 |
| Intersection Capacity Utilization | 67．9\％ | ICU Level of Service | C |
| Analysis Period（min） | 15 |  |  |

c Critical Lane Group

c Critical Lane Group


c Critical Lane Group

|  | - |  |  | 7 |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | $4{ }^{4}$ |  | \% | ¢4 | \% | * | F |  | ${ }^{7 / 1 \%}$ | F |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Utill Factor | 1.00 | 0.95 |  | 1.00 | 0.95 | 1.00 | 1.00 | 1.00 |  | 0.97 | 1.00 |  |
| Frt | 1.00 | 1.00 |  | 1.00 | 1.00 | 0.85 | 1.00 | 0.92 |  | 1.00 | 0.87 |  |
| Fit Protected | 0.95 | 1.00 |  | 0.95 | 100 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 1736 | 3425 |  | 1770 | 3438 | 1553 | 1770 | 1723 |  | 3367 | 1586 |  |
| Fit Permitted | 0.12 | 1.00 |  | 0.12 | 1.00 | 100 | 0.38 | 100 |  | 0.95 | 1.00 |  |
| Satd. Flow (perm) | 216 | 3425 |  | 220 | 3438 | 1553 | 703 | 1723 |  | 3367 | 1586 |  |
| Volume (vph) | 400 | 1050 | 30 | 60 | 1225 | 410 | 30 | 60 | 60 | 440 | 55 | 500 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.85 | 0.85 | 0.96 | 0.95 | 0.85 | 0.90 | 0.90 | 0.95 | 0.85 | 0.95 |
| Adj. Flow (vph) | 421 | 1105 | 35 | 71 | 1276 | 432 | 35 | 67 | 67. | 463 | 65 | 526 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 | 0 | 262 | 0 | 36 | 0 | 0 | 283 | 0 |
| Lane Group Flow (vph) | 421 | 1138 | 0 | 71 | 1276 | 170 | 35 | 98 | 0 | 463 | 308 | 0 |
| Heavy Vehicles (\%) | 4\% | 5\% | 2\% | 2\% | 5\% | 4\% | 2\% | 2\% | 2\% | 4\% | 2\% | 4\% |
| Turn Type | pm+pt |  |  | pm+pt |  | Perm | pm+pt |  |  | Prot |  |  |
| Protected Phases | 7 | 4 |  | 3 | 8 |  | 5 | 2 |  | 1 | 6 |  |
| Permitted Phases | 4. |  |  | 8 |  | 8 | 2 |  |  |  |  |  |
| Actuated Green, G (s) | 53.5 | 52.6 |  | 34.2 | 34.2 | 34.2 | 9.3 | 7.5 |  | 16.3 | 23.1 |  |
| Effective Green, g (s) | 55.6 | 55.6 |  | 37.2 | 37.2 | 37.2 | 13.4 | 10.6 |  | 18.4 | 26.2 |  |
| Actuated g/C Ratio | 0.56 | 0.56 |  | 0.37 | 0.37 | 0.37 | 0.13 | 0.11 |  | 0.18 | 0.26 |  |
| Clearance Time (s) | 5.1 | 6.0 |  | 4.0 | 6.0 | 6.0 | 4.0 | 6.1 |  | 5.1 | 6.1 |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 451. | 1904 |  | 135 | 1279 | 578 | 124 | 183 |  | 620 | 416 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | c0.20 | 0.33 |  | 0.02 | c0.37 |  | 0.01 | 0.06 |  | c0. 14 | c0.19 |  |
| v/s Ratio Perm | 0.31 |  |  | 0.18 |  | 0.11 | 0.03 |  |  |  |  |  |
| v/c Ratio | 0.93 | 0.60 |  | 0.53 | 1.00 | 0.29 | 0.28 | 0.54 |  | 0.75 | 0.74 |  |
| Uniform Delay, d1 | 34.3 | 14.8 |  | 23.3 | 31.4 | 22.1 | 38.8 | 42.4 |  | 38.6 | 33.8 |  |
| Progression Factor | 0.81 | 0.64 |  | 0.44 | 0.59 | 1.30 | 1.00 | 1.00 |  | 0.83 | 0.43 |  |
| Incremental Delay d2 | 26.1 | 12 |  | 2.4 | 19.8 | 0.8 | 13 | 3.0 |  | 4.4 | 6.3 |  |
| Delay (s) | 54.0 | 10.7 |  | 12.6 | 38.2 | 29.6 | 40.1 | 45.4 |  | 36.5 | 20.9 |  |
| Level of Service | D. | B |  | B | D | C | D | D |  | D | C |  |
| Approach Delay (s) |  | 22.3 |  |  | 35.1 |  |  | 44.3 |  |  | 27.7 |  |
| Approach LOS |  | C |  |  | D |  |  | D |  |  | C |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 29.4 |  | HCM Lev | vel of | ervice |  | C |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.86 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 100.0 |  | Sum of 1 | ost time |  |  | 6.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 99.8\% |  | ICU Leve | of Se | vice |  | F |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group








C Critical Lane Group

|  |  |  | \% |  | $\checkmark$ |  |  | $\dagger$ | P |  |  | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | * | 性 |  | 7 | $\uparrow+$ |  |  | ¢ |  |  | $\uparrow$ | 「 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 150 | 150 | 6 | 1 | 250 | 20 | 2 | 0 | 1 | 20 | 0 | 55 |
| Peak Hour Factor | 0.95 | 0.95 | 0.65 | 0.60 | 0.95 | 0.75 | 0.60 | 0.60 | 0.60 | 0.75 | 0.60 | 0.85 |
| Hourly flow rate (vph) | 158 | 158 | 9 | 2 | 263 | 27 | 3 | 0 | 2 | 27 | 0 | 65 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (fts) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX , platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC , conficting volume | 290 |  |  | 167 |  |  | 678 | 771 | 84 | 676 | 763 | 145 |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 290 |  |  | 167 |  |  | 678 | 771 | 84 | 676 | 763 | 145 |
| tc, single (s) | 4.1 |  |  | 41 |  |  | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 2.2 |  |  | 2.2 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free \% | 88 |  |  | 100 |  |  | 99 | 100 | 100 | 91 | 100 | 93 |
| cM capacity (veh/h) | 1269 |  |  | 1408 |  |  | 283 | 288 | 959 | 306 | 291 | 876 |
| Direction Lane\# | EB 1 | EB 2 | EB 3 | WB1 | WB 2 | WB 3 | NB 1 | SB 1 | SB2 |  |  |  |
| Volume Total | 158 | 105 | 62 | 2 | 175 | 114 | 5 | 27 | 65 |  |  |  |
| Volume Left | 158 | 0 | 0 | 2 | 0 | 0 | 3 | 27 | 0 |  |  |  |
| Volume Right | 0 | 0 | 9 | 0 | 0 | 27 | 2 | 0 | 65 |  |  |  |
| cSH | 1269 | 1700 | 1700 | 1408 | 1700 | 1700 | 370 | 306 | 876 |  |  |  |
| Volume to Capacity | 0.12 | 0.06 | 0.04 | 0.00 | 0.10 | 0.07 | 0.01 | 0.09 | 0.07 |  |  |  |
| Queue Length 95th (ft) | 11 | 0 | 0 | 0 | 0 | 0 | 1 | 7 | 6 |  |  |  |
| Control Delay (s) | 8.2 | 0.0 | 0.0 | 76 | 0.0 | 00 | 14.9 | 17.9 | 9.4 |  |  |  |
| Lane LOS | A |  |  | A |  |  | B | C | A |  |  |  |
| Approach Delay (s) | 4.0 |  |  | 0.0 |  |  | 14.9 | 11.9 |  |  |  |  |
| Approach LOS |  |  |  |  |  |  | B | B |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 3.5 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 29.2\% | 1 | CU Lev | of Se |  |  | A |  |  | $\pm$ |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

LSC, Inc.

| $4$ |  |  |  |  | $4$ |  | 4 |  | * | $\dagger$ | * |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement EBL | EBT | EBR | WBL | WBI | MBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 4P |  | ${ }^{7}$ | 中 ${ }^{\circ}$ |  |  | * |  |  | 4 | T |
| Sign Control. | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) $\square_{\square} 65$ | 305 | 32 | 2 | 340 | 15 | 25 | 3 | 2 | 15 | 3 | 80 |
| Peak Hour Factor 0.85 | 0.95 | 0.85 | 0.60 | 0.95 | 0.75 | 0.80 | 0.60 | 0.60 | 0.75 | 0.60 | 0.85 |
| Hounly flow rate (vph) $\square 76$ | 321 | 38 | - 3 | 358 | 20 | 31 | 5 | 3 | 20 | 5 | 94 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (f) |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{ft} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage. |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |
| Median type, , |  |  |  |  |  | $\pm$ | None |  |  | None | $1+$ |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |  |  |  |  |
| pX , platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |
| $V C$, conflicting volume $\quad 378$ |  |  | 359 |  |  | 775 | 877 | 179 | 694 | 886 | 189 |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol 378 |  |  | 359 |  |  | 775 | 877 | 179 | 694 | 886 | 189 |
|  |  |  | 4.1 | $\square$ | - | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 |
| tC, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |
| $\mathrm{tF}(\mathrm{s}) \times \square+\square$ |  |  | 22 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 |  |
| p0 queue free \% 94 |  |  | 100 |  |  | 87 | 98 | 100 | 93 | 98 | 89 |
| cM capacity (veh/h) $\square^{\square} 1177$ |  |  | 1197 |  |  | 238 | 266 | 833 | 307 | 263 | 821 |
| Direction, Lane \#, Eba | EB2 | EB3 | WB 1 | WB 2 | WB 3 | NB1 | SB 1 | SB2 |  |  |  |
| Volume Total | 214 | 145 | 3 | 239 | 139 | 40 | 25 | 94 |  |  |  |
| Volume Left 76 | 0 | 0 | 3 | 0 | 0 | 31 | 20 | 0 |  |  |  |
| Volume Right ${ }_{\square}+{ }_{\square}$ | 0 | 38 | 0 | 0 | 20 | 3 | 0 | 94 |  |  |  |
| cSH 1177 | 1700 | 1700 | 1197 | 1700 | 1700 | 257 | 297 | 821 |  |  |  |
| Volume to Capacity $\quad 006$ | 0.13 | 0.09 | 0.00 | 0.14 | 0.08 | 015 | 0.08 | 0.11 |  | , | $\pm$ |
| Queue Length 95th (ft) 5 | 0 | 0 | 0 | 0 | 0 | 13 | 7 | 10 |  |  |  |
| Control Delay (s) $\quad 8$. | 0.0 | 0.0 | 8.0 | 0.0 | 0.0 | 21.5 | 18.2 | 10.0 | $\pm$ | \% | \% |
| Lane LOS |  |  | A |  |  | C | C | A |  |  |  |
| Approach Delay (s) $\quad 15$ |  |  | 01 | $\pm$ |  | 21.5 | 11.7 |  |  |  | $\square$ |
| Approach LOS C B |  |  |  |  |  |  |  |  |  |  |  |
| intersection Summary |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  | 3.0 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  | 31.8\% | $\square 1$ | ULev | of Ser |  |  | A |  |  |  |
| Analysis Period (min) |  | 15 |  |  |  |  |  |  |  |  |  |



|  | 4 |  | $\pm$ |  |  |  |  |  | \% |  | $\frac{1}{7}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{4}$ | 44 | 7 | ${ }^{K}$ | 14 | 「" |  | $\uparrow$ |  |  | 4 | 「 |
| Sign Control |  | Free |  |  | Free |  |  | Stop |  |  | Stop |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 80 | 570 | 40 | 3 | 425 | 20. | 30 | 3 | 3 | 20 | 3 | 100 |
| Peak Hour Factor | 0.90 | 0.95 | 0.85 | 0.60 | 0.95 | 0.80 | 0.85 | 0.65 | 0.65 | 0.85 | 0.65 | 0.95 |
| Hourly flow rate (vph) | 89 | 600 | 47 | 5 | 447 | 25 | 35 | 5 | 5 | 24 | 5 | 105 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{ft} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  |  |  |  |  |  |  | None |  |  | None | $\pm$ |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| pX , platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC, conflicting volume | 472 |  |  | 647 |  |  | 1119 | 1260 | 300 | 942 | 1282 | 224 |
| $v C 1$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 472 |  |  | 647 |  |  | 1119 | 1260 | 300 | 942 | 1282 | 224 |
| tC, single (s),.. | 4.1 |  |  | 4.1 |  |  | 75 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 |
|  |  |  |  |  |  |  |  |  |  |  |  |  |
| tF ( s ) | 2.2 |  |  | 22 |  |  | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 |
| p0 queue free \% | 92 |  |  | 99 |  |  | 72 | 97 | 99 | 88 | 97 | 86 |
| cM capacity (veh/h) | 1086 |  |  | 934 |  |  | 127 | 154 | 696 | 197 | 150 | 780 |
| Direction Lane \# | EB. 1 | EB2 | EB3 | EB4 | WB 1 | WB2 | WE 3 | WB 4 | NB1 | SB1 | SB2 |  |
| Volume Total | 89 | 300 | 300 | 47 | 5 | 224 | 224 | 25 | 45 | 28 | 105 |  |
| Volume Left | 89 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 35 | 24 | 0 |  |
| Volume Right | 0 | 0 | 0 | 47 | 0 | 0 | 0 | 25 | 5 | 0 | 105 |  |
| CSH | 1086 | 1700 | 1700 | 1700 | 934 | 1700 | 1700 | 1700 | 142 | 188 | 780 |  |
| Volume to Capacity | 0.08 | 0.18 | 0.18 | 0.03 | 0.01 | 0.13 | 0.13 | 001 | 0.31 | 015 | 0.14 |  |
| Queue Length 95th (ft) | 7 | 0 | $0$ | 0 | 0 | 0 | 0 | 0 | 31 | 13 | 12 |  |
| Control Delay (s). | 8.6 | 0.0 | 0.0 | 0.0 | 8.9 | 0.0 | 0.0 | 0.0 | 41.5 | 276 | 10.3 |  |
| Lane LOS | A |  |  |  | A |  |  |  | E | D | B |  |
| Approach Delay (s) | 10 |  |  |  | 0.1 |  |  |  | 41.5 | 14.0 |  |  |
| Approach LOS |  |  |  |  |  |  |  |  | E | B |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay 3.3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 378\% |  | U Lev | of Se | ce |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ |  | $t$ |  |  | $\checkmark$ | 4 | \% |  | $\downarrow$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | 4 | " | ${ }^{\dagger}$ | 平个 | ${ }^{7}$ |  | $\uparrow$ |  |  | $\uparrow$ | 7 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 |  |  | 4.0 | 4.0 |
| Lane Util Factor | 1.00 | 0.95 | 100 | 100 | 0.95 | 1.00 |  | 1.00 |  |  | 100 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |  | 0.97 |  |  | 1.00 | 0.85 |
| Fit Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |  | 0.97 |  |  | 0.95 | 1.00 |
| Satd. Flow (prot) | 1770 | 3312 | 1583 | 1770 | 3312 | 1583 |  | 1759 |  |  | 1778 | 1583 |
| Fit Permitted | 0.20 | 100 | 1.00 | 0.21 | 1.00 | 100 |  | 0.85 |  |  | 073 | 1.00 |
| Satd. Flow (perm) | 382 | 3312 | 1583 | 391 | 3312 | 1583 |  | 1541 |  |  | 1354 | 1583 |
| Volume (vph) | 190 | 1175 | 10 | 2 | 1195 | 50 | 5 | 2 | 2 | 45 | 2 | 70 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.70 | 0.60 | 0.95 | 0.85 | 0.65 | 0.60 | 0.60 | 0.80 | 0.60 | 0.85 |
| Adj. Flow (vph) | 200. | 1237 | 14 | 3 | 1258 | 59 | 8 | 3 | 3. | 56 | 3 | 82 |
| RTOR Reduction (vph) | 0 | 0 | 2 | 0 | 0 | 10 | 0 | 3 | 0 | 0 | 0 | 74 |
| Lane Group Flow (vph) | 200 | 1237 | 12 | 3 | 1258 | 49 | 0 | 11 | 0 | 0 | 59 | 8 |
| Heavy Vehicles (\%) | 2\% | 9\% | 2\% | 2\% | 9\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Perm |  |  | Perm |  | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4. |  | 4 | - 8 |  | 8 | 2 |  |  | 6 |  | 6 |
| Actuated Green, G (s) | 82.5 | 82.5 | 82.5 | 82.5 | 82.5 | 82.5 |  | 9.5 |  |  | 9.5 | 9.5 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 82.5 | 82.5 | 82.5 | 82.5 | 82.5 | 82.5 |  | 9.5 |  |  | 9.5 | 9.5 |
| Actuated g/C Ratio | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |  | 0.10 |  |  | 0.10 | 0.10 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 |  |  | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 |  |  | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 315 | 2732 | 1306 | 323 | 2732 | 1306 |  | 146 |  |  | 129 | 150 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | 0.37 |  |  | 0.38 |  |  |  |  |  |  |  |
| v/s Ratio Perm | co. 52 |  | 0.01 | 0.01 |  | 0.03 |  | 0.01 |  |  | c0. 04 | 0.00 |
| v/c Ratio | 0.63 | 0.45 | 0.01 | 0.01 | 0.46 | 0.04 |  | 0.08 |  |  | 0.46 | 0.05 |
| Uniform Delay, d1 | 3.2 | 2.4 | 1.5 | 1.5 | 25 | 1.6 |  | 413 |  |  | 42.8 | 41.2 |
| Progression Factor | 1.32 | 0.53 | 0.82 | 0.17 | 1.12 | 0.11 |  | 1.00 |  |  | 1.00 | 1.00 |
| Incremental Delay, d2 | 8.1 | 0.5 | 0.0 | 0.0 | 0.5 | 0.0 |  | 0.2 |  |  | 2.6 | 01 |
| Delay (s) | 12.4 | 1.8 | 1.3 | 0.3 | 3.3 | 0.2 |  | 41.5 |  |  | 45.4 | 41.3 |
| Level of Service | B | A | A | A | A | A |  | D |  |  | D | D |
| Approach Delay (s) |  | 3.2 |  |  | 3.1 |  |  | 41.5 |  |  | 43.0 |  |
| Approach LOS |  | A |  |  | A |  |  | D |  |  | D |  |
| htersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 5.3 |  | HCM Le | el of S | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.62 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 100.0 |  | Sum of 1 | ost time |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 58.4\% |  | ICU Leve | of Ser | vice |  | B |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |

Analysis Period (min)
c Critical Lane Group

|  | 4 |  | V | 7 |  | 4 | 4 | 4 | 7 |  | $\downarrow$ | $\pm$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | 7 | 个个 | 7 | ${ }^{*}$ | 44 | 7 |  | $\uparrow$ |  |  | $\dagger$ | \% |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900. | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 |  |  | 4.0 | 4.0 |
| Lane Util Factor | 1.00 | 0.95 | 100 | 1.00 | 0.95 | 1.00 |  | 100 |  |  | 1.00 | 1.00 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |  | 0.98 |  |  | 1.00 | 0.85 |
| Fil Protected | 0.95 | 1.00 | 100 | 0.95 | 1.00 | 1.00 |  | 0.96 |  |  | 0.96 | 1.00 |
| Satd. Flow (prot) | 1770 | 3312 | 1583 | 1770 | 3312 | 1583 |  | 1766 |  |  | 1781 | 1583 |
| Fit Permitted | 0.11 | 1.00 | 1.00 | 0.11 | 1.00 | 100 |  | 0.74 |  |  | 0.78 | 1.00 |
| Satd. Flow (perm) | 214 | 3312 | 1583 | 207 | 3312 | 1583 |  | 1354 |  |  | 1453 | 1583 |
| Volume (vph) | 80 | 1660 | 40 | 3 | 1635 | 45 | 30 | 3 | 3 | 45 | 3 | 100 |
| Peak-hour factor, PHF | 0.90 | 0.95 | 0.85 | 0.60 | 0.95 | 0.80 | 0.85 | 0.60 | 0.60 | 0.80 | 0.60 | 0.95 |
| Adj. Flow (vph) | 89 | 1747 | 47 | 5 | 1721 | 56 | 35. | 5 | 5 | 56 | 5 | 105 |
| RTOR Reduction (vph) | 0 | 0 | 8 | 0 | 0 | 10 | 0 | 5 | 0 | 0 | 0 | 47 |
| Lane Group Flow (vph) | 89 | 1747 | 39 | 5 | 1721 | 46 | 0 | 40. | 0 | 0 | 61 | 58 |
| Heavy Vehicles (\%) | 2\% | 9\% | 2\% | 2\% | 9\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Perm |  |  | Perm |  | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8. | 2 |  |  | 6 |  | 6 |
| Actuated Green, G (s) | 82.3 | 82.3 | 82.3 | 82.3 | 82.3 | 82.3 |  | 9.7 |  |  | 9.7 | 9.7 |
| Effective Green, g (s) | 82.3 | 82.3 | 82.3 | 82.3 | 82.3 | 82.3 |  | 9.7 |  |  | 9.7 | 97 |
| Actuated g/C Ratio | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 | 0.82 |  | 0.10 |  |  | 0.10 | 0.10 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 |  |  | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 |  |  | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 176 | 2726 | 1303 | 170 | 2726 | 1303 |  | 131 |  |  | 141 | 154 |
| v/s Ratio Prot |  | c0.53 |  |  | 0.52 |  |  |  |  |  |  |  |
| v/s Ratio Perm | 0.42 |  | 0.02 | 0.02 |  | 0.03 |  | 0.03 |  |  | c0.04 | 0.04 |
| v/c Ratio | 0.51 | 0.64 | 0.03 | 0.03 | 0.63 | 0.04 |  | 0.31 |  |  | 0.43 | 0.38 |
| Uniform Delay, d1 | 2.7 | 3.3 | 16 | 1.6 | 3.3 | 1.6 |  | 42.0 |  |  | 42.6 | 42.3 |
| Progression Factor | 1.06 | 1.00 | 1.86 | 0.32 | 0.47 | 0.08 |  | 1.00 |  |  | 1.00 | 1.00 |
| Incremental Delay d2 | 7.2 | 0.8 | 0.0 | 0.2 | 0.8 | 0.0 |  | 1.3 |  |  | 2.1 | 15 |
| Delay (s) | 10.0 | 4.2 | 3.0 | 0.7 | 2.3 | 0.2 |  | 43.4 |  |  | 44.7 | 43.9 |
| Level of Service | B | A | A | A | A | A |  | D |  |  | D | D |
| Approach Delay (s) |  | 4.4 |  |  | 2.3 |  |  | 43.4 |  |  | 44.2 |  |
| Approach LOS |  | A |  |  | A |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 5.6 |  | HCM Lev | vel of Se | ervice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.62 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 100.0 |  | Sum of lo | ost time |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 68.3\% |  | ICU Leve | el of Ser | vice |  | C |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

Analysis Period (min)
c Critical Lane Group

|  | 4 |  |  | $\checkmark$ |  |  | 4 | 4 | 7 |  | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBI | SBT | SBR |
| Lane Configurations | \% | 4 4 | * | ${ }^{*}$ | 4 | F' | \% | F |  | \% | + | \% |
| Ideal Flow (vphpl) | 1900. | 1900 | 1900. | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Util Factor | 1.00 | 0.95 | 100 | 1.00 | 0.95 | 100 | 1.00 | 1.00 |  | 1.00 | 100 | 100 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.89 |  | 1.00 | 1.00 | 0.85 |
| Flt Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) | 1770 | 3471 | 1583 | 1770 | 3471 | 1583 | 1770 | 1657 |  | 1770 | 1863 | 1583 |
| Fit Permitted | 0.22 | 1.00 | 100 | 0.33 | 1.00 | 1.00 | 0.56 | 100 |  | 0.75 | 1.00 | 100 |
| Satd. Flow (perm) | 412 | 3471 | 1583 | 612 | 3471 | 1583 | 1041 | 1657 |  | 1388 | 1863 | 1583 |
| Volume (vph) | 116 | 820 | 280 | 45 | 960 | 18 | 55 | 3 | 10 | 28 | 25 | 197 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.85 | 0.95 | 0.75 | 0.85 | 0.60 | 0.70 | 0.80 | 0.80 | 0.95 |
| Adj Flow (vph) | 122 | 863 | 295 | 53 | 1011 | 24 | 65 | 5 | 14 | 35 | 31 | 207 |
| RTOR Reduction (vph) | 0 | 0 | 71 | 0 | 0 | 8 | 0 | 11 | 0 | 0 | 0 | 188 |
| Lane Group Flow (vph) | 122. | 863 | 224 | 53 | 1011 | 16 | 65 | 8 | 0 | 35 | 31 | 19 |
| Heavy Vehicles (\%) | 2\% | 4\% | 2\% | 2\% | 4\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Tum Type | pm+pt |  | Perm | Perm |  | Perm | pm+pt |  |  | Perm |  | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  | 5 | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  |  | 6 |  | 6 |
| Actuated Green, G (s) | 74.8 | 74.8 | 74.8 | 63.6 | 63.6 | 63.6 | 17.2 | 17.2 |  | 8.4 | 8.4 | 8.4 |
| Effective Green, g (s) | 75.8 | 75.8 | 75.8 | 64.6 | 64.6 | 64.6 | 18.2 | 18.2 |  | 9.4 | 9.4 | 9.4 |
| Actuated g/C Ratio | 0.76 | 0.76 | 0.76 | 0.65 | 0.65 | 0.65 | 0.18 | 0.18 |  | 0.09 | 0.09 | 0.09 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (Vph) | 424 | 2631 | 1200 | 395 | 2242 | 1023 | 232 | 302 |  | 130 | 175 | 149 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | 0.02 | c0. 25 |  |  | c0.29 |  | c0.02 | 0.00 |  |  | 0.02 |  |
| $\mathrm{V} / \mathrm{s}$ Ratio Perm | 0.19 |  | 0.14 | 0.09 |  | 0.01 | c0.03 |  |  | 0.03 |  | 0.01 |
| v/c Ratio | 0.29 | 0.33 | 0.19 | 0.13 | 0.45 | 0.02 | 0.28 | 0.02 |  | 0.27 | 0.18 | 0.13 |
| Uniform Delay, d1 | 4.6 | 3.9 | 3.4 | 6.9 | 8.8 | 6.3 | 34.8 | 33.6 |  | 42.1 | 41.7 | 41.6 |
| Progression Factor | 0.50 | 0.36 | 0.52 | 0.96 | 1.00 | 1.05 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 0.3 | 0.3 | 0.3 | 0.7 | 0.6 | 0.0 | 0.7 | 0.0 |  | 11. | 0.5 | 0.4 |
| Delay (s) | 2.6 | 1.7 | 2.1 | 7.3 | 9.5 | 6.7 | 35.4 | 33.6 |  | 43.2 | 42.2 | 42.0 |
| Level of Service | A | A | A | A | A | A | D | C |  | D | D | D |
| Approach Delay (s) |  | 1.9 |  |  | 9.3 |  |  | 35.0 |  |  | 42.1 |  |
| Approach LOS |  | A |  |  | A |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 9.9 |  | HCM Le | vel of S | ervice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.41 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s)... |  |  | 100.0 |  | Sum of 1 | ost time |  |  | 9.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 52.7\% |  | ICU Lev | l of Se | vice |  | A |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


|  | $\rangle$ | $\rightarrow$ |  | $\checkmark$ |  |  | , | 4 | 1 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBE | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{*}$ | 4 | $\stackrel{\square}{7}$ | \% | $4 \uparrow$ | ${ }^{7}$ | ${ }^{*}$ | F |  | ${ }^{7}$ | 4 | 7 |
| \|deal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor | 1.00 | 0.95 | 100 | 100 | 0.95 | 1.00 | 1.00 | 100 |  | 100 | 1.00 | 100 |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.91 |  | 1.00 | 1.00 | 0.85 |
| Fil Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 100 | 0.95 | 1.00 |  | 0.95 | 100 | 1.00 |
| Satd. Flow (prot) | 1770 | 3471 | 1583 | 1770 | 3471 | 1583 | 1770 | 1702 |  | 1770 | 1863 | 1583 |
| Fit Permitted | 013 | 1.00 | 100 | 021 | 1.00 | 1.00 | 0.59 | 100 |  | 070 | 100 | 1.00 |
| Satd. Flow (perm) | 242 | 3471 | 1583 | 391 | 3471 | 1583 | 1097 | 1702 |  | 1313 | 1863 | 1583 |
| Volume (vph) | 395 | 1245 | 60 | 10 | 1105 | 60 | 220 | 29 | 39 | 53 | 20 | 330 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.85 | 0.70 | 0.95 | 0.85 | 0.95 | 0.85 | 0.85 | 0.85 | 0.80 | 0.95 |
| Adj Flow (vph) | 416 | 1311 | 71. | 14 | 1163 | 71 | 232 | 34 | 46 | 62 | 25 | 347 |
| RTOR Reduction (vph) | 0 | 0 | 20 | 0 | 0 | 35 | 0 | 36 | 0 | 0 | 0 | 241 |
| Lane Group Flow (vph) | 416 | 1311 | 51. | 14 | 1163. | 36 | 232 | 44 | 0 | 62 | 25 | 106 |
| Heavy Vehicles (\%) | 2\% | 4\% | 2\% | 2\% | 4\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | pm+pt |  | Perm | Perm |  | Perm | pm+pt |  |  | Perm |  | Perm |
| Protected Phases | 7 | 4 |  |  | 8 |  | 5 | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  |  | 6 |  | 6 |
| Actuated Green, G (s) | 71.4 | 71.4 | 71.4 | 50.0 | 50.0 | 50.0 | 20.6 | 20.6 |  | 10.6 | 10.6 | 10.6 |
| Effective Green, g (s) | 72.4 | 72.4 | 72.4 | 51.0 | 51.0 | 51.0 | 21.6 | 21.6 |  | 11.6 | 11.6 | 11.6 |
| Actuated g/C Ratio | 0.72 | 0.72 | 0.72 | 0.51 | 0.51 | 0.51 | 0.22 | 0.22 |  | 0.12 | 0.12 | 0.12 |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) | 456 | 2513 | 1146 | 199 | 1770 | 807 | 284 | 368 |  | 152 | 216 | 184 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot | c0.17 | 0.38 |  |  | 0.34 |  | c0.06 | 0.03 |  |  | 0.01 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | c0.49 |  | 0.03 | 0.04 |  | 0.02 | co 12 |  |  | 0.05 |  | 0.07 |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.91 | 0.52 | 0.04 | 0.07 | 0.66 | 0.04 | 0.82 | 0.12 |  | 0.41 | 0.12 | 0.57 |
| Uniform Delay, d1 | 24.0 | 6.1 | 3.9 | 12.5 | 18.1 | 12.3 | 36.8 | 31.5 |  | 41.0 | 39.6 | 41.9 |
| Progression Factor | 1.40 | 0.53 | 0.27 | 1.11 | 1.29 | 1.38 | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 | 18.5 | 0.6 | 0.1 | 0.6 | 17. | 0.1 | 16.4 | 0.1 |  | 18 | 0.2 | 4.3 |
| Delay (s) | 52.0 | 3.9 | 1.1 | 14.4 | 24.9 | 17.0 | 53.3 | 31.7 |  | 42.8 | 39.8 | 46.1 |
| Level of Service | D | A | A | B | C. | B | D | C |  | D | D | D |
| Approach Delay (s) |  | 14.9 |  |  | 24.3 |  |  | 47.7 |  |  | 45.3 |  |
| Approach LOS |  | B |  |  | C |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 24.2 |  | HCM Lev | el of Se | rvice |  | C |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.88 |  |  |  |  |  |  |  |  |  |
|  |  |  | 100.0 |  | Sum of lo | ost time |  |  | 6.0 |  |  |  |
| Actuated Cycle Length (s) |  |  | 81.3\% |  | CU Leve | of Ser | vice |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |






LSC, Inc.


LSC, Inc.







LSC, Inc.





LSC, Inc.







LSC, Inc.




LSC, Inc.

|  | * | $\rightarrow$ | \% | 7 |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{4}$ | 4 | 7 | \% | F |  | ${ }^{*}$ | f |  | \% | F |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Utill Factor | 1.00 | 1.00 | 100 | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 100 | 1.00 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 |  | 1.00 | 0.89 |  | 1.00 | 0.86 |  |
| Fil Protected | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |  | 0.95 | 1.00 |  | 0.95 | 100 |  |
| Satd. Flow (prot) | 1770 | 1759 | 1583 | 1770 | 1758 |  | 1770 | 1653 |  | 1770 | 1593 |  |
| Fit Permitted | 0.25 | 1.00 | 100 | 0.33 | 1.00 |  | 0.63 | 100 |  | 0.75 | 100 |  |
| Satd. Flow (perm) | 467 | 1759 | 1583 | 622 | 1758 |  | 1181 | 1653 |  | 1397 | 1593 |  |
| Volume (vph) | 135 | 700 | 158 | 9 | 870 | 6 | 88 | 2 | 6 | 3 | 2 | 75 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.70 | 0.95 | 0.65 | 0.90 | 0.60 | 0.65 | 0.60 | 0.60 | 0.90 |
| Adj Flow (vph) | 142 | 737 | 166 | 13 | 916 | 9 | 98 | 3 | 9 | 5 | 3 | 83 |
| RTOR Reduction (vph) | 0 | 0 | 33 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 72 | 0 |
| Lane Group Flow (vph) | 142 | 737 | 133 | 13 | 925 | 0 | 98 | 4 | 0 | 5 | 14 | 0 |
| Heavy Vehicles (\%) | 2\% | 8\% | 2\% | 2\% | 8\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | Perm |  | Perm | Perm |  |  | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8. |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) | 79.2 | 79.2 | 79.2 | 79.2 | 79.2 |  | 12.8 | 12.8 |  | 12.8 | 12.8 |  |
| Effective Green, $\mathrm{g}(\mathrm{s})$ | 80.2 | 80.2 | 80.2 | 80.2 | 80.2 |  | 13.8 | 13.8 |  | 13,8 | 13.8 |  |
| Actuated g/C Ratio | 0.80 | 0.80 | 0.80 | 0.80 | 0.80 |  | 0.14 | 0.14 |  | 0.14 | 0.14 |  |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 375 | 1411 | 1270 | 499 | 1410 |  | 163 | 228 |  | 193 | 220 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | 0.42 |  |  | c0.53 |  |  | 0.00 |  |  | 0.01 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm | 0.30 |  | 0.08 | 0.02 |  |  | co. 08 |  |  | 0.00 |  |  |
| $\mathrm{v} / \mathrm{c}$ Ratio | 0.38 | 0.52 | 0.10 | 0.03 | 0.66 |  | 0.60 | 0.02 |  | 0.03 | 0.07 |  |
| Uniform Delay, d1 | 28 | 3.4 | 2.1 | 20 | 4.1 |  | 40.5 | 37.2 |  | 37.3 | 37.5 |  |
| Progression Factor | 0.29 | 0.25 | 0.00 | 1.15 | 1.29 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 2.6 | 12 | 0.1 | 0.1 | 1.8 |  | 6.1 | 0.0 |  | 0.1 | 0.1 |  |
| Delay (s) | 3.4 | 2.1 | 0.2 | 2.4 | 7.2 |  | 46.6 | 37.3 |  | 37.3 | 37.6 |  |
| Level of Service | A | A | A | A | A |  | D | D |  | D | D |  |
| Approach Delay (s) |  | 1.9 |  |  | 7.1 |  |  | 45.6 |  |  | 37.6 |  |
| Approach LOS |  | A |  |  | A |  |  | D |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 78 |  | HCM Le | vel of S | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.65 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 100.0 |  | Sum of | st time |  |  | 6.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 75.2\% |  | CU Lev | of Se | vice |  | D |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |

LSC, Inc.



|  | 4 | $\rightarrow$ |  | $\%$ |  |  | 4 | 4 | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | ${ }^{4}$ | 4 | 7 | $\xi$ | $\square$ |  | \% | F |  | ${ }^{k}$ | $t$ |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Util Factor | 1.00 | 1.00 | 100 | 100 | 100 |  | 100 | 100 |  | 100 | 100 |  |
| Frt | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 |  | 1.00 | 0.93 |  | 1.00 | 0.87 |  |
| Fit Protected | 0.95 | 1.00 | 1.00 | 0.95 | 100 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) | 1770 | 1759 | 1583 | 1770 | 1756 |  | 1787 | 1734 |  | 1770 | 1616 |  |
| Fit Permitted | 0.53 | 1.00 | 100 | 0.47 | 1.00 |  | 0.95 | 1.00 |  | 0.80 | 100 |  |
| Satd. Flow (perm) | 989 | 1759 | 1583 | 881 | 1756 |  | 1787 | 1734 |  | 1490 | 1616 |  |
| Volume (vph) | 30 | 350 | 332 | 16 | 275 | 3 | 144 | 10 | 8 | 6 | 10 | 100 |
| Peak-hour factor, PHF | 0.85 | 0.95 | 0.95 | 0.75 | 0.95 | 0.60 | 0.95 | 0.70 | 0.65 | 0.65 | 0.70 | 0.95 |
| Adj. Flow (vph) | 35 | 368 | 349 | 21 | 289 | 5 | 152 | 14 | 12 | 9 | 14 | 105 |
| RTOR Reduction (vph) | 0 | 0 | 143 | 0 | 1 | 0 | 0 | 9 | 0 | 0 | 100 | 0 |
| Lane Group Flow (vph) | 35 | 368 | 206 | 21 | 293 | 0 | 152 | 17. | 0 | 9 | 19 | 0 |
| Heavy Vehicles (\%) | 2\% | 8\% | 2\% | 2\% | 8\% | 2\% | 1\% | 2\% | 2\% | 2\% | 2\% | 2\% |
| Turn Type | Perm |  | Perm | Perm |  |  | Split |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  | 2 | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  |  |  |  |  | 6 |  |  |
| Actuated Green, G (s) | 58.0 | 58.0 | 58.0 | 58.0 | 58.0 |  | 26.0 | 26.0 |  | 4.0 | 4.0 |  |
| Effective Green, g (s) | 59.0 | 59.0 | 59.0 | 59.0 | 59.0 |  | 27.0 | 27.0 |  | 5.0 | 5.0 |  |
| Actuated g/C Ratio | 0.59 | 0.59 | 0.59 | 0.59 | 0.59 |  | 0.27 | 0.27 |  | 0.05 | 0.05 |  |
| Clearance Time (s) | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Vehicle Extension (s) | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) | 584 | 1038 | 934 | 520 | 1036 |  | 482 | 468 |  | 75 | 81 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | c0. 21 |  |  | 0.17 |  | c0.09 | 0.01 |  |  | c0.01 |  |
| $\mathrm{V} / \mathrm{s}$ Ratio Perm | 0.04 |  | 0.13 | 0.02 |  |  |  |  |  | 0.01 |  |  |
| v/c Ratio | 0.06 | 0.35 | 0.22 | 0.04 | 0.28 |  | 0.32 | 0.04 |  | 0.12 | 0.24 |  |
| Uniform Delay, d1 | 8.7 | 10.6 | 9.7 | 8.6 | 10.1 |  | 29.1 | 26.9 |  | 45.4 | 45.7 |  |
| Progression Factor | 0.47 | 0.61 | 2.28 | 1.00 | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 | 0.2 | 0.8 | 0.5 | 0.1 | 0.7 |  | 1.7 | 0.1 |  | 0.7 | 1.5 |  |
| Delay (s) | 4.3 | 7.3 | 22.5 | 8.8 | 10.8 |  | 30.8 | 27.1 |  | 46.1 | 47.2 |  |
| Level of Service | A | A | C | A | B |  | C | C |  | D | D |  |
| Approach Delay (s) |  | 14.2 |  |  | 10.6 |  |  | 30.3 |  |  | 47.1 |  |
| Approach LOS |  | B |  |  | B |  |  | C |  |  | D |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 18.6 |  | HCM Le | el of S | ervice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.34 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 100.0 |  | Sum of | ost time | (s) |  | 9.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 46.2\% |  | ICU Lev | l of Se | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

Analysis Period (min) 15
c Critical Lane Group

LSC, Inc.

c Critical Lane Group


LSC, Inc.



LSC, Inc.


| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\ddagger$ |  |  | $\stackrel{ }{*}$ |  | ${ }^{*}$ | 餄 |  | * | 性 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Lane Util Factor |  | 1.00 |  |  | 100 |  | 1.00 | 0.95 |  | 1.00 | 0.95 |  |
| Frt |  | 0.96 |  |  | 0.94 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  |
| Flt Protected |  | 0.98 |  |  | 0.99 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) |  | 1746 |  |  | 1749 |  | 1770 | 3363 |  | 1770 | 3343 |  |
| Fit Permitted |  | 0.86 |  |  | 0.96 |  | 0.38 | 1.00 |  | 0.45 | 1.00 |  |
| Satd. Flow (perm) |  | 1529 |  |  | 1690 |  | 704 | 3363 |  | 846 | 3343 |  |
| Volume (vph) | 52 | 30 | 39 | 8 | 41 | 36 | 22 | 490 | 11 | 48 | 605 | 53 |
| Peak-hour factor, PHF | 0.85 | 0.80 | 0.85 | 0.65 | 0.85 | 0.85 | 0.80 | 0.95 | 0.70 | 0.85 | 0.95 | 0.85 |
| Adj Flow (vph) | 61 | 38 | 46 | 12 | 48 | 42 | 28 | 516 | 16 | 56 | 637 | 62 |
| RTOR Reduction (vph) | 0 | 38 | 0 | 0 | 34 | 0 | 0 | 3 | 0 | 0 | 8 | 0 |
| Lane Group Flow (vph) | 0 | 107 | 0 | 0 | 68 | 0 | 28 | 529 | 0 | 56 | 691 | 0 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 7\% | 2\% | 2\% | 7\% | 2\% |
| Turn Type | Perm |  |  | Perm |  |  | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 9.9 |  |  | 9.9 |  | 39.5 | 39.5 |  | 39.5 | 39.5 |  |
| Effective Green, g (s) |  | 10.9 |  |  | 10.9 |  | 40.5 | 40.5 |  | 40.5 | 40.5 |  |
| Actuated g/C Ratio |  | 0.18 |  |  | 0.18 |  | 0.68 | 0.68 |  | 0.68 | 0.68 |  |
| Clearance Time (s) |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| tane Grp Cap (vph) |  | 281 |  |  | 310 |  | 480 | 2293 |  | 577 | 2279 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  | 0.16 |  |  | c0.21 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | c0.07 |  |  | 0.04 |  | 0.04 |  |  | 0.07 |  |  |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.38 |  |  | 0.22 |  | 0.06 | 0.23 |  | 0.10 | 0.30 |  |
| Uniform Delay, d1 |  | 21.3 |  |  | 20.6 |  | 3.1 | 3.6 |  | 3.2 | 3.8 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 |  | 0.9 |  |  | 0.4 |  | 0.2 | 0.2 |  | 0.3 | 0.3 |  |
| Delay (s) |  | 22.2 |  |  | 21.0 |  | 3.4 | 3.8 |  | 3.6 | 4.1 |  |
| Level of Service |  | C |  |  | C |  | A | A |  | A | A |  |
| Approach Delay (s) |  | 22.2 |  |  | 21.0 |  |  | 3.8 |  |  | 4.1 |  |
| Approach LOS |  | C |  |  | c |  |  | A |  |  | A |  |
| intersection summary |  |  |  |  |  |  |  |  |  |  |  |  |

intersection Summary



LSC, Inc.

|  | $\rangle$ |  |  |  |  |  | 4 | $\dagger$ | 7 |  | $\dagger$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBE | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\oplus$ |  |  | $\dagger$ |  | ${ }^{4}$ | 性 |  | ${ }_{1}$ | 侾 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 |  |  | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  |
| Lane Util Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 0.95 |  | 1.00 | 0.95 |  |
| Frt |  | 0.96 |  |  | 0.94 |  | 1.00 | 0.99 |  | 1.00 | 0.99 |  |
| Filt Protected |  | 0.98 |  |  | 0.99 |  | 095 | 1.00 |  | 0.95 | 100 |  |
| Satd. Flow (prot) |  | 1746 |  |  | 1738 |  | 1770 | 3361 |  | 1770 | 3344 |  |
| Flt Permitted |  | 0.81 |  |  | 0.94 |  | 0.31 | 1.00 |  | 0.39 | 1.00 |  |
| Satd. Flow (perm) |  | 1451 |  |  | 1642 |  | 583 | 3361 |  | 732 | 3344 |  |
| Volume (vph) | 75 | 40 | 50 | 20 | 50 | 55 | 30 | 610 | 20 | 60 | 735 | 60 |
| Peak-hour factor, PHF | 0.90 | 0.85 | 0.85 | 0.80 | 0.85 | 0.85 | 0.85 | 0.95 | 0.80 | 0.85 | 0.95 | 0.85 |
| Adj. Flow (vph) | 83 | 47 | 59 | 25 | 59 | 65 | 35 | 642 | 25 | 71 | 774 | 71 |
| RTOR Reduction (vph) | 0 | 38 | 0 | 0 | 52 | 0 | 0 | 4 | 0 | 0 | 9 | 0 |
| Lane Group Flow (vph) | 0 | 151 | 0 | 0 | 97 | 0 | 35 | 663 | 0 | 71 | 836 | 0 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 7\% | 2\% | 2\% | 7\% | 2\% |
| Turn Type | Perm |  |  | Perm |  |  | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 9.2 |  |  | 9.2 |  | 30.3 | 30.3 |  | 30.3 | 30.3 |  |
| Effective Green, g ( $s$ ) |  | 10.2 |  |  | 10.2 |  | 31.3 | 31.3 |  | 31.3 | 31.3 |  |
| Actuated g/C Ratio |  | 0.21 |  |  | 0.21 |  | 0.63 | 0.63 |  | 0.63 | 0.63 |  |
| Clearance Time (s) |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) |  | 299 |  |  | 338 |  | 369 | 2125 |  | 463 | 2114 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  | 0.20 |  |  | c0. 25 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | co. 10 |  |  | 0.06 |  | 0.06 |  |  | 0.10 |  |  |
| v/c Ratio |  | 0.50 |  |  | 0.29 |  | 0.09 | 0.31 |  | 0.15 | 0.40 |  |
| Uniform Delay, d1 |  | 17.4 |  |  | 16.6 |  | 3.6 | 4.2 |  | 3.7 | 4.5 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.00 | 1.00 |  | 1.00 | 1.00 |  |
| Incremental Delay, d2 |  | 1.3 |  |  | 0.5 |  | 0.5 | 0.4 |  | 0.7 | 0.6 |  |
| Delay (s) |  | 18.8 |  |  | 17.1 |  | 4.1 | 4.6 |  | 4.4 | 5.0 |  |
| Level of Service |  | B |  |  | B |  | A | A |  | A | A |  |
| Approach Delay (s) |  | 18.8 |  |  | 17.1 |  |  | 4.5 |  |  | 5.0 |  |
| Approach LOS |  | B |  |  | B |  |  | A |  |  | A |  |
| ntersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 7.1 |  | HCM Le | el of S | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.42 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 49.5 |  | Sum of | st time |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 51.5\% |  | ICU Leve | of Se | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


|  | 4 |  |  |  |  |  | 4 | $\dagger$ | $p$ |  | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | $\dagger$ |  | ${ }^{4}$ | 4t |  | ${ }_{1}$ | 49 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Util. Factor |  | 1.00 |  |  | 100 |  | 1.00 | 0.95 |  | 100 | 0.95 |  |
| Frt |  | 0.95 |  |  | 0.96 |  | 1.00 | 1.00 |  | 1.00 | 0.98 |  |
| Fit Protected |  | 0.99 |  |  | 0.99 |  | 0.95 | 1.00 |  | 0.95 | 100 |  |
| Satd. Flow (prot) |  | 1751 |  |  | 1786 |  | 1770 | 3397 |  | 1770 | 3365 |  |
| Fit Permitted |  | 0.82 |  |  | 0.95 |  | 0.38 | 1.00 |  | 0.41 | 1.00 |  |
| Satd. Flow (perm) |  | 1452 |  |  | 1703 |  | 715 | 3397 |  | 758 | 3365 |  |
| Volume (vph) | 50 | 65 | 60 | 10 | 70 | 30 | 50 | 570 | 10 | 55 | 565 | 60 |
| Peak-hour factor, PHF | 0.85 | 0.85 | 0.85 | 0.70 | 0.85 | 0.85 | 0.85 | 0.95 | 0.70 | 0.85 | 0.95 | 0.85 |
| Adj Flow (vph) | 59 | 76 | 71 | 14 | 82 | 35 | 59 | 600 | 14. | 65 | 595 | 71 |
| RTOR Reduction (vph) | 0 | 23 | 0 | 0 | 16 | 0 | 0 | 1 | 0 | 0 | 6 | 0 |
| Lane Group Flow (vph) | 0 | 183 | 0 | 0 | 115 | 0 | 59 | 613 | 0 | 65 | 660 | 0 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 6\% | 2\% | 2\% | 6\% | 2\% |
| Turn Type | Perm |  |  | Perm |  |  | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 16.0 |  |  | 16.0 |  | 74.0 | 74.0 |  | 74.0 | 74.0 |  |
| Effective Green, g (s) |  | 18.0 |  |  | 18.0 |  | 76.0 | 76.0 |  | 76.0 | 76.0 |  |
| Actuated g/C Ratio |  | 0.18 |  |  | 0.18 |  | 0.76 | 0.76 |  | 0.76 | 0.76 |  |
| Clearance Time (s) |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) |  | 261 |  |  | 307 |  | 543 | 2582 |  | 576 | 2557 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  | 0.18 |  |  | c0. 20 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | co. 13 |  |  | 0.07 |  | 0.08 |  |  | 0.09 |  |  |
| v/c Ratio |  | 0.70 |  |  | 0.38 |  | 0.11 | 0.24 |  | 0.11 | 0.26 |  |
| Uniform Delay, d1 |  | 38.5 |  |  | 36.1 |  | 3.1 | 3.5 |  | 3.2 | 3.6 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.26 | 1.31 |  | 0.91 | 0.97 |  |
| Incremental Delay, d2 |  | 8.2 |  |  | 0.8 |  | 0.4 | 0.2 |  | 0.4 | 0.2 |  |
| Delay (s) |  | 46.7 |  |  | 36.8 |  | 4.3 | 4.8 |  | 3.3 | 3.7 |  |
| Level of Service |  | D |  |  | D |  | A | A |  | A | A |  |
| Approach Delay (s) |  | 46.7 |  |  | 36.8 |  |  | 4.7 |  |  | 3.7 |  |
| Approach LOS |  | D |  |  | D |  |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 117 |  | HCM Le | el of S | rvice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.34 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 100.0 |  | Sum of | st tim |  |  | 6.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 47.4\% |  | ICU Leve | of Se | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| C Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


|  | * |  |  |  |  |  | 4 | $\dagger$ | 7 | \% | $\downarrow$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | \$ |  | \% | 中t |  | * | 性 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Util, Factor |  | 100 |  |  | 100 |  | 1.00 | 0.95 |  | 100 | 0.95 |  |
| Frt |  | 0.95 |  |  | 0.95 |  | 1.00 | 1.00 |  | 1.00 | 0.99 |  |
| Fit Protected |  | 0.99 |  |  | 0.99 |  | 0.95 | 1.00 |  | 0.95 | 1.00 |  |
| Satd. Flow (prot) |  | 1750 |  |  | 1759 |  | 1770 | 3394 |  | 1770 | 3378 |  |
| Flt Permitted |  | 0.76 |  |  | 0.92 |  | 0.25 | 1.00 |  | 0.30 | 1.00 |  |
| Satd. Flow (perm) |  | 1356 |  |  | 1629 |  | 462 | 3394 |  | 566 | 3378 |  |
| Volume (vph) | 75 | 105 | 95 | 20 | 100 | 65 | 80 | 770 | 20 | 70 | 880 | 60 |
| Peak-hour factor, PHF | 0.90 | 0.95 | 0.90 | 0.80 | 0.95 | 0.85 | 0.90 | 0.95 | 0.80 | 0.85 | 0.95 | 0.85 |
| Adj Flow (vph) | 83 | 111 | 106 | 25 | 105 | 76 | 89 | 811 | 25 | 82 | 926 | 71 |
| RTOR Reduction (vph) | 0 | 22 | 0 | 0 | 23 | 0 | 0 | 2 | 0 | 0 | 5 | 0 |
| Lane Group Flow (vph) | 0 | 278 | 0 | 0 | 183 | 0 | 89 | 834 | 0 | 82 | 992 | 0 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 6\% | 2\% | 2\% | 6\% | 2\% |
| Turn Type | Perm |  |  | Perm |  |  | Perm |  |  | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |  |
| Actuated Green, G (s) |  | 22.5 |  |  | 22.5 |  | 67.5 | 67.5 |  | 67.5 | 67.5 |  |
| Effective Green, g (s) |  | 24.5 |  |  | 24.5 |  | 69.5 | 69.5 |  | 69.5 | 69.5 |  |
| Actuated g/C Ratio |  | 0.24 |  |  | 0.24 |  | 0.70 | 0.70 |  | 0.70 | 0.70 |  |
| Clearance Time (s) |  | 5.0 |  |  | 5.0 |  | 5.0 | 5.0 |  | 5.0 | 5.0 |  |
| Vehicle Extension (s) |  | 3.0 |  |  | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) |  | 332 |  |  | 399 |  | 321 | 2359 |  | 393 | 2348 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  | 0.25 |  |  | c0.29 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | c0.21 |  |  | 0.11 |  | 0.19 |  |  | 0.14 |  |  |
| v/c Ratio |  | 0.84 |  |  | 0.46 |  | 0.28 | 0.35 |  | 0.21 | 0.42 |  |
| Uniform Delay, d1 |  | 35.9 |  |  | 32.1 |  | 5.8 | 6.2 |  | 5.4 | 6.6 |  |
| Progression Factor |  | 1.00 |  |  | 1.00 |  | 1.19 | 1.13 |  | 1.04 | 1.11 |  |
| Incremental Delay, d2 |  | 16.6 |  |  | 0.8 |  | 1.5 | 0.3 |  | 12 | 0.5 |  |
| Delay (s) |  | 52.5 |  |  | 32.9 |  | 8.3 | 7.3 |  | 6.8 | 7.8 |  |
| Level of Service |  | D |  |  | C |  | A | A |  | A | A |  |
| Approach Delay (s) |  | 52.5 |  |  | 32.9 |  |  | 7.4 |  |  | 7.8 |  |
| Approach LOS |  | D |  |  | C |  |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 15.0 |  | HCM Level of Service |  |  |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.53 |  | Sum of lost time (s) |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 100.0 |  |  |  |  |  | 6.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 69.8\% |  | ICU Level of Service |  |  |  | C |  |  |  |

Analysis Period (min) 15
c Critical Lane Group


HCM Unsignalized Intersection Capacity Analysis

## 22: Georgia \& SH 135

| Movement | EBL | EBT | EBR | WBL | WBT | WBE | NBL | NBT | NBR |  | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | 4 |  |  | 4 |  | ${ }_{1}$ | 个中 |  | ${ }^{7}$ | $\uparrow$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 20 | 10 | 15 | 5 | 10 |  | 515 | 515 | 10 | 45 | 475 | 45 |
| Peak Hour Factor | 0.80 | 0.70 | 0.75 | 0.65 | 0.70 | 0.80 | 0.75 | 0.95 | 0.70 | 0.85 | 0.95 | 0.85 |
| Hourly flow rate (vph) | 25 | 14 | 20 | 8 | 14 | 25 | 20 | 542 | 14 | 53 | 500 | 53 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{ft} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  | 410 |  |  |  |  |
| pX, platoon unblocked |  |  |  |  |  |  |  |  |  |  |  |  |
| VC, conflicting volume | 976 | 1229 | 276 | 972 | 1248 | 278 | 553 |  |  | 556 |  |  |
| vC1, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 976 | 1229 | 276 | 972 | 1248 | 278 | 553 |  |  | 556 |  |  |
| tc, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC, 2 stage ( s ) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 86 | 91 | 97 | 96 | 91 | 97 | 98 |  |  | 95 |  |  |
| cM capacity (veh/h) | 175 | 164 | 721 | 178 | 160 | 719 | 1013 |  |  | 1010 |  |  |
| Pirecton, Lane \# | EB1 | WB1 | NB1 | NB2 | NB 3 | SB1 | SB2 | SB3 |  |  |  |  |
| Volume Total | 59 | 47 | 20 | 361 | 195 | 53 | 333 | 220 |  |  |  |  |
| Volume Left | 25 | 8 | 20 | 0 | 0 | 53 | 0 | 0 |  |  |  |  |
| Volume Right | 20 | 25 | 0 | 0 | 14 | 0 | 0 | 53 |  |  |  |  |
| CSH | 230 | 280 | 1013 | 1700 | 1700 | 1010 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.26 | 0.17 | 0.02 | 0.21 | 0.11 | 005 | 0.20 | 0.13 |  |  |  |  |
| Queue Length 95th (ft) | 25 | 15 | 2 | 0 | 0 | 4 | 0 | 0 |  |  |  |  |
| Control Delay (s) | 26.0 | 20.4 | 8.6 | 0.0 | 00 | 8.8 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | D | C | A |  |  | A |  |  |  |  |  |  |
| Approach Delay (s) | 26.0 | 20.4 | 0.3 |  |  | 0.8 |  |  |  |  |  |  |
| Approach LOS | D | C |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay 2.4 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity UtilizationAnalysis Period (min) |  | - $34.0 \%$ |  | ICU Level of Service |  |  |  |  | A |  |  |  |
|  |  | 15 |  |  |  |  |  |  |  |  |  |  |


|  |  |  |  | 7 |  |  | 4 | 4 | 7 |  | $\downarrow$ | * |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | ERL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 |  |  | $\oplus$ |  | ${ }_{1}$ | 19 |  | ${ }_{5}$ | $\uparrow \uparrow$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 35 | 10. | 25 | 15 | 10 | 35 | 25 | 700 | 15 | 30 | 815 | 30 |
| Peak Hour Factor | 0.85 | 0.70 | 0.80 | 0.75 | 0.70 | 0.85 | 0.85 | 0.95 | 0.75 | 0.85 | 0.95 | 0.85 |
| Hourly flow rate (vph) | 41 | 14 | 31 | 20 | 14 | 41 | 29 | 737 | 20 | 35 | 858 | 35 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed ( $\mathrm{ft} / \mathrm{s}$ ) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) . |  |  |  |  |  |  |  |  |  |  |  |  |
| PX, platoon unblocked | 0.95 | 0.95 |  | 0.95 | 0.95 | 0.95 |  |  |  | 0.95 |  |  |
| vC, conflicting volume | 1422 | 1762 | 447 | 1344 | 1769 | 378 | 893 |  |  | 757. |  |  |
| $\mathrm{VC1}$, stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 1392 | 1749 | 447 | 1309 | 1757 | 294 | 893 |  |  | 692 |  |  |
| tc, single (s) | 7.5 | 6.5 | 6.9 | 75 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| $\mathrm{tc}, 2$ stage ( s ) |  |  |  |  |  |  |  |  |  |  |  |  |
| tr (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| po queue free \% | 43 | 81 | 94 | 76 | 81 | 94 | 96 |  |  | 96 |  |  |
| cM capacity (veh/h) | 73 | 74 | 559 | 84 | 74 | 668 | 755 |  |  | 854 |  |  |
| Direction, Lane \# EB1 WB1 NB1 NB 2 NB3 SB1 SB2 SB3 |  |  |  |  |  |  |  |  |  |  |  |  |
| Volume Total | 87 | 75 | 29 | 491 | 266 | 35 | 572 | 321 |  |  |  |  |
| Volume Left | 41 | 20 | 29 | 0 | 0 | 35 | 0 | 0 |  |  |  |  |
| Volume Right | 31 | 41 | 0 | 0 | 20 | 0 | 0 | 35 |  |  |  |  |
| CSH | 106 | 153 | 755 | 1700 | 1700 | 854 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 082 | 0.49 | 0.04 | 029 | 0.16 | 0.04 | 0.34 | 0.19 |  |  |  |  |
| Queue Length 95th (ft) | 115 | 59 | 3 | 0 | 0 | 3 | 0 | 0 |  |  |  |  |
| Control Delay (s) | 116.4 | 49.6 | 10.0 | 0.0 | 0.0 | 9.4 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | F | E | A |  |  | A |  |  |  |  |  |  |
| Approach Delay (s) | 116.4 | 49.6 | 0.4 |  |  | 0.4 |  |  |  |  |  |  |
| Approach LOS | F | E |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay 7.7 |  |  |  |  |  |  |  |  |  |  |  |  |
| Intersection Capacity UtilizationAnalysis Period (min) |  |  | 39,1\% | ICU Level of Service |  |  |  |  | A |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |


|  | 4 |  |  | 7 |  |  | 4 | 4 | 7 |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | ¢ |  | ${ }^{4}$ | 个t |  | 4 | 中 ${ }^{\text {a }}$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 20 | 15 | 35 | 5 | 20 | 25 | 30 | 600 | 10 | 50 | 590 | 45 |
| Peak Hour Factor | 0.80 | 0.75 | 0.85 | 0.65 | 0.80 | 0.85 | 0.85 | 0.95 | 0.70 | 0.85 | 0.95 | 0.85 |
| Hourly flow rate (vph) | 25 | 20 | 41 | 8 | 25 | 29 | 35. | 632 | 14 | 59 | 621 | 53 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (tt/s) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  | 410 |  |  |  |  |
| pX, platoon unblocked | 0.99 | 0.99 |  | 0.99 | 0.99 | 0.99 |  |  |  | 0.99 |  |  |
| VC, conflicting volume | 1193 | 1482 | 337 | 1189 | 1501 | 323 | 674 |  |  | 646 |  |  |
| vC 1 , stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu, unblocked vol | 1181 | 1474 | 337 | 1176 | 1493 | 298 | 674 |  |  | 626 |  |  |
| tc, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tC, 2 stage ( s ) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 76 | 82 | 94 | 93 | 77 | 96 | 96 |  |  | 94 |  |  |
| cM capacity (veh/h) | 104 | 111 | 659 | 108 | 108 | 688 | 913 |  |  | 938 |  |  |
| Direction, Lane \# | EB1 | WB 1 | NB 1 | NB 2 | NB3 | SB1 | SB2 | SB 3 |  |  |  |  |
| Volume Total | 86 | 62 | 35 | 421 | 225 | 59 | 414 | 260 |  |  |  |  |
| Volume Left | 25 | 8 | 35 | 0 | 0 | 59 | 0 | 0 |  |  |  |  |
| Volume Right | 41 | 29 | 0 | 0 | 14 | 0 | 0 | 53 |  |  |  |  |
| CSH | 179 | 180 | 913 | 1700 | 1700 | 938 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 0.48 | 0.34 | 0.04 | 0.25 | 0.13 | 0.06 | 0.24 | 0.15 |  |  |  |  |
| Queue Length 95th (ft) | 58 | 36 | 3 | 0 | 0 | 5 | 0 | 0 |  |  |  |  |
| Control Delay (s) | 42.5 | 35.1 | 9.1 | 0.0 | 0.0 | 9.1 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | E | E | A |  |  | A |  |  |  |  |  |  |
| Approach Delay (s) | 42.5 | 35.1 | 0.5 |  |  | 0.7 |  |  |  |  |  |  |
| Approach LOS | E | E |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 4.3 |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 39.7\% | ICU Level of Service |  |  |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |



| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations |  | $\dagger$ |  |  | $\uparrow$ |  | ${ }^{*}$ | 中 |  | \% | 4t |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Free |  |  | Free |  |
| Grade |  | 0\% |  |  | 0\% |  |  | 0\% |  |  | 0\% |  |
| Volume (veh/h) | 35 | 20 | 65 | 15 | 20 | 40 | 50 | 835 | 15 | 35 | 920 | 30 |
| Peak Hour Factor | 0.85 | 0.80 | 0.85 | 0.75 | 0.80 | 0.85 | 0.85 | 0.95 | 0.75 | 0.85 | 0.95 | 0.85 |
| Hourly flow rate (vph) | 41 | 25 | 76 | 20 | 25 | 47 | 59 | 879 | 20 | 41 | 968 | 35 |
| Pedestrians |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Width (ft) |  |  |  |  |  |  |  |  |  |  |  |  |
| Walking Speed (fts) |  |  |  |  |  |  |  |  |  |  |  |  |
| Percent Blockage |  |  |  |  |  |  |  |  |  |  |  |  |
| Right turn flare (veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Median type |  | None |  |  | None |  |  |  |  |  |  |  |
| Median storage veh) |  |  |  |  |  |  |  |  |  |  |  |  |
| Upstream signal (ft) |  |  |  |  |  |  |  | 410 |  |  |  |  |
| pX , platoon unblocked | 0.93 | 0.93 |  | 0.93 | 0.93 | 0.93 |  |  |  | 0.93 |  |  |
| VC, conflicting volume | 1685 | 2085 | 502 | 1662 | 2093 | 449 | 1004 |  |  | 899 |  |  |
| VC 1 , stage 1 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| VC2, stage 2 conf vol |  |  |  |  |  |  |  |  |  |  |  |  |
| vCu , unblocked vol | 1660 | 2092 | 502 | 1635 | 2100 | 324 | 1004 |  |  | 810 |  |  |
| tc, single (s) | 7.5 | 6.5 | 6.9 | 7.5 | 6.5 | 6.9 | 4.1 |  |  | 4.1 |  |  |
| tc, 2 stage (s) |  |  |  |  |  |  |  |  |  |  |  |  |
| tF (s) | 3.5 | 4.0 | 3.3 | 3.5 | 4.0 | 3.3 | 2.2 |  |  | 2.2 |  |  |
| p0 queue free \% | 0 | 40 | 85 | 19 | 39 | 92 | 91 |  |  | 95 |  |  |
| cM capacity (veh/h) | 25 | 41 | 515 | 25 | 41 | 621 | 686 |  |  | 751 |  |  |
| Oirection, Lane \# | EB 1 | WB 1 | NB 1 | NB 2 | NB 3 | SB 1 | SB2 | SB 3 |  |  |  |  |
| Volume Total | 143 | 92 | 59 | 586 | 313 | 41 | 646 | 358 |  |  |  |  |
| Volume Left | 41 | 20 | 59 | 0 | 0 | 41 | 0 | 0 |  |  |  |  |
| Volume Right | 76 | 47 | 0 | 0 | 20 | 0 | 0 | 35 |  |  |  |  |
| CSH | 60 | 62 | 686 | 1700 | 1700 | 751 | 1700 | 1700 |  |  |  |  |
| Volume to Capacity | 2.37 | 1.49 | 0.09 | 0.34 | 0.18 | 0.05 | 0.38 | 0.21 |  |  |  |  |
| Queue Length 95th (ft) | 353 | 202 | 7 | 0 | 0 | 4 | 0 | 0 |  |  |  |  |
| Control Delay (s) | 771.6 | 401.8 | 10.7 | 0.0 | 0.0 | 10.1 | 0.0 | 0.0 |  |  |  |  |
| Lane LOS | F | F | B |  |  | B |  |  |  |  |  |  |
| Approach Delay (s) | 771.6 | 4018 | 0.7 |  |  | 0.4 |  |  |  |  |  |  |
| Approach LOS | F | F |  |  |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Average Delay |  |  | 66.2 |  |  |  |  |  |  |  |  |  |
|  |  |  | 50.6\% | ICU Level of Service |  |  |  |  | A |  |  |  |
|  |  |  | 15 |  |  |  |  |  |  |  |  |  |


|  | $\stackrel{ }{*}$ |  |  |  |  | 4 | 4 | 4 | P |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | F |  | 4 | F | ${ }^{7}$ | 4 $\uparrow$ | " | 7 | 中t |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |  |
| Lane Util. Factor |  | 100 | 100 |  | 1.00 | 1.00 | 100 | 0.95 | 1.00 | 1.00 | 0.95 |  |
| Frt |  | 1.00 | 0.85 |  | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 0.97 |  |
| Flt Protected |  | 0.97 | 1.00 |  | 0.98 | 1.00 | 0.95 | 100 | 1.00 | 0.95 | 1.00 |  |
| Satd. Flow (prot) |  | 1810 | 1583 |  | 1822 | 1583 | 1770 | 3374 | 1583 | 1770 | 3294 |  |
| Flt Permitted |  | 0.79 | 1.00 |  | 0.82 | 1.00 | 0.47 | 1.00 | 1.00 | 0.58 | 1.00 |  |
| Satd. Flow (perm) |  | 1462 | 1583 |  | 1531 | 1583 | 872 | 3374 | 1583 | 1081 | 3294 |  |
| Volume (vph) | 48 | 34 | 30 | 22 | 27 | 17 | 42 | 265 | 19 | 21 | 368 | 108 |
| Peak-hour factor, PHF | 0.85 | 0.85 | 0.85 | 0.80 | 0.80 | 0.75 | 0.85 | 0.95 | 0.75 | 0.80 | 0.95 | 0.95 |
| Adj. Flow (vph) | 56 | 40 | 35 | 28 | 34 | 23 | 49 | 279 | 25 | 26 | 387 | 114 |
| RTOR Reduction (vph) | 0 | 0 | 30 | 0 | 0 | 20 | 0 | 0 | 7 | 0 | 30 | 0 |
| Lane Group Flow (vph) | 0 | 96 | 5 | 0 | 62 | 3 | 49 | 279 | 18 | 26 | 471 | 0 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 7\% | 2\% | 2\% | 7\% | 2\% |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Perm |  | Perm | Perm |  |  |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8. |  | 8 | 2 |  | 2 | 6 |  |  |
| Actuated Green, G (s) |  | 7.7 | 7.7 |  | 7.7 | 7.7 | 41.8 | 41.8 | 41.8 | 41.8 | 41.8 |  |
| Effective Green, g (s) |  | 7.7 | 7.7 |  | 7.7 | 77 | 43.8 | 43.8 | 43.8 | 43.8 | 43.8 |  |
| Actuated g/C Ratio |  | 0.13 | 0.13 |  | 0.13 | 0.13 | 0.74 | 0.74 | 0.74 | 0.74 | 0.74 |  |
| Clearance Time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |  |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |  |
| Lane Grp Cap (vph) |  | 189 | 205 |  | 198 | 205 | 642 | 2484 | 1165 | 796 | 2425 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  | 0.08 |  |  | c0. 14 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | c0.07 | 0.00 |  | 0.04 | 0.00 | 0.06 |  | 0.01 | 0.02 |  |  |
| v/c Ratio |  | 0.51 | 0.02 |  | 0.31 | 0.01 | 0.08 | 0.11 | 0.02 | 0.03 | 0.19 |  |
| Uniform Delay, d1 |  | 24.1 | 22.6 |  | 23.5 | 22.6 | 2.2 | 2.3 | 21 | 2.1 | 2.4 |  |
| Progression Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |  |
| Incremental Delay, d2 |  | 2.1 | 0.0 |  | 09 | 0.0 | 0.2 | 0.1 | 0.0 | 0.1 | 0.2 |  |
| Delay (s) |  | 26.3 | 22.7 |  | 24.4 | 22.6 | 2.4 | 2.3 | 2.1 | 2.2 | 2.6 |  |
| Level of Service |  | c | C |  | c | C | A | A | A | A | A |  |
| Approach Delay (s) |  | 25.3 |  |  | 23.9 |  |  | 2.3 |  |  | 2.6 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control DelayHCM Volume to Capacity ratio |  |  | 6.9 |  | HCM Le | el of S | rvice |  | A |  |  |  |
|  |  |  | 0.24 |  |  |  |  |  |  |  |  |  |
| HCM Volume to Capacity ratioActuated Cycle Length (s) |  |  | 59.5 |  | Sum of | st time |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 38.1\% |  | CU Lev | of Se | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |



C Critical Lane Group

|  |  |  |  |  | 4 |  | 4 | 4 | 7 |  | 1 | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL. | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 | 7 |  | 4 | " | \% | 44 | \% | ${ }^{4}$ | 44 | 7 |
| \|deal Flow (vphpl). | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 100 | 0.95 | 100 | 1.00 | 0.95 | 1.00 |
| Frt |  | 1.00 | 0.85 |  | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Fit Protected |  | 0.97 | 100 |  | 0.98 | 1.00 | 0.95 | 100 | 1.00 | 0.95 | 1.00 | 100 |
| Satd. Flow (prot) |  | 1809 | 1583 |  | 1817 | 1583 | 1770 | 3374 | 1583 | 1770 | 3374 | 1583 |
| Fit Permitted |  | 0.76 | 1.00 |  | 0.79 | 1.00 | 0.48 | 1.00 | 1.00 | 0.48 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1425 | 1583 |  | 1481 | 1583 | 901 | 3374 | 1583 | 887 | 3374 | 1583 |
| Volume (vph) | 80 | 55 | 100 | 40 | 40 | 35 | 80 | 460 | 45 | 60 | 445 | 65 |
| Peak-hour factor, PHF | 0.85 | 0.85 | 0.95 | 0.85 | 0.85 | 0.85 | 0.85 | 0.95 | 0.85 | 0.85 | 0.95 | 0.85 |
| Adj. Flow (vph) | 94 | 65 | 105 | 47 | 47 | 41 | 94 | 484 | 53 | 71 | 468 | 76 |
| RTOR Reduction (vph) | 0 | 0 | 84 | 0 | 0 | 33 | 0 | 0 | 18 | 1 | 0 | 25 |
| Lane Group Flow (vph) | 0 | 159 | 21 | 0 | 94 | 8 | 94 | 484 | 35 | 71 | 468 | 51 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 7\% | 2\% | 2\% | 7\% | 2\% |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Perm |  | Perm | Perm |  | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 1. | 6 |  | 6 |
| Actuated Green, G (s) |  | 11.7 | 11.7 |  | 11.7 | 11.7 | 37.1 | 37.1 | 37.1 | 37.1 | 37.1 | 37.1 |
| Effective Green, 9 ( s ) |  | 11.7 | 11.7 |  | 117 | 117 | 39.1 | 39.1 | 39.1 | 39.1 | 39.1 | 39.1 |
| Actuated g/C Ratio |  | 0.20 | 0.20 |  | 0.20 | 0.20 | 0.66 | 0.66 | 0.66 | 0.66 | 0.66 | 0.66 |
| Clearance Time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 284 | 315 |  | 295 | 315 | 599 | 2244 | 1053 | 590 | 2244 | 1053 |
| $\mathrm{V} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  | c0. 14 |  |  | 0.14 |  |
| $\mathrm{V} / \mathrm{s}$ Ratio Perm |  | c0. 11 | 0.01 |  | 0.06 | 0.01 | 0.10 |  | 0.02 | 0.08 |  | 0.03 |
| v/c Ratio |  | 0.56 | 0.07 |  | 0.32 | 0.03 | 0.16 | 0.22 | 0.03 | 0.12 | 0.21 | 0.05 |
| Uniform Delay, d1 |  | 21.2 | 19.1 |  | 20.1 | 190 | 3.7 | 3.9 | 3.4 | 3.6 | 3.8 | 3.4 |
| Progression Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 2.4 | 0.1 |  | 0.6 | 0.0 | 06 | 0.2 | 0.1 | 0.4 | 02 | 0.1 |
| Delay (s) |  | 23.6 | 19.2 |  | 20.8 | 19.0 | 4.2 | 4.1 | 3.4 | 4.0 | 4.0 | 3.5 |
| Level of Service |  | c | B |  | c | B | A | A | A | A | A | A |
| Approach Delay (s) |  | 21.9 |  |  | 20.2 |  |  | 4.0 |  |  | 4.0 |  |
| Approach LOS |  | c |  |  | C |  |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 8.2 |  | HCM Le | el of S | rvice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.30 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s). |  |  | 58.8 |  | Sum of | st time |  |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 40.7\% |  | ICU Lev | of Se | vice |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

|  | * |  |  |  |  |  | 4 | $\dagger$ | $P$ |  | $\downarrow$ | $\stackrel{ }{ }+$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 | 7 |  | $\uparrow$ | " | \% | 44 | " | ${ }^{K}$ | 44 | 「 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 | 4.0 |
| Lane Util. Factor |  | 1.00 | 100 |  | 1.00 | 1.00 | 1.00 | 0.95 | 100 | 100 | 0,95 | 1.00 |
| Frt |  | 1.00 | 0.85 |  | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Flt Protected |  | 0.97 | 1.00 |  | 098 | 1.00 | 0.95 | 1.00 | 100 | 0.95 | 100 | 1.00 |
| Satd. Flow (prot) |  | 1814 | 1583 |  | 1817 | 1583 | 1770 | 3374 | 1583 | 1770 | 3374 | 1583 |
| Flt Permitted |  | 0.71 | 100 |  | 076 | 1.00 | 0.35 | 1.00 | 100 | 0.41 | 100 | 100 |
| Satd. Flow (perm) |  | 1324 | 1583 |  | 1413 | 1583 | 650 | 3374 | 1583 | 765 | 3374 | 1583 |
| Volume (vph) | 75 | 65 | 75 | 80 | 80 | 75 | 120 | 600 | 125 | 90 | 725 | 65 |
| Peak-hour factor, PHF | 0.85 | 0.85 | 0.85 | 0.90 | 0.90 | 0.85 | 0.95 | 0.95 | 0.95 | 0.90 | 0.95 | 0.85 |
| Adj Flow (vph) | 88 | 76 | 88 | 89 | 89 | 88 | 126 | 632 | 132 | 100 | 763 | 76 |
| RTOR Reduction (vph) | 0 | 0 | 70 | 0 | 0 | 70 | 0 | 0 | 48 | 0 | 0 | 28 |
| Lane Group Flow (vph) | 0 | 164 | 18 | 0 | 178 | 18 | 126 | 632 | 84 | 100 | 763 | 48 |
| Heavy Vehicles (\%) | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 2\% | 7\% | 2\% | 2\% | 7\% | 2\% |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Perm |  | Perm | Perm |  | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 10.1 | 10.1 |  | 10.1 | 10.1 | 29.9 | 29.9 | 29.9 | 29.9 | 29.9 | 29.9 |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 10.1 | 10.1 |  | 10.1 | 10.1 | 31.9 | 31.9 | 319 | 31.9 | 31.9 | 31.9 |
| Actuated g/C Ratio |  | 0.20 | 0.20 |  | 0.20 | 0.20 | 0.64 | 0.64 | 0.64 | 0.64 | 0.64 | 0.64 |
| Clearance Time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 267 | 320 |  | 285 | 320 | 415 | 2153 | 1010 | 488 | 2153 | 1010 |
| v/s Ratio Prot |  |  |  |  |  |  |  | 0.19 |  |  | c0. 23 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | 0.12 | 0.01 |  | co. 13 | 0.01 | 0.19 |  | 0.05 | 0.13 |  | 0.03 |
| v/c Ratio |  | 0.61 | 0.06 |  | 0.62 | 0.06 | 0.30 | 0.29 | 0.08 | 0.20 | 0.35 | 0.05 |
| Uniform Delay, d1 $^{1}$ |  | 18.2 | 16.1 |  | 18.2 | 16.1 | 4.1 | 4.0 | 3.5 | 3.8 | 4.2 | 3.4 |
| Progression Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 42 | 0.1 |  | 4.2 | 0.1 | 19 | 0.3 | 0.2 | 0.9 | 0.5 | 0.1 |
| Delay (s) |  | 22.3 | 16.2 |  | 22.4 | 16.2 | 5.9 | 4.4 | 3.6 | 4.7 | 4.7 | 3.5 |
| Level of Service |  | C | B |  | C | B | A | A | A | A | A | A |
| Approach Delay (s) |  | 20.2 |  |  | 20.4 |  |  | 4.5 |  |  | 4.6 |  |
| Approach LOS |  | C |  |  | C |  |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 8.0 |  | HCM Lev | el of S | ervice |  | A |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.42 |  |  |  |  |  |  |  |  |  |
|  |  |  | 50.0 |  | Sum of lo | ost time | (s) |  | 8.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 52.0\% |  | ICU Leve | of Se | vice |  | A |  |  |  |
| Analysis Period (min)... |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


|  | 4 | $\rightarrow$ |  |  |  |  | 4 | 4 | 7 | 5 | $\downarrow$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | 4 | $\stackrel{7}{7}$ |  | $\uparrow$ | \％ | ＊ | 坐 | 7 | \％ | 本車 | P |
| Ideal Flow（vphpl） | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time（s） |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Utill Factor |  | 1.00 | 100 |  | 1.00 | 100 | 1.00 | 0.95 | 100 | 1.00 | 0.95 | 1.00 |
| Frt |  | 1.00 | 0.85 |  | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Fit Protected |  | 0.97 | 1.00 |  | 0.98 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd．Flow（prot） |  | 1813 | 1583 |  | 1823 | 1583 | 1770 | 3406 | 1583 | 1770 | 3406 | 1583 |
| Flt Permitted |  | 0.70 | 100 |  | 0.70 | 100 | 0.44 | 1.00 | 1.00 | 0.45 | 1.00 | 1.00 |
| Satd．Flow（perm） |  | 1307 | 1583 |  | 1301 | 1583 | 825 | 3406 | 1583 | 830 | 3406 | 1583 |
| Volume（vph） | 80 | 65 | 100 | 40 | 50 | 65 | 80 | 510 | 45 | 85 | 515 | 65 |
| Peak－hour factor，PHF | 0.90 | 0.90 | 0.95 | 0.90 | 0.90 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.85 |
| Adj Flow（vph） | 89 | 72 | 105 | 44 | 56 | 68 | 84 | 537 | 47 | 89 | 542 | 76 |
| RTOR Reduction（vph） | 0 | 0 | 88 | 0 | 0 | 57 | 0 | 0 | 10 | 0 | 0 | 17 |
| Lane Group Flow（vph） | 0 | 161 | 17. | 0 | 100 | 11 | 84 | 537 | 37 | 89 | 542 | 59 |
| Heavy Vehicles（\％） | 2\％ | 2\％ | 2\％ | 2\％ | 2\％ | 2\％ | 2\％ | 6\％ | 2\％ | 2\％ | 6\％ | 2\％ |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Perm |  | Perm | Perm |  | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8 | 2 |  | 2 | 6 |  | 6 |
| Actuated Green，G（s） |  | 15.2 | 15.2 |  | 15.2 | 15.2 | 74.8 | 74.8 | 74.8 | 74.8 | 74.8 | 74.8 |
| Effective Green，g（s） |  | 16.2 | 16.2 |  | 16.2 | 16.2 | 77.8 | 77.8 | 77.8 | 77.8 | 77.8 | 77.8 |
| Actuated g／C Ratio |  | 0.16 | 0.16 |  | 0.16 | 0.16 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 | 0.78 |
| Clearance Time（s） |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension（s） |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap（vph） |  | 212 | 256 |  | 211 | 256 | 642 | 2650 | 1232 | 646 | 2650 | 1232 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  | 0.16 |  |  | c0． 16 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | co． 12 | 0.01 |  | 0.08 | 0.01 | 0.10 |  | 0.02 | 0.11 |  | 0.04 |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.76 | 0.07 |  | 0.47 | 0.04 | 0.13 | 0.20 | 0.03 | 0.14 | 0.20 | 0.05 |
| Uniform Delay，d1 |  | 40.0 | 35.5 |  | 38.0 | 35.4 | 2.7 | 2.9 | 2.5 | 2.8 | 2.9 | 2.6 |
| Progression Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 2.34 | 2.22 | 4.66 | 1.00 | 1.00 | 1.00 |
| Incremental Delay，d2 |  | 14.4 | 0.1 |  | 17 | 0.1 | 0.4 | 0.2 | 0.0 | 0.4 | 0.2 | 0.1 |
| Delay（s） |  | 54.5 | 35.6 |  | 39.7 | 35.4 | 6.8 | 6.7 | 11.8 | 3.2 | 3.1 | 2.6 |
| Level of Service |  | D | D |  | D | D | A | A | B | A | A | A |
| Approach Delay（s） |  | 47.0 |  |  | 38.0 |  |  | 7.0 |  |  | 3.1 |  |
| Approach LOS |  | D |  |  | D |  |  | A |  |  | A |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 14.2 |  | HCM Le | vel of S | rvice |  | B |  |  |  |
| HCM Volume to Capacity ratioActuated Cycle Length（s） |  |  | 0.30 |  |  |  |  |  |  |  |  |  |
|  |  |  | 100.0 |  | Sum of | ost time |  |  | 6.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 43．3\％ |  | ICU Level of Service |  |  |  | A |  |  |  |
| Analysis Period（min） |  | 15 |  |  |  |  |  |  |  |  |  |  |

c Critical Lane Group

|  | 4 |  |  |  |  | 4 | 4 | $\dagger$ | 7 | * | $\dagger$ | $\checkmark$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\uparrow$ | F |  | $\uparrow$ | 「 | ${ }^{4}$ | 14 | 7 | ${ }^{*}$ | 44 | F |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Util. Factor |  | 1.00 | 1.00 |  | 1.00 | 100 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 |
| Frt |  | 1.00 | 0.85 |  | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 | 1.00 | 1.00 | 0.85 |
| Fit Protected |  | 0.98 | 100 |  | 0.98 | 1.00 | 0.95 | 1.00 | 1.00 | 0.95 | 1.00 | 1.00 |
| Satd. Flow (prot) |  | 1835 | 1599 |  | 1838 | 1599 | 1787 | 3406 | 1599 | 1787 | 3406 | 1599 |
| Fit Permitted |  | 0.79 | 1.00 |  | 0.80 | 1.00 | 0.32 | 100 | 100 | 0.36 | 1.00 | 1.00 |
| Satd. Flow (perm) |  | 1486 | 1599 |  | 1505 | 1599 | 596 | 3406 | 1599 | 672 | 3406 | 1599 |
| Volume (vph) | 75 | 75 | 75 | 80 | 90 | 115 | 120 | 695 | 125 | 140 | 795 | 65 |
| Peak-hour factor, PHF | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.95 | 0.90 |
| Adj. Flow (vph) | 79 | 79 | 79 | 84 | 95 | 121 | 126 | 732 | 132 | 147 | 837 | 72 |
| RTOR Reduction (vph) | 0 | 0 | 65 | 0 | 0 | 100 | 0 | 0 | 31 | 0 | 0 | 17 |
| Lane Group Flow (vph) | 0 | 158 | 14 | 0 | 179 | 21. | 126 | 732 | 101. | 147 | 837 | 55 |
| Heavy Vehicles (\%) | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 1\% | 6\% | 1\% | 1\% | 6\% | 1\% |
| Turn Type | Perm |  | Perm | Perm |  | Perm | Perm |  | Perm | Perm |  | Perm |
| Protected Phases |  | 4 |  |  | 8 |  |  | 2 |  |  | 6 |  |
| Permitted Phases | 4 |  | 4 | 8 |  | 8. | 2 |  | 2 | 6 |  | 6 |
| Actuated Green, G (s) |  | 16.3 | 16.3 |  | 16.3 | 16.3 | 73.7 | 73.7 | 73.7 | 73.7 | 73.7 | 73.7 |
| Effective Green, g (s) |  | 17.3 | 17.3 |  | 17.3 | 173 | 76.7 | 76.7 | 76.7 | 76.7 | 76.7 | 76.7 |
| Actuated g/C Ratio |  | 0.17 | 0.17 |  | 0.17 | 0.17 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 | 0.77 |
| Clearance Time (s) |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 | 6.0 |
| Vehicle Extension (s) |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 | 3.0 |
| Lane Grp Cap (vph) |  | 257 | 277 |  | 260 | 277 | 457 | 2612 | 1226 | 515 | 2612 | 1226 |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  |  |  |  |  |  |  | 0.21 |  |  | c0.25 |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  | 011 | 0.01 |  | co. 12 | 0.01 | 0.21 |  | 0.06 | 0.22 |  | 0.03 |
| v/c Ratio |  | 0.61 | 0.05 |  | 0.69 | 0.08 | 0.28 | 0.28 | 0.08 | 0.29 | 0.32 | 0.05 |
| Uniform Delay, d1 |  | 38.3 | 34.5 |  | 38.8 | 34.6 | 3.4 | 3.5 | 2.9 | 3.5 | 3.6 | 2.8 |
| Progression Factor |  | 1.00 | 1.00 |  | 1.00 | 1.00 | 1.89 | 1.89 | 4.19 | 1.00 | 1.00 | 1.00 |
| Incremental Delay, d2 |  | 4.3 | 0.1 |  | 7.4 | 0.1 | 1.4 | 0.3 | 0.1 | 1.4 | 0,3 | 0.1 |
| Delay (s) |  | 42.6 | 34.6 |  | 46.2 | 34.8 | 7.9 | 6.8 | 12.3 | 4.9 | 3.9 | 2.9 |
| Level of Service |  | D | C. |  | D | C. | A | A | B | A | A | A |
| Approach Delay (s) |  | 39.9 |  |  | 41.6 |  |  | 7.7 |  |  | 4.0 |  |
| Approach LOS |  | D |  |  | D |  |  | A |  |  | A |  |
| mersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 13.1 |  | HCM Le | el of Se | rvice |  | B |  |  |  |
| HCM Volume to Capacity ratio |  |  | 0.39 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) . |  |  | 100.0 |  | Sum of 1 | st time |  |  | 6.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 54.5\% |  | ICU Leve | of Ser | vice |  | A |  |  |  |
| Analysis Period (min) . |  |  | 15 |  |  |  |  |  |  |  |  |  |

c Critical Lane Group








|  | \% |  |  |  |  |  |  | $\uparrow$ | 1 | * | $\dagger$ | * |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | ¢ |  |  | 4 |  |  | $\dagger$ |  |  | * |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Volume (vph) | 5 | 20 | 5 | 10 | 30 | 65 | 5 | 85 | 10 | 45 | 150 | 10 |
| Peak Hour Factor | 065 | 0.80 | 0.65 | 070 | 0.85 | 0.85 | 0.65 | 0.90 | 0.70 | 0.85 | 0.95 | 0.70 |
| Hourly flow rate (vph) | 8 | 25 | 8 | 14 | 35 | 76 | 8 | 94 | 14 | 53 | 158 | 14 |
| Direction Lane \# | EB 1 | WB1 | NB 1 | SB 1 |  |  |  |  |  |  |  |  |
| Volume Total (vph) | 40 | 126 | 116 | 225 |  |  |  |  |  |  |  |  |
| Volume Left (vph) | 8 | 14 | 8 | 53 |  |  |  |  |  |  |  |  |
| Volume Right (vph) | 8 | 76 | 14 | 14 |  |  |  |  |  |  |  |  |
| Hadj (s) | -0.04 | -0.31 | -0.03 | 0.04 |  |  |  |  |  |  |  |  |
| Departure Headway (s) | 4.8 | 4.4 | 4.5 | 4.5 |  |  |  |  |  |  |  |  |
| Degree Utilization, $x$ | 0.05 | 0.16 | 015 | 0.28 |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 681 | 747 | 753 | 767 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 8.1 | 8.3 | 8.3 | 92 |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 8.1 | 8.3 | 8.3 | 9.2 |  |  |  |  |  |  |  |  |
| Approach LOS | A | A | A | A |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Delay |  |  | 8.7 |  |  |  |  |  |  |  |  |  |
| HCM Level of Service |  |  | A |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 31.5\% |  | CU Leve | of Ser |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |



|  | * |  |  | $\psi$ |  |  | 4 | $\uparrow$ | \% |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations |  | $\dagger$ |  |  | $\dagger$ |  |  | $\uparrow$ |  |  | $\dagger$ |  |
| Sign Control |  | Stop |  |  | Stop |  |  | Stop |  |  | Stop |  |
| Volume (vph) | 5 | 110 | 30 | 20 | 100 | 95 | 30 | 135 | 20 | 85 | 200 | 10 |
| Peak Hour Factor | 0.65 | 0,95 | 0.85 | 0.80 | 0.95 | 090 | 0.85 | 0.95 | 080 | 0.90 | 0.95 | 0.70 |
| Hourly flow rate (vph) | 8 | 116 | 35 | 25 | 105 | 106 | 35 | 142 | 25 | 94 | 211 | 14 |
| Birection, Lane \# | EB 1 | WB1 | NB1 | SB1 |  |  |  |  |  |  |  |  |
| Volume Total (vph) | 159 | 236 | 202 | 319 |  |  |  |  |  |  |  |  |
| Volume Left (vph) | 8 | 25 | 35 | 94 |  |  |  |  |  |  |  |  |
| Volume Right (vph) | 35 | 106 | 25 | 14 |  |  |  |  |  |  |  |  |
| Hadj (s) | -0.09 | -0.21 | -0.01 | 0.07 |  |  |  |  |  |  |  |  |
| Departure Headway (s) | 5.7 | 5.4 | 5.6 | 5.4 |  |  |  |  |  |  |  |  |
| Degree Utilization, $\times$ | 0.25 | 0.36 | 0.31 | 0.48 |  |  |  |  |  |  |  |  |
| Capacity (veh/h) | 559 | 599 | 584 | 620 |  |  |  |  |  |  |  |  |
| Control Delay (s) | 10.6 | 11.4 | 11.1 | 13.4 |  |  |  |  |  |  |  |  |
| Approach Delay (s) | 10.6 | 11.4 | 11.1 | 13.4 |  |  |  |  |  |  |  |  |
| Approach LOS | B | B | B | B |  |  |  |  |  |  |  |  |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| Delay |  |  | 11.9 |  |  |  |  |  |  |  |  |  |
| HCM Level of Service |  |  | B |  |  |  |  |  |  |  |  |  |
| Intersection Capacity Utilization |  |  | 53.8\% |  | CU Leve | of Se |  |  | A |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |




|  | 7 |  | $\dagger$ | 7 |  | $\downarrow$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | WBL | WBR | NBT | NBR | SB1 | SBT |  |
| Lane Configurations | ${ }^{4}$ |  | 4 | 7 |  | $\uparrow$ |  |
| Sign Control | Stop |  | Stop |  |  | Stop |  |
| Volume (vph) | 20 | 15 | 50 | 105 | 75 | 65 |  |
| Peak Hour Factor | 0.80 | 0.75 | 0.85 | 0.95 | 0,85 | 0.85 |  |
| Hourly flow rate (vph) | 25 | 20 | 59 | 111 | 88 | 76 |  |
| Direction, Lane \# | WB 1 | NB1 | NB2 | SB1 |  |  |  |
| Volume Total (vph) | 45 | 59 | 111 | 165 |  |  |  |
| Volume Left (vph) | 25 | 0 | 0 | 88 |  |  |  |
| Volume Right (vph) | 20 | 0 | 111 | 0 |  |  |  |
| Hadj (s) | -0.12 | 0.03 | -0.67 | 0.14 |  |  |  |
| Departure Headway (s) | 4.5 | 4.8 | 4.1 | 4.4 |  |  |  |
| Degree Utilization, $x$ | 0.06 | 0.08 | 0.12 | 0.20 |  |  |  |
| Capacity (veh/h) | 739 | 738 | 864 | 803 |  |  |  |
| Control Delay (s) | 7.8 | 7.0 | 6.4 | 8.5 |  |  |  |
| Approach Delay (s) | 7.8 | 6.6 |  | 8.5 |  |  |  |
| Approach Los | A | A |  | A |  |  |  |
| Hetersection Summary |  |  |  |  |  |  |  |
| Delay |  |  | 7.6 |  |  |  |  |
| HCM Level of Service |  |  | A |  |  |  |  |
| Intersection Capacity Utilization |  |  | 24.2\% |  | ICU Leve | of Service | A |
| Analysis Period (min) |  |  | 15 |  |  |  |  |




LSC, Inc.


## Appendix C: Time/Space Diagrams









[^0]:    W: \LSC $\backslash$ Projects $\backslash 2021 \backslash 210040$-GunnisonRisingPhase2 $\backslash$ Report $\backslash$ Nov-2021 $\backslash$ GunnisonRising-Summary-112921.wpd

